pg

of

rudow + berry
structural engineering
scottsdale, arizona 85251

t (480) 946-8171

f (480) 946-9480

job name: job number:

designed by:

checked by:

CCW Powdercat

17100

MAR

date: 2/18

date:

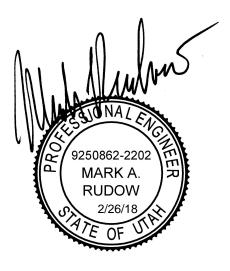
COPPER CREST WEST – POWDERCAT

Foundation Revisions

During the Initial construction period, the geotechnical engineer has reassessed the foundation conditions and has made supplemental recommendations. These new recommendations are significantly different than the original recommendations such that most footings can be decreased. The allowable soil bearing pressure has been increased from 2400 psf to 3700 psf and in addition, a 1.33 increase factor has been allowed for load cases that include wind and/or seismic loading.

The following calculations reflect the changes to the foundation design to incorporate these new recommendations. The slab support recommendations were also revised and the slab system called out on the foundation plans has been revised accordingly.

The geotechnical addendum has been attached following the revised calculations.



structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

	SHE	AR WALL FO	OTING DESIG	GN	
INPUT DATA :	Typical L	Init Far South Wal			
Fy = 60 ksi f'c = 3000 psi Wall DL = 0.61 klf Roof LL = 2.08 klf Floor LL = 0.24 klf	ksf feet inches		DL OTM = FLR LL OTM = RF LL OTM = WIND OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	0.00 ft-kips 0 ft-kips 0 ft-kips 45.06 ft-kips 20.00 feet 0.81 feet 12 inches 0.636 klf	
EQ'N 16-11: DL + .75(FL + R P = 59.7 kips OTM = 0.00 ft-kips e = 0.00 feet Soil Pr. = 3.68 ksf, max., EQ'N 16-13: DL + .75(FL + RL	$P_{ult} = OTM_{ult} = X bar = 5.28$	0 ft-kips		USE 1'-8" x 12" TI (Min. per Geotech Ro (2) #5 Longitudin Required Width =	eport) al
P = 59.7 kips OTM = 33.8 ft-kips e = 0.57 feet Soil Pr. = 4.31 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	54.072 ft-kips		Required Width =	0.71 feet
EQ'N 16-15: 0.6DL + W P = 14.9 kips OTM = 45.1 ft-kips e = 3.02 feet Soil Pr. = 1.75 ksf, max., Resisting Moment = 248.37	$ OTM_{ULT} = X bar = 2.11 $ ' ft-kips	72.096 ft-kips		Required Width = Factor of Safety =	0.29 feet 7.87
LONGITUDINAL DIRECTION					
Req'd Unreinf Thickness = Moment = 0.34 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	21 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.50 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	30 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.01 0.01	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OTING DESIG	GN	
INPUT DATA :	Unit 124	Far South Wall			
			Footing Length: Footing Width: Footing Thkness:	0 ft-kips 42.56 ft-kips 26.67 feet 0.85 feet	
OUTPUT DATA :					
EQ'N 16-11: DL + .75(FL + RL P = 82.5 kips OTM = 0.00 ft-kips e = 0.00 feet Soil Pr. = 3.64 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	N/A feet		USE 1'-8" x 12" The (Min. per Geotech Received (2) #5 Longituding Required Width =	eport) al
EQ'N 16-13: DL + .75(FL + RL + P = 82.5 kips OTM = 31.9 ft-kips e = 0.39 feet Soil Pr. = 3.96 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	51.072 ft-kips N/A feet		Required Width =	0.68 feet
OTM = 42.6 ft-kips	$OTM_{ULT} = X bar =$	N/A feet		Required Width =	0.24 feet
Resisting Moment = 480.77	•			Factor of Safety =	16.14
FOOTING REINFORCING	3:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 0.31 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	19 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.51 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	-	fb(act.)= fv(act.)=	30 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.01 0.01	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no. 17100

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 124 North Wall Allow. Soil Pr. = DL OTM = 3.700 ksf 19.20 ft-kips 60 ksi FLR LL OTM = Fy = 3.39 ft-kips f 'c = RF LL OTM = 3000 118.07 ft-kips psi Wall DL = 0.27 klf SEISMIC OTM = 163.52 ft-kips Roof LL = Footing Length: 20.08 feet 1.77 klf Floor LL = Footing Width: 0.05 klf 2.14 feet Footing Thkness: Wall Length = 18.08 feet 12 inches Wall Thickness = 8 inches Footing DL: 1.409 klf OUTPUT DATA : EQ'N 16-11: DL + .75(FL + RL): USE 2'-6" x 12" THK P = 57.9 kips $P_{ult} =$ 79.4 kips (3) #5 Longitudinal 110.30 ft-kips OTM = $OTM_{ult} = 168.79 \text{ ft-kips}$ #5 @ 14 Transverse e = 1.90 feet X bar = N/A feet Soil Pr. = 2.11 ksf, max., 2.89 ksf, ult. Required Width = 1.22 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 57.9 kips $P_{ULT} =$ 79.4 kips $OTM_{ULT} = 365.02 \text{ ft-kips}$ OTM = 232.9 ft-kips 4.02 feet X bar = 6.02 feet e = Soil Pr. = 2.99 ksf, max., 4.10 ksf, ult. Required Width = 1.30 feet EQ'N 16-16: 0.6DL + 0.7E P = 19.9 kips P(ult) =23.9 kips OTM = 175.0 ft-kips $OTM_{ULT} = 196.97 \text{ ft-kips}$ 8.78 feet X bar = 1.26 feet e = Soil Pr. = 4.91 ksf, max., 5.89 ksf, ult. Required Width = 2.14 feet Factor of Safety = Resisting Moment = 333.70 ft-kips 2.65 FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 16 inches 5.24 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 160psi Fv(allow)= 71 psi Shear = 0.00 kips/ft fv(act.)= 0 psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 14 inches Moment = 3.39 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 141psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 12 inches Longitudinal Steel Required = 0.14 sq.in./ft. v(longit.) =17 psi Transverse Steel Required = 0.09 v(transv.)= 2 sq.in./ft. psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no.

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 124 South Wall Allow. Soil Pr. = DL OTM = 3.700 ksf 21.21 ft-kips FLR LL OTM = 11.13 ft-kips Fy = 60 ksi f 'c = RF LL OTM = 124.5 ft-kips 3000 psi Wall DL = 1.99 klf SEISMIC OTM = 246.9 ft-kips Roof LL = Footing Length: 16.00 feet 10.40 klf Floor LL = Footing Width: 0.05 klf **7.16** feet Footing Thkness: Wall Length = 5.33 feet 24 inches Wall Thickness = 8 inches Footing DL: 3.026 klf OUTPUT DATA : EQ'N 16-11: DL + .75(FL + RL): USE 16'-0" x 7'-2" x 12" THK P = 100.8 kips $P_{ult} = 137.7 \text{ kips}$ (10) #8 Longitudinal OTM = 122.93 ft-kips $OTM_{ult} = 188.21 \text{ ft-kips}$ (14) #7 Transverse e = 1.22 feet X bar = N/A feet Soil Pr. = 1.28 ksf, max., 1.75 ksf, ult. Required Width = 2.48 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 100.8 kips $P_{ULT} = 137.7 \text{ kips}$ $OTM_{ULT} = 484.49 \text{ ft-kips}$ OTM = 308.1 ft-kips 3.06 feet X bar = 4.94 feet e = Soil Pr. = 1.90 ksf, max., 2.59 ksf, ult. Required Width = 2.76 feet EQ'N 16-16: 0.6DL + 0.7E P = 35.4 kips P(ult) =42.5 kips OTM = 259.6 ft-kips $OTM_{UIT} =$ 291.8 ft-kips 7.33 feet 0.67 feet e = X bar = Soil Pr. = 4.92 ksf, max., 5.91 ksf, ult. Required Width = 7.16 feet Factor of Safety = 2.55 Resisting Moment = 472.27 ft-kips FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 60 inches 94.90 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 169psi Fv(allow)= 71 psi Shear = 1.98 kips/ft fv(act.)= psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 38 inches Moment = 37.83 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 175psi Shear = 0.47 kips/ft Fv(allow)= 71 psi fv(act.)= 2 psi Reinf. Thickness (if used) = 24 inches Longitudinal Steel Required = 1.09 sq.in./ft. v(longit.) =87 psi Transverse Steel Required = 0.42 v(transv.)= sq.in./ft. 37 psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no. 17100

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 125 & 126 South Walls Allow. Soil Pr. = DL OTM = 0.00 ft-kips 3.700 ksf FLR LL OTM = 0 ft-kips Fy = 60 ksi f 'c = RF LL OTM = 0 ft-kips 3000 psi Wall DL = 1.54 klf SEISMIC OTM = 343.42 ft-kips Roof LL = 11.14 Footing Length: 19.33 feet klf Floor LL = Footing Width: 0.11 klf 6.18 feet Footing Thkness: Wall Length = 9.33 feet 24 inches Wall Thickness = 8 inches Footing DL: 2.616 klf OUTPUT DATA: EQ'N 16-11: DL + .75(FL + RL): USE 19'-4" x 6'-0" x 12" THK P = 143.7 kips $P_{ult} =$ (10) #7 Longitudinal 203.9 kips OTM = 0.00 ft-kips $OTM_{ult} =$ 0.00 ft-kips (17) #7 Transverse (Delta W = 3% - OK) e = 0.00 feet X bar = N/A feet Soil Pr. = 1.20 ksf, max., 1.71 ksf, ult. Required Width = 2.01 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 143.7 kips $P_{ULT} = 203.9 \text{ kips}$ $OTM_{ULT} =$ OTM = 257.6 ft-kips 412.1 ft-kips 1.79 feet X bar = N/A feet e = Soil Pr. = 1.87 ksf, max., 2.66 ksf, ult. Required Width = 2.35 feet EQ'N 16-16: 0.6DL + 0.7E P = 39.0 kips P(ult) =46.8 kips OTM = 343.4 ft-kips $OTM_{ULT} = 384.63 \text{ ft-kips}$ 8.81 feet X bar = 0.85 feet e = Soil Pr. = 4.92 ksf, max., 5.90 ksf, ult. Required Width = 6.18 feet Factor of Safety = 2.61 Resisting Moment = 627.86 ft-kips FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 56 inches 83.97 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 173psi Fv(allow)= 71 psi Shear = 1.97 kips/ft fv(act.)= psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 34 inches Moment = 28.21 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 165psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 24 inches Longitudinal Steel Required = 0.95 sq.in./ft. v(longit.) =79 psi Transverse Steel Required = v(transv.)= 25 0.31 sq.in./ft. psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

	SHE	AR WALL FO	OTING DESIG	N	
INPUT DATA :	Unit 125	North Wall			
•	ksf feet inches		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	22.95 ft-kips 2.7 ft-kips 148.45 ft-kips 114.79 ft-kips 16.92 feet 2.39 feet 12 inches 1.407 klf	
EQ'N 16-11 : DL + .75(FL + R P = 53.1 kips OTM = 136.31 ft-kips e = 2.56 feet Soil Pr. = 2.51 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	•		USE 2'-6" x 12" TI (3) #5 Longitudin #5 @ 14 Transver	al rse
EQ'N 16-14: DL + .75(FL + RL P = 53.1 kips OTM = 222.4 ft-kips e = 4.18 feet Soil Pr. = 3.47 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	346.67 ft-kips 4.28 feet		Required Width =	1.68 feet
EQ'N 16-16: 0.6DL + 0.7E P = 17.2 kips OTM = 128.6 ft-kips e = 7.49 feet Soil Pr. = 4.93 ksf, max., Resisting Moment = 242.12	OTM _{ULT} = X bar = 5.91	145.09 ft-kips		Required Width = Factor of Safety =	
FOOTING REINFORCING	•			•	
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 5.25 ft-kips/ft Shear = 0.00 kips/ft		inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	161 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 4.21 ft-kips/ft Shear = 0.00 kips/ft	14	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	176 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.14 0.11	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	17 psi 9 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no. 17100

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 126 North Wall Allow. Soil Pr. = DL OTM = 3.700 ksf 23.07 ft-kips FLR LL OTM = Fy = 60 ksi 2.23 ft-kips f 'c = RF LL OTM = 3000 psi 151.91 ft-kips Wall DL = 0.33 klf SEISMIC OTM = 135.46 ft-kips Roof LL = Footing Length: 16.83 feet 2.19 klf Floor LL = Footing Width: 0.04 klf 2.89 feet Footing Thkness: Wall Length = 14.83 feet 12 inches Wall Thickness = 8 inches Footing DL: klf 1.689 OUTPUT DATA : EQ'N 16-11: DL + .75(FL + RL): USE 3'-0" x 12" THK P = 58.0 kips $P_{ult} =$ (3) #5 Longitudinal 79.6 kips OTM = 138.68 ft-kips $OTM_{ult} = 212.65 \text{ ft-kips}$ #5 @ 14 Transverse e = 2.39 feet X bar = N/A feet Soil Pr. = 2.21 ksf, max., 3.03 ksf, ult. Required Width = 1.73 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 58.0 kips $P_{ULT} =$ 79.6 kips $OTM_{ULT} =$ OTM = 240.3 ft-kips 375.2 ft-kips 4.14 feet X bar = 4.28 feet e = Soil Pr. = 3.13 ksf, max., 4.29 ksf, ult. Required Width = 1.84 feet EQ'N 16-16: 0.6DL + 0.7E P = 20.0 kips P(ult) =24.0 kips OTM = 149.3 ft-kips $OTM_{ULT} = 168.33 \text{ ft-kips}$ 7.48 feet X bar = 0.94 feet e = Soil Pr. = 4.92 ksf, max., 5.91 ksf, ult. Required Width = 2.89 feet Factor of Safety = 2.58 Resisting Moment = 279.94 ft-kips FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 16 inches 5.25 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 161psi Fv(allow)= 71 psi Shear = 0.00 kips/ft fv(act.)= 0 psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 18 inches Moment = 6.17 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 145psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 12 inches Longitudinal Steel Required = 0.14 sq.in./ft. v(longit.) =17 psi Transverse Steel Required = v(transv.)= 23 0.16 sq.in./ft. psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

	2:15			- - ,				
SHEAR WALL FOOTING DESIGN								
INPUT DATA :	Unit 127	& 128 South Wall	s					
Wall Thickness = 8	ksf feet inches		Footing Length: Footing Width: Footing Thkness:	0 ft-kips 0 ft-kips 333.47 ft-kips 19.33 feet 5.95 feet				
OUTPUT DATA:								
EQ'N 16-11: DL + .75(FL + RL P = 141.8 kips OTM = 0.00 ft-kips e = 0.00 feet Soil Pr. = 1.23 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	N/A feet	(10)	-4" x 6'-0" x 12" THK #7 Longitudinal) #7 Transverse Required Width =	1.98 feet			
EQ'N 16-14: DL + .75(FL + RL + P = 141.8 kips OTM = 250.1 ft-kips e = 1.76 feet Soil Pr. = 1.91 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	400.16 ft-kips N/A feet		Required Width =	2.31 feet			
EQ'N 16-16: 0.6DL + 0.7E P = 37.9 kips OTM = 333.5 ft-kips e = 8.80 feet Soil Pr. = 4.92 ksf, max.,	OTM _{ULT} = X bar =	373.49 ft-kips 0.86 feet		Required Width =	5.95 feet			
		Noi, ait.		-				
Resisting Moment = 610.27		1		Factor of Safety =	2.61			
FOOTING REINFORCING LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 83.93 ft-kips/ft Shear = 1.97 kips/ft TRANSVERSE DIRECTION:	<u>: ح</u>	inches Fb(allow)= 17 Fv(allow)= 7	•	fb(act.)= fv(act.)=	173 psi 4 psi			
Req'd Unreinf Thickness = Moment = 26.13 ft-kips/ft Shear = 0.00 kips/ft	32	inches Fb(allow)= 17 Fv(allow)= 7	-	fb(act.)= fv(act.)=	174 psi 0 psi			
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	24 0.95 0.29	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	79 psi 22 psi 93.1 psi			

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

	SHEA	AR WALL F	-00	TING DESIG	SN		
INPUT DATA :	Unit 127	North Wall					
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 0.32 klf Roof LL = 2.14 klf Floor LL = 0.03 klf Wall Length = 14.92 Wall Thickness = 8	feet		F S F F	L OTM = LR LL OTM = F LL OTM = EISMIC OTM = ooting Length : ooting Width : ooting Thkness: ooting DL :	136.16 ft-kips 16.92 feet 2.88 feet		
EQ'N 16-11 : DL + .75(FL + R P = 57.4 kips OTM = 136.45 ft-kips e = 2.38 feet Soil Pr. = 2.17 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	N/A feet	i		USE 3'-0" x 12" T (3) #5 Longitudin #5 @ 14 Transve	nal erse	feet
EQ'N 16-14: DL + .75(FL + RL P = 57.4 kips OTM = 238.6 ft-kips e = 4.16 feet Soil Pr. = 3.09 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	372.59 ft-kips 4.30 feet	;		Required Width =	1.81	feet
EQ'N 16-16: 0.6DL + 0.7E P = 19.9 kips OTM = 149.9 ft-kips e = 7.52 feet Soil Pr. = 4.92 ksf, max.,	$OTM_{ULT} = X bar =$	168.93 ft-kips 0.94 feet	;		Required Width =	2.88	feet
Resisting Moment = 280.83	ft-kips	_			Factor of Safety =	2.58	
FOOTING REINFORCING	G:						
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 5.25 ft-kips/ft Shear = 0.00 kips/ft	16	inches Fb(allow)= Fv(allow)=			fb(act.)= fv(act.)=	161 0	psi psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 6.13 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= Fv(allow)=			fb(act.)= fv(act.)=	144 0	psi psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.14 0.16	inches sq.in./ft. sq.in./ft.			v(longit.) = v(transv.)= V(allow) =	17 23 93.1	psi psi psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

SHE	AR WALL FOOTING DESIG	SN
INPUT DATA : Unit 128	North Wall	
Allow. Soil Pr. = 3.700 ksf Fy = 60 ksi f 'c = 3000 psi Wall DL = 0.32 klf Roof LL = 2.15 klf Floor LL = 0.03 klf Wall Length = 14.83 feet Wall Thickness = 8 inches	DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	116.19 ft-kips 16.83 feet 2.45 feet
OUTPUT DATA :		
$\begin{array}{llll} \mbox{EQ'N 16-11}: & DL + .75(FL + RL): \\ \mbox{P} = & 53.2 & \mbox{kips} & P_{ult} = \\ \mbox{OTM} = & 135.20 & \mbox{ft-kips} & \mbox{OTM}_{ult} = \\ \mbox{e} = & 2.54 & \mbox{feet} & X & \mbox{bar} = \\ \mbox{Soil Pr.} = & 2.46 & \mbox{ksf, max.}, & 3.39 & \mbox{Soil Pr.} \end{array}$	207.29 ft-kips N/A feet	USE 2'-6" x 12" THK (3) #5 Longitudinal #5 @ 14 Transverse Required Width = 1.63 feet
EQ'N 16-14: DL + .75(FL + RL + .7E) P = 53.2 kips P _{ULT} = OTM = 222.3 ft-kips OTM _{ULT} = e = 4.18 feet X bar = Soil Pr. = 3.41 ksf, max., 4.72	346.72 ft-kips 4.24 feet	Required Width = 1.70 feet
EQ'N 16-16: $0.6DL + 0.7E$ P = 17.4 kips P (ult) = OTM = 129.7 ft-kips OTM _{ULT} = e = 7.45 feet X bar = Soil Pr. = 4.90 ksf, max., 5.88	0.97 feet	Required Width = 2.44 feet
Resisting Moment = 244.26 ft-kips		Factor of Safety = 2.57
FOOTING REINFORCING:	1	
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = 16 Moment = 5.23 ft-kips/ft Shear = 0.00 kips/ft	inches Fb(allow)= 178 psi Fv(allow)= 71 psi	fb(act.)= 160 psi fv(act.)= 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = 16 Moment = 4.43 ft-kips/ft Shear = 0.00 kips/ft	inches Fb(allow)= 178 psi Fv(allow)= 71 psi	fb(act.)= 136 psi fv(act.)= 0 psi
Reinf. Thickness (if used) = 12 Longitudinal Steel Required = 0.14 Transverse Steel Required = 0.12	inches sq.in./ft. sq.in./ft.	v(longit.) = 17 psi v(transv.)= 11 psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no. 17100

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 129 & 130 South Walls Allow. Soil Pr. = DL OTM = 0.00 ft-kips 3.700 ksf FLR LL OTM = 0 ft-kips Fy = 60 ksi f 'c = RF LL OTM = 0 ft-kips 3000 psi Wall DL = 1.55 klf SEISMIC OTM = 333.17 ft-kips Roof LL = Footing Length: 19.33 feet 11.14 klf Floor LL = Footing Width: 0.11 klf 5.94 feet Footing Thkness: Wall Length = 9.33 feet 24 inches Wall Thickness = 8 inches Footing DL: 2.516 klf OUTPUT DATA: EQ'N 16-11: DL + .75(FL + RL): USE 19'-4" x 6'-0" x 12" THK P = 141.8 kips $P_{ult} =$ (10) #7 Longitudinal 201.6 kips OTM = 0.00 ft-kips $OTM_{ult} =$ 0.00 ft-kips (17) #7 Transverse e = 0.00 feet X bar = N/A feet Soil Pr. = 1.23 ksf, max., 1.75 ksf, ult. Required Width = 1.98 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 141.8 kips $P_{ULT} =$ 201.6 kips $OTM_{ULT} =$ OTM = 249.9 ft-kips 399.8 ft-kips 1.76 feet X bar = N/A feet e = Soil Pr. = 1.91 ksf, max., 2.71 ksf, ult. Required Width = 2.31 feet EQ'N 16-16: 0.6DL + 0.7E P = 37.8 kips P(ult) =45.4 kips OTM = 333.2 ft-kips $OTM_{ULT} = 373.15 \text{ ft-kips}$ 8.80 feet X bar = 0.86 feet e = Soil Pr. = 4.93 ksf, max., 5.91 ksf, ult. Required Width = 5.95 feet Factor of Safety = 2.61 Resisting Moment = 609.64 ft-kips FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 56 inches 84.07 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 173psi Fv(allow)= 71 psi Shear = 1.97 kips/ft fv(act.)= psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 32 inches Moment = 26.10 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 174psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 24 inches Longitudinal Steel Required = 0.96 sq.in./ft. v(longit.) =79 psi Transverse Steel Required = 0.29 v(transv.)= sq.in./ft. 22 psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no. 17100

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 129 North Wall Allow. Soil Pr. = DL OTM = 3.700 ksf 22.70 ft-kips 60 ksi FLR LL OTM = 1.64 ft-kips Fy = f 'c = RF LL OTM = 149.8 ft-kips 3000 psi Wall DL = 0.32 klf SEISMIC OTM = 113.92 ft-kips Roof LL = Footing Length: 16.92 feet 2.14 klf Floor LL = Footing Width: 0.03 klf 2.38 feet Footing Thkness: Wall Length = 14.92 feet 12 inches Wall Thickness = 8 inches Footing DL: klf 1.399 OUTPUT DATA: EQ'N 16-11: DL + .75(FL + RL): USE 2'-6" x 12" THK P = 52.6 kips $P_{ult} =$ (3) #5 Longitudinal 72.8 kips OTM = 136.28 ft-kips $OTM_{ult} = 208.97 \text{ ft-kips}$ #5 @ 14 Transverse e = 2.59 feet X bar = N/A feet Soil Pr. = 2.51 ksf, max., 3.48 ksf, ult. Required Width = 1.61 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 52.6 kips $P_{ULT} =$ 72.8 kips $OTM_{ULT} = 345.67 \text{ ft-kips}$ OTM = 221.7 ft-kips 4.22 feet X bar = 4.24 feet e = Soil Pr. = 3.48 ksf, max., 4.81 ksf, ult. Required Width = 1.68 feet EQ'N 16-16: 0.6DL + 0.7E P = 17.0 kips P(ult) =20.4 kips OTM = 127.5 ft-kips $OTM_{ULT} = 143.93 \text{ ft-kips}$ 7.49 feet X bar = 0.97 feet e = Soil Pr. = 4.91 ksf, max., 5.90 ksf, ult. Required Width = 2.37 feet Factor of Safety = Resisting Moment = 240.19 ft-kips 2.57 FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 16 inches 5.24 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 160psi Fv(allow)= 71 psi Shear = 0.00 kips/ft fv(act.)= 0 psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 14 inches Moment = 4.16 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 173psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 12 inches Longitudinal Steel Required = 0.14 sq.in./ft. v(longit.) =17 psi Transverse Steel Required = 0.11 v(transv.)= 8 sq.in./ft. psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: May-17 (602) 946-8171 checked by: date:

project no.

SHEAR WALL FOOTING DESIGN **INPUT DATA:** Unit 130 North Wall Allow. Soil Pr. = DL OTM = 3.700 ksf 22.45 ft-kips 60 ksi FLR LL OTM = 1.7 ft-kips Fy = f 'c = RF LL OTM = 3000 psi 148.52 ft-kips Wall DL = 0.32 klf SEISMIC OTM = 135.53 ft-kips Roof LL = Footing Length: 16.83 2.15 klf feet Floor LL = Footing Width: 0.03 klf 2.90 feet Footing Thkness: Wall Length = 14.83 feet 12 inches Wall Thickness = 8 inches Footing DL: 1.692 klf OUTPUT DATA: EQ'N 16-11: DL + .75(FL + RL): USE 3'-0" x 12" THK P = 57.4 kips $P_{ult} =$ (3) #5 Longitudinal 78.5 kips OTM = 135.12 ft-kips $OTM_{ult} = 207.20 \text{ ft-kips}$ #5 @ 14 Transverse e = 2.35 feet X bar = N/A feet Soil Pr. = 2.16 ksf, max., 2.96 ksf, ult. Required Width = 1.69 feet EQ'N 16-14: DL + .75(FL + RL + .7E) P = 57.4 kips $P_{ULT} =$ 78.5 kips $OTM_{ULT} = 369.84 \text{ ft-kips}$ OTM = 236.8 ft-kips 4.13 feet X bar = 4.29 feet e = Soil Pr. = 3.08 ksf, max., 4.21 ksf, ult. Required Width = 1.81 feet EQ'N 16-16: 0.6DL + 0.7E P = 19.9 kips P(ult) =23.9 kips OTM = 149.0 ft-kips $OTM_{ULT} = 167.96 \text{ ft-kips}$ 7.49 feet X bar = 0.93 feet e = Soil Pr. = 4.93 ksf, max., 5.91 ksf, ult. Required Width = 2.90 feet Factor of Safety = 2.58 Resisting Moment = 279.17 ft-kips FOOTING REINFORCING: LONGITUDINAL DIRECTION: Reg'd Unreinf Thickness = 16 inches 5.26 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 161psi Fv(allow)= 71 psi Shear = 0.00 kips/ft fv(act.)= 0 psi TRANSVERSE DIRECTION: Rea'd Unreinf Thickness = 18 inches Moment = 6.20 ft-kips/ft Fb(allow)= 178 psi fb(act.) = 145psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi Reinf. Thickness (if used) = 12 inches Longitudinal Steel Required = 0.14 sq.in./ft. v(longit.) =17 psi Transverse Steel Required = v(transv.)= 0.17 sq.in./ft. 24 psi V(allow) = 93.1 psi

rudow + berry

project name: Powdercat - CCW - Revisions

project no. 17100

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

SHEAR WALL FOOTING DESIGN

INPUT DATA: Unit 124 West

Allow. Soil Pr. = DL OTM = 3.700 ksf 198.04 ft-kips FLR LL OTM = Fy = 60 ksi 119.56 ft-kips f 'c = RF LL OTM = 3000 psi 1211.87 ft-kips Wall DL = 0.90 klf SEISMIC OTM = 282.38 ft-kips Roof LL = Footing Length: 55.75 feet 4.53 klf Floor LL = Footing Width: 0.38 klf 2.48 feet Footing Thkness: Wall Length = 53.25 feet 12 inches

Wall Thickness = 10 inches Footing DL: klf 1.271

OUTPUT DATA :

EQ'N 16-11: DL + FL:

P = 360.1 kips $P_{ult} = 528.7 \text{ kips}$ 1409.9 ft-kips OTM = $OTM_{ult} = 2176.6 \text{ ft-kips}$ e = 3.91 feet X bar = N/A feet

Soil Pr. = 3.70 ksf, max., 5.44 ksf, ult.

EQ'N 16-14: DL + .75(FL + RL + .7E)

P = 314.9 kips $P_{ULT} = 456.4 \text{ kips}$ $OTM_{ULT} = 2174.2 \text{ ft-kips}$ OTM = 1408.4 ft-kips 4.47 feet X bar = N/A feet e =

Soil Pr. = 3.37 ksf, max., 4.89 ksf, ult.

EQ'N 16-16: 0.6DL + 0.7E

P = 71.2 kips P(ult) =85.5 kips OTM = 401.2 ft-kips $OTM_{ULT} = 458.85 \text{ ft-kips}$ 5.63 feet X bar = N/A feet e =

Soil Pr. = 0.83 ksf, max., 0.99 ksf, ult.

Resisting Moment = 3309.04 ft-kips

Required Width = 0.42 feet

Factor of Safety = 10.46

USE 2'-6" x 12" THK

(3) #5 Longitudinal

#5 @ 14 Transverse

Required Width = 2.48 feet

Required Width = 1.70 feet

FOOTING REINFORCING:

LONGITUDINAL DIRECTION:

Reg'd Unreinf Thickness = 18 inches

6.78 ft-kips/ft Moment = Fb(allow)= 178 psi fb(act.) = 159psi Fv(allow)= 71 psi Shear = 0.00 kips/ft fv(act.)= 0 psi

TRANSVERSE DIRECTION:

Rea'd Unreinf Thickness = 14 inches

Moment = 3.58 ft-kips/ft Fb(allow)= 178 psi fb(act.)= 149 psi Shear = 0.00 kips/ft Fv(allow)= 71 psi fv(act.)= 0 psi

Reinf. Thickness (if used) = 12 inches Longitudinal Steel Required = 0.18

sq.in./ft. v(longit.) =29 psi Transverse Steel Required = 0.09 v(transv.)= sq.in./ft. 6 psi V(allow) = 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OTING DESIG	iN	
INPUT DATA :	Unit 124E	7/125W Lower Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f'c = 3000 psi Wall DL = 1.31 klf Roof LL = 4.29 klf Floor LL = 0.69 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	83.47 ft-kips 58.81 ft-kips 356.71 ft-kips 224.74 ft-kips 25.00 feet 2.45 feet 12 inches 0.686 klf	
EQ'N 16-11: DL + .75(FL + RL P = 131.8 kips OTM = 395.11 ft-kips e = 3.00 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	•		USE 2'-6" x 12" To (3) #5 Longitudin	al
·	$\begin{aligned} &P_{ULT} = \\ &OTM_{ULT} = \\ &X \ bar = \\ &6.36 \end{aligned}$ $&P \ (ult) = \\ &OTM_{ULT} = \end{aligned}$	8.22 feet ksf, ult. 33.8 kips 311.81 ft-kips		Required Width =	2.17 feet
e = 9.77 feet Soil Pr. = 2.80 ksf, max.,	X bar = 3.36	2.73 feet ksf, ult.		Required Width =	1.40 feet
Resisting Moment = 586.01	•	I		Factor of Safety =	2.83
FOOTING REINFORCING LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 6.63 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	155 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 2.38 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	143 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.18 0.06	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 0 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL F	OOTING DES	SIGN	
INPUT DATA :	Unit 124E	E/125W Upper V	Vall		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f'c = 3000 psi Wall DL = 1.56 klf Roof LL = 6.62 klf Floor LL = 0.86 klf Wall Length = 24.67 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM Footing Length Footing Width: Footing Thknes Footing DL:	281.34 ft-kips = 160.1 ft-kips : 27.00 feet 3.17 feet	
EQ'N 16-11: DL + .75(FL + RL P = 232.3 kips OTM = 378.72 ft-kips e = 1.63 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar = 5.32$	•		USE 3'-2" x 12" The (3) #5 Longitudin #5 @ 14 Transver	al ·se
EQ'N 16-14: DL + .75(FL + RL + P = 232.3 kips OTM = 498.8 ft-kips e = 2.15 feet Soil Pr. = 4.01 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	785.64 ft-kips		Required Width =	2.58 feet
EQ'N 16-16: 0.6DL + 0.7E P = 56.3 kips OTM = 178.7 ft-kips e = 3.17 feet Soil Pr. = 1.12 ksf, max., Resisting Moment = 1267.32 FOOTING REINFORCING	OTM _{ULT} = X bar = 1.35 ft-kips	201.69 ft-kips		Required Width = Factor of Safety =	
LONGITUDINAL DIRECTION:	J				
Req'd Unreinf Thickness = Moment = 6.40 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= Fv(allow)=	•	fb(act.)= fv(act.)=	150 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 4.37 ft-kips/ft Shear = 0.00 kips/ft	16	inches Fb(allow)= 1 Fv(allow)=	•	fb(act.)= fv(act.)=	134 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.17 0.12	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 12 psi 93.1 psi
				page	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OTING DESIG	N	
INPUT DATA :	Unit 125E	7/126W Lower Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.37 klf Roof LL = 3.07 klf Floor LL = 0.95 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	98.61 ft-kips 85.3 ft-kips 331.39 ft-kips 227.7 ft-kips 25.00 feet 2.32 feet 12 inches 0.653 klf	
EQ'N 16-11: DL + .75(FL + RL P = 116.1 kips OTM = 411.13 ft-kips e = 3.54 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	166.8 kips 618.36 ft-kips N/A feet ksf, ult.	[USE 2'-6" x 12" To (3) #5 Longitudin	al
EQ'N 16-14: DL + .75(FL + RL + P = 116.1 kips OTM = 581.9 ft-kips e = 5.01 feet Soil Pr. = 4.46 ksf, max., EQ'N 16-16: 0.6DL + 0.7E P = 28.5 kips OTM = 286.9 ft-kips	+ .7E) P _{ULT} = OTM _{ULT} = X bar = 6.40 P (ult) = OTM _{ULT} =	7.49 feet ksf, ult. 34.2 kips 326.02 ft-kips		Required Width =	
e = 10.07 feet Soil Pr. = 3.37 ksf, max.,	X bar = 4.05	2.43 feet ksf, ult.		Required Width =	1.59 feet
Resisting Moment = 593.24	<u> </u>	ı		Factor of Safety =	2.71
FOOTING REINFORCING LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 6.66 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	156 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 2.04 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	123 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.18 0.05	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 0 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OTING DESIG	N	
INPUT DATA :	Unit 125E	7/126W Upper Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.49 klf Roof LL = 6.47 klf Floor LL = 0.75 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	35.60 ft-kips 102.1 ft-kips 334.58 ft-kips 155.66 ft-kips 25.75 feet 3.08 feet 12 inches 2.003 klf	
EQ'N 16-11: DL + .75(FL + RL P = 208.8 kips OTM = 363.11 ft-kips e = 1.74 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar = 5.31$	•		USE 3'-2" x 12" TI (3) #5 Longitudin #5 @ 14 Transver Required Width =	al rse
EQ'N 16-14: DL + .75(FL + RL + P = 208.8 kips OTM = 479.9 ft-kips e = 2.30 feet Soil Pr. = 4.04 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	299.9 kips 753.53 ft-kips N/A feet ksf, ult.		Required Width =	2.53 feet
e = 3.45 feet Soil Pr. = 1.17 ksf, max., Resisting Moment = 1101.52	$OTM_{ULT} = X bar = 1.40$ ft-kips	199.97 ft-kips		Required Width = Factor of Safety =	
FOOTING REINFORCING	j:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 9.61 ft-kips/ft Shear = 0.00 kips/ft	22	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	144 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 4.04 ft-kips/ft Shear = 0.00 kips/ft	14	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	168 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.26 0.11	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	45 psi 9 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	R WALL FO	OTING DESIG	GN	
INPUT DATA :	Unit 126	East (EQ OTM to I	North)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10 OUTPUT DATA:	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length : Footing Width : Footing Thkness: Footing DL :		
EQ'N 16-11 : DL + FL: P = 179.3 kips OTM = -318.2 ft-kips e = -1.77 feet Soil Pr. = 3.70 ksf, max.,	$ OTM_{ult} = X bar = 5.41 $	•		USE 1'-8" x 12" To (Min. per Geotech Root) #5 Longitudin Required Width =	eport) al
EQ'N 16-14: DL + .75(FL + RL P = 161.0 kips OTM = -47.8 ft-kips e = -0.30 feet Soil Pr. = 4.20 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	•		Required Width =	0.71 feet
EQ'N 16-16: 0.6DL + 0.7E P = 37.0 kips OTM = 326.8 ft-kips e = 8.83 feet Soil Pr. = 2.23 ksf, max., Resisting Moment = 1367.33	OTM _{ULT} = X bar = 2.68	•		Required Width = Factor of Safety =	
FOOTING REINFORCING	G :				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 0.75 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	45 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.33 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	20 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.02 0.01	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi
				nane	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	R WALL FO	OTING DESIG	3N	
INPUT DATA :	Unit 126	East (EQ OTM to	South)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length : Footing Width : Footing Thkness: Footing DL :	-222.10 ft-kips 13.16 ft-kips 540.32 ft-kips 193.57 ft-kips 44.83 feet 1.38 feet 12 inches 0.390 klf	
EQ'N 16-11 : DL + FL: P = 185.7 kips OTM = 318.2 ft-kips e = 1.71 feet Soil Pr. = 3.69 ksf, max.,	$OTM_{ult} = X bar =$	269.9 kips 598.0 ft-kips N/A feet ksf, ult.		USE 1'-8" x 12" TI (Min. per Geotech Ro (2) #5 Longitudin Required Width =	eport) al
EQ'N 16-14: DL + .75(FL + RL P = 167.5 kips OTM = 338.2 ft-kips e = 2.02 feet Soil Pr. = 3.44 ksf, max., EQ'N 16-16: 0.6DL + 0.7E P = 40.9 kips	$P_{ULT} = OTM_{ULT} = X bar = 4.94$	629.94 ft-kips N/A feet ksf, ult.		Required Width =	0.96 feet
OTM = 60.3 ft-kips e = 1.48 feet Soil Pr. = 0.79 ksf, max., Resisting Moment = 1527.03	$ OTM_{ULT} = X bar = 0.95 $ $ ft-kips$	56.886 ft-kips		Required Width = Factor of Safety =	0.22 feet 682
FOOTING REINFORCIN	G:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 1.50 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	90 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.98 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	59 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.04 0.03	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

SHEAR WALL FOOTING DESIGN					
INPUT DATA :	Unit 127	West (EQ OTM to	North)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10 OUTPUT DATA:	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length : Footing Width : Footing Thkness: Footing DL :		
EQ'N 16-11 : DL + FL: P = 179.0 kips OTM = -309.7 ft-kips e = -1.73 feet Soil Pr. = 3.70 ksf, max.,	$ OTM_{ult} = X bar = 5.41 $	•		USE 1'-8" x 12" TI (Min. per Geotech Ro (2) #5 Longitudin Required Width =	eport) al
EQ'N 16-14: DL + .75(FL + RL P = 160.8 kips OTM = -46.5 ft-kips e = -0.29 feet Soil Pr. = 4.15 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	•		Required Width =	0.70 feet
EQ'N 16-16: 0.6DL + 0.7E P = 37.0 kips OTM = 320.5 ft-kips e = 8.66 feet Soil Pr. = 2.16 ksf, max., Resisting Moment = 1382.59	$OTM_{ULT} = X bar = 2.59$ ft-kips	•		Required Width = Factor of Safety =	
FOOTING REINFORCING	3:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 1.68 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	101 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.33 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	20 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.04 0.01	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi
				nane	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL F	OOTING DESIG	GN	
INPUT DATA :	Unit 127	West (EQ OTM	to South)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	186.4 ft-kips 44.83 feet 1.37 feet	
EQ'N 16-11 : DL + FL: P = 185.2 kips OTM = 309.7 ft-kips e = 1.67 feet Soil Pr. = 3.69 ksf, max.,	OTM _{ult} = X bar =	584.9 ft-kips		USE 1'-8" x 12" T (Min. per Geotech R (2) #5 Longitudin Required Width =	eport) ial
Soil Pr. = 3.43 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	•		Required Width =	0.95 feet
EQ'N 16-16: 0.6DL + 0.7E P = 40.7 kips OTM = 52.3 ft-kips e = 1.28 feet Soil Pr. = 0.78 ksf, max.,	$OTM_{ULT} = X bar =$	48.9 kips 47.87 ft-kips N/A feet ksf, ult.		Required Width =	0.22 feet
Resisting Moment = 1521.50	ft-kips			Factor of Safety =	5.75
FOOTING REINFORCING	G:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 1.50 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)=	•	fb(act.)= fv(act.)=	90 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.97 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)=	•	fb(act.)= fv(act.)=	58 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.04 0.03	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OTING DESIG	iN	
INPUT DATA :	Unit 127E	7/128W Lower Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.37 klf Roof LL = 3.07 klf Floor LL = 0.95 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	252.78 ft-kips 25.00 feet 2.38 feet 12 inches	
EQ'N 16-11: DL + .75(FL + RI P = 116.5 kips OTM = 411.45 ft-kips e = 3.53 feet Soil Pr. = 3.62 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	N/A feet		USE 2'-6" x 12" T (3) #5 Longitudin Required Width =	al
EQ'N 16-14: DL + .75(FL + RL P = 116.5 kips OTM = 601.0 ft-kips e = 5.16 feet Soil Pr. = 4.45 ksf, max., EQ'N 16-16: 0.6DL + 0.7E P = 28.7 kips OTM = 312.1 ft-kips e = 10.86 feet	+ .7E) $P_{ULT} = $ $OTM_{ULT} = $ $X \text{ bar} = $ 6.38 $P \text{ (ult)} = $ $OTM_{ULT} = $	167.3 kips 922.08 ft-kips 7.34 feet ksf, ult. 34.5 kips 354.34 ft-kips		Required Width =	
Soil Pr. = 4.92 ksf, max., Resisting Moment = 598.61	5.90			Required Width = Factor of Safety =	
FOOTING REINFORCING	3 :				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 6.64 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	156 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 2.19 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	131 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.18 0.06	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 0 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	R WALL FO	OTING DESIG	SN	
INPUT DATA :	Unit 127E	E/128W Upper Wa	all		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.51 klf Roof LL = 6.58 klf Floor LL = 0.75 klf Wall Length = 22.75 Wall Thickness = 16	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	33.38 ft-kips 95.37 ft-kips 315.05 ft-kips 152.81 ft-kips 25.75 feet 3.04 feet 12 inches 1.980 klf	
EQ'N 16-11: DL + .75(FL + R P = 210.4 kips OTM = 341.20 ft-kips e = 1.62 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = $ $OTM_{ult} = $ $X bar = $ 5.32	•		USE 3'-2" x 12" TI (3) #5 Longitudin #5 @ 14 Transver Required Width =	al rse
EQ'N 16-14: DL + .75(FL + RL P = 210.4 kips OTM = 455.8 ft-kips e = 2.17 feet Soil Pr. = 4.04 ksf, max., EQ'N 16-16: 0.6DL + 0.7E	$P_{ULT} = OTM_{ULT} = X bar =$	715.93 ft-kips		Required Width =	2.50 feet
P = 51.2 kips OTM = 172.8 ft-kips e = 3.38 feet Soil Pr. = 1.17 ksf, max., Resisting Moment = 1098.60	$ OTM_{ULT} = X bar = 1.40 $ ft-kips	195.18 ft-kips		Required Width = Factor of Safety =	
FOOTING REINFORCING	G:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 9.63 ft-kips/ft Shear = 0.00 kips/ft	22	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	144 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 3.92 ft-kips/ft Shear = 0.00 kips/ft	14	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	163 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.26 0.10	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	45 psi 8 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

SHEAR WALL FOOTING DESIGN					
INPUT DATA :	Unit 128E	7/129W Lower Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f'c = 3000 psi Wall DL = 1.51 klf Roof LL = 4.92 klf Floor LL = 0.87 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	78.88 ft-kips 55.59 ft-kips 315.64 ft-kips 254.43 ft-kips 25.00 feet 2.56 feet 12 inches 0.714 klf	
EQ'N 16-11: DL + .75(FL + RL P = 151.1 kips OTM = 357.30 ft-kips e = 2.36 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar = 5.41$	•		USE 2'-6" x 12" To (Delta = 2.4% - O (3) #5 Longitudin Required Width =	K) al
EQ'N 16-14: DL + .75(FL + RL + P = 151.1 kips OTM = 548.1 ft-kips e = 3.63 feet Soil Pr. = 4.42 ksf, max., EQ'N 16-16: 0.6DL + 0.7E	$P_{ULT} = $ $OTM_{ULT} = $ $X bar = $ 6.45	N/A feet ksf, ult.		Required Width =	2.30 feet
P = 31.4 kips OTM = 301.8 ft-kips e = 9.62 feet Soil Pr. = 2.83 ksf, max., Resisting Moment = 653.68 FOOTING REINFORCING	$OTM_{ULT} = X bar = 3.40$ ft-kips	341.76 ft-kips		Required Width = Factor of Safety =	
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 6.76 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	159 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 2.77 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	166 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.18 0.07	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 0 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	R WALL FO	OTING DESIG	iN	
INPUT DATA :	Unit 128E	E/129W Upper Wa	III		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.45 klf Roof LL = 5.94 klf Floor LL = 0.75 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	171.79 ft-kips 140.17 ft-kips 25.75 feet 2.78 feet	
EQ'N 16-11: DL + .75(FL + R P = 194.4 kips OTM = 300.97 ft-kips e = 1.55 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	•		USE 3'-0" x 12" To (3) #5 Longitudin #5 @ 14 Transver	al rse
EQ'N 16-14: DL + .75(FL + RL P = 194.4 kips OTM = 406.1 ft-kips e = 2.09 feet Soil Pr. = 4.04 ksf, max., EQ'N 16-16: 0.6DL + 0.7E	$P_{ULT} = OTM_{ULT} = X bar =$	641.71 ft-kips		Required Width =	2.28 feet
P = 48.1 kips OTM = 152.2 ft-kips e = 3.16 feet Soil Pr. = 1.17 ksf, max., Resisting Moment = 1032.42	$OTM_{ULT} = X bar = 1.40$	171.48 ft-kips		Required Width = Factor of Safety =	
FOOTING REINFORCING	G:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 9.60 ft-kips/ft Shear = 0.00 kips/ft	20	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	178 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 3.10 ft-kips/ft Shear = 0.00 kips/ft	14	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	129 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.26 0.08	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	45 psi 1 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

SHEAR WALL FOOTING DESIGN					
INPUT DATA :	Unit 129E	/130W Lower Wa	II		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.37 klf Roof LL = 3.07 klf Floor LL = 0.95 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	2.39 feet	
EQ'N 16-11: DL + .75(FL + RL P = 122.5 kips OTM = 411.61 ft-kips e = 3.36 feet Soil Pr. = 3.70 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	N/A feet		USE 2'-6" x 12" Th (3) #5 Longitudina Required Width =	al
EQ'N 16-14: DL + .75(FL + RL + P = 122.5 kips OTM = 602.4 ft-kips e = 4.92 feet Soil Pr. = 4.51 ksf, max., EQ'N 16-16: 0.6DL + 0.7E P = 32.3 kips OTM = 313.9 ft-kips	+ .7E) P _{ULT} = OTM _{ULT} = X bar = 6.42 P (ult) =	174.4 kips 924.25 ft-kips 7.58 feet ksf, ult. 38.8 kips 356.31 ft-kips		Required Width =	
Soil Pr. = 3.24 ksf, max., Resisting Moment = 673.11	3.88	ksf, ult.		Required Width = Factor of Safety =	
FOOTING REINFORCING	3:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 6.68 ft-kips/ft Shear = 0.00 kips/ft	18	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	157 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 2.23 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	134 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =		inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	26 psi 0 psi 93.1 psi
				nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHEA	AR WALL FO	OOTING DESIG	SN	
INPUT DATA :	Unit 129E	/130W Upper W	/all		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.51 klf Roof LL = 6.58 klf Floor LL = 0.75 klf Wall Length = 22.75 Wall Thickness = 16 OUTPUT DATA:			DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length: Footing Width: Footing Thkness: Footing DL:	153.73 ft-kips 25.75 feet 3.00 feet	
EQ'N 16-11 : DL + .75(FL + RL P = 209.8 kips OTM = 324.51 ft-kips e = 1.55 feet Soil Pr. = 3.69 ksf, max.,	$P_{ult} = OTM_{ult} = X bar =$	•		USE 3'-0" x 12" T (3) #5 Longitudin #5 @ 14 Transve	al rse
EQ'N 16-14: DL + .75(FL + RL P = 209.8 kips OTM = 439.8 ft-kips e = 2.10 feet Soil Pr. = 4.04 ksf, max., EQ'N 16-16: 0.6DL + 0.7E	$P_{ULT} = OTM_{ULT} = X bar =$			Required Width =	2.46 feet
-	$ OTM_{ULT} = X bar = 1.38 $	61.0 kips 184.19 ft-kips N/A feet ksf, ult.		Required Width = Factor of Safety =	
FOOTING REINFORCING	3:				
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 9.63 ft-kips/ft Shear = 0.00 kips/ft	22	inches Fb(allow)= 1 Fv(allow)= 7	•	fb(act.)= fv(act.)=	145 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 3.79 ft-kips/ft Shear = 0.00 kips/ft	14	inches Fb(allow)= 1 Fv(allow)= 7	-	fb(act.)= fv(act.)=	158 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.26 0.10	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	45 psi 7 psi 93.1 psi

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

	SHE	R WALL FO	OTING DESIG	3N	
INPUT DATA :	Unit 130	East (EQ OTM to I	North)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f 'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length : Footing Width : Footing Thkness: Footing DL :	0.83 feet	
EQ'N 16-11 : DL + FL: P = 179.1 kips OTM = -310.7 ft-kips e = -1.73 feet Soil Pr. = 3.70 ksf, max.,	$OTM_{ult} = X bar =$	261.8 kips -586.3 ft-kips N/A feet ksf, ult.		USE 1'-8" x 12" TI (Min. per Geotech Re (2) #5 Longitudin Required Width =	eport) al
EQ'N 16-14: DL + .75(FL + RL P = 160.9 kips OTM = -46.2 ft-kips e = -0.29 feet Soil Pr. = 4.16 ksf, max., EQ'N 16-16: 0.6DL + 0.7E P = 37.0 kips	$P_{ULT} = OTM_{ULT} = X bar = 6.01$	-163.1 ft-kips N/A feet ksf, ult. 44.4 kips		Required Width =	0.70 feet
OTM = 321.7 ft-kips e = 8.69 feet Soil Pr. = 2.17 ksf, max., Resisting Moment = 1383.57 FOOTING REINFORCING	X bar = 2.60 ft-kips	371.03 ft-kips 13.73 feet ksf, ult.		Required Width = Factor of Safety =	
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 1.68 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	-	fb(act.)= fv(act.)=	101 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.33 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	20 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.04 0.01	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi
·			·	nage	

structural engineering

scottsdale, arizona designed by: MAR date: 2/24/18

(602) 946-8171 checked by: date:

SHEAR WALL FOOTING DESIGN					
INPUT DATA :	Unit 130	East (EQ OTM to S	South)		
Allow. Soil Pr. = 3.700 Fy = 60 ksi f'c = 3000 psi Wall DL = 1.15 klf Roof LL = 2.67 klf Floor LL = 0.34 klf Wall Length = 44.00 Wall Thickness = 10 OUTPUT DATA:	feet		DL OTM = FLR LL OTM = RF LL OTM = SEISMIC OTM = Footing Length : Footing Width : Footing Thkness: Footing DL :	-223.02 ft-kips 13.16 ft-kips 533.68 ft-kips 187.91 ft-kips 44.83 feet 1.37 feet 12 inches 0.387 klf	
EQ'N 16-11 : DL + FL: P = 185.3 kips OTM = 310.7 ft-kips e = 1.68 feet Soil Pr. = 3.69 ksf, max.,	OTM _{ult} = X bar = 5.37	269.3 kips 586.3 ft-kips N/A feet ksf, ult.		USE 1'-8" x 12" To (Min. per Geotech Ro (2) #5 Longitudin Required Width =	eport) al
OTM = 328.0 ft-kips e = 1.96 feet Soil Pr. = 3.43 ksf, max.,	$P_{ULT} = OTM_{ULT} = X bar =$	240.1 kips 614.08 ft-kips N/A feet ksf, ult.		Required Width =	0.96 feet
e = 1.33 feet Soil Pr. = 0.78 ksf, max., Resisting Moment = 1522.48	$OTM_{ULT} = X bar = 0.94$	49.885 ft-kips		Required Width = Factor of Safety =	0.22 feet 669
FOOTING REINFORCING					
LONGITUDINAL DIRECTION: Req'd Unreinf Thickness = Moment = 1.50 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	90 psi 0 psi
TRANSVERSE DIRECTION: Req'd Unreinf Thickness = Moment = 0.97 ft-kips/ft Shear = 0.00 kips/ft	12	inches Fb(allow)= 178 Fv(allow)= 71	•	fb(act.)= fv(act.)=	58 psi 0 psi
Reinf. Thickness (if used) = Longitudinal Steel Required = Transverse Steel Required =	12 0.04 0.03	inches sq.in./ft. sq.in./ft.		v(longit.) = v(transv.)= V(allow) =	0 psi 0 psi 93.1 psi
				nage	

Project Title: Engineer: Project Descr: **Powdercat** MAR

Project ID: 16126

Printed: 26 FEB 2018, 10:20AM

Cantilevered Retaining Wall

Lic. #: KW-06002357

File = C:_jobs\17100C~1\ENG\LATERA~1\SPREAD~1\RETAIN~1\POWDER~1.EC6 ENERCALC, INC. 1983-2017, Build:10.17.12.10, Ver:10.17.12.10 Licensee : RUDOW & BERRY

Description : Breezeway Ret. Wall w/ Bas	ement Slab in place - Revised	
Criteria	Soil Data	Calculations per ACI 318-14, ACI 530-11, IBC 2015,
Retained Height = 9.58 ft	Allow Soil Bearing = 3,700.0 psf	CBC 2016, ASCE 7-10
Wall height above soil = 0.33 ft	Equivalent Fluid Pressure Method	
Slope Behind Wall = 0.00 : 1	Heel Active Pressure = 35.0 psf/f	t
Height of Soil over Toe = 12.00 in	Toe Active Pressure = 35.0 psf/f	t
Water height over heel = 0.0 ft	Passive Pressure = 320.0 psf/f	t
Vertical component of active Lateral soil pressure options: NOT USED for Soil Pressure.	Soil Density, Heel = 106.00 pcf Soil Density, Toe = 106.00 pcf Friction Coeff btwn Ftg & Soil = 0.000	
NOT USED for Sliding Resistance. NOT USED for Overturning Resistance	Soil height to ignore for passive pressure = 0.00 in	
Surcharge Loads	Lateral Load Applied to Stem	Adjacent Footing Load

5 a . 5 a . g 5		_
Curoborgo	Our	امماا

Surcharge Over Heel = 100.0 pst Used To Resist Sliding & Overturning Over The = 0.0 psf Surcharge Over Toe = Used for Sliding & Overturning

Axial Load Applied to Stem

975.0 lbs Axial Dead Load Axial Live Load
Axial Load Eccentricity 3,820.0 lbs 0.0 in

Design Summary

Live Load

Earth, H

Wind, W

Seismic, E

Wall Stability Ratios Overturning Sliding Slab Resists All Sliding	= = y!		1.64 0.29	Ök	
Total Bearing Loadresultant ecc.	=		7,730 2.86		
Soil Pressure @ Toe Soil Pressure @ Heel Allowable	= = = Tb		1,104 1,988 3,700	psf	
Soil Pressure Less	Inar	1 Allo			
ACI Factored @ Toe	=		1,543		
ACI Factored @ Heel	=		2,778	psf	
Footing Shear @ Toe	=		45.2	psi	OK
Footing Shear @ Heel	=			psi	
Allowable	=		82.2		0
Sliding Calcs Slab Resist	ts Al	l Sli	ding!		
Lateral Sliding Force	=		2,238.2	lbs	
less 100% Passive Force	=	_	640.0		
less 100% Friction Force	=	-	0.0	lbs	
Added Force Reg'd	=		1,598.2	lbs	NG
for 1.5 : 1 Stability	=		2,717.3	lbs	NG
Load Factors ———					
Dead Load			1.20	0	

1.600

1.600

1.600

1.000

Height to Top =	
-----------------	--

Lateral Load 0.0 plf 0.00 ft ...Height to Bottom 0.00 ft

Wind on Exposed Stem 0.0 psf

| Adjacent Footing Load

Adjacent Footing Load 0.0 lbs Footing Width 0.00 ft Eccentricity 0.00 in Wall to Ftg CL Dist 0.00 ft Footing Type Line Load Base Above/Below Soil 0.0 ft at Back of Wall Poisson's Ratio 0.300

Stem Construction] _	Top Stem	
Design Height Above Ftg	ft =	Stem OK 0.00	
Wall Material Above "Ht"	=	Concrete	
Thickness	in =	10.00	
Rebar Size	=	# 5	
Rebar Spacing	in =	10.00	
Rebar Placed at	=	User Spec	
Design Data ————		0.021	
fb/FB + fa/Fa	=	0.821	
Total Force @ Section	lbs =	3,047.9	
MomentActual	ft-l =	10,621.0	
MomentAllowable	ft-l =	12,932.7	
ShearActual	psi =	31.7	
ShearAllowable	psi =	94.9	
Wall Weight	psf =	125.0	
Rebar Depth 'd'	in =	8.00	
Lap splice if above	in =	18.50	
Lap splice if below	in =	7.82	
Hook embed into footing	in =	7.82	
Concrete Data —			
f'c	psi =	4,000.0	
Fy	psi =		

rudow + berry, inc. 4021 north 75th street, #101 scottsdale, arizona 85251 480.946.8171

Project Title: Engineer: Project Descr: **Powdercat** MAR

Project ID: 16126

Printed: 26 FEB 2018, 10:20AM

Cantilevered Retaining Wall

File = C:_jobs\17100C~1\ENG\LATERA~1\SPREAD~1\RETAIN~1\POWDER~1.EC6 ENERCALC, INC. 1983-2017, Build:10.17.12.10, Ver:10.17.12.10

Licensee: RUDOW & BERRY

Lic. # : KW-06002357

Breezeway Ret. Wall w/ Basement Slab in place - Revised Description:

Footing	Dimensions	&	Strengths
---------	-------------------	---	-----------

Toe Width	= 3.67 ft	
Heel Width	= 1.33	
Total Footing Width	= 5.00	
Footing Thickness	= 12.00 in	
Key Width	= 0.00 in	
Key Depth	= 0.00 in	
Key Distance from Toe	= 0.00 ft	
f'c = 3,000 psi	Fy = 60,000 psi = 150.00 pcf	
Footing Concrete Density	= 150.00 pcf	
Min. As %	= 0.0018	
Cover @ Top 3.00	@ Btm.= 3.00	in

Footing Design Results

		<u>Toe</u>	<u>Heel</u>
Factored Pressure	=	1,543	2,778 psf
Mu': Upward	=	12,406	407 ft-lb
Mu' : Downward	=	2,065	195 ft-lb
Mu: Design	=	10,340	212 ft-lb
Actual 1-Way Shear	=	45.22	5.67 psi
Allow 1-Way Shear	=	82.16	82.16 psi
Toe Reinforcing	=	# 5 @ 10.00 in	
Heel Reinforcing	=	None Spec'd	
Key Reinforcing	=	# 5 @ 16.00 in	

Other Acceptable Sizes & Spacings

Toe: #4@ 7.25 in, #5@ 11.00 in, #6@ 15.75 in, #7@ 21.25 in, #8@ 28.00 in, #9@ 35

Heel: Not req'd, Mu < S * Fr Key: No key defined

Summary of Overturning & Resisting Forces & Moments

		0	VERTURN					RI	ESISTING	
Item		Force lbs	Distance ft	9	Moment ft-lb			Force lbs	Distance ft	Moment ft-lb
Heel Active Pressure	=	1,958.9	3.53	}	6,908.3	Soil Over Heel	=	507.4	4.75	2,410.2
Surcharge over Heel	=	349.3	5.29)	1,848.0	Sloped Soil Over Heel	=			
Toe Active Pressure	=	-70.0	0.67	1	-46.7	Surcharge Over Heel	=	50.0	4.75	237.3
Surcharge Over Toe	=					Adjacent Footing Load	=			
Adjacent Footing Load	=					Axial Dead Load on Stem	=	975.0	4.08	3,981.6
Added Lateral Load	=					* Axial Live Load on Stem	=	3,820.0	4.08	15,599.6
Load @ Stem Above Soil	=					Soil Over Toe	=	388.7	1.83	712.7
						Surcharge Over Toe	=			
						Stem Weight(s)	=	1,238.8	4.08	5,058.6
						Earth @ Stem Transitions	=			
Total	=	2,238.2	O.T.M.	=	8,709.7	Footing Weight	=	750.0	2.50	1,875.0
Resisting/Overturning	Ratio		=	1	.64	Key Weight	=			
Vertical Loads used	for S	oil Pressure	= 7	729.8	lbs	Vert. Component	=		_	
						Tota	al =	3,909.8 I	bs R.M. =	14,275.5

^{*} Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

rudow + berry job name: **CCW Powdercat** pg structural engineering scottsdale, arizona 85251 job number: 17100 designed by: t (480) 946-8171 MAR date: 2/18 f (480) 946-9480 checked by: date: APPENDIX: Geotechnical Report Revisions



January 30, 2018

Powder Cat Townhomes, LLC c/o Mr. David Orr 11180 Sunrise Valley Drive, #300 Reston, VA 20191

IGES Project No. 02579-001

Subject: Supplemental Subsurface Assessment

Copper Crest West Townhomes Summit Powder Mountain Resort

Weber County, Utah

Reference: IGES, Inc., 2017a, Geotechnical and Geologic Hazard Investigation, Copper Crest

West, Summit Powder Mountain Resort, Weber County, Utah, Project No. 01628-

022, dated January 16, 2017

Mr. Orr:

As requested, IGES has conducted a supplemental subsurface assessment to further evaluate subsurface conditions for the remaining units of the Copper Crest West Townhomes. The purpose of our work is to further quantify the elevation of various geologic units within the footprint of the townhomes, provide data with which the Client can more accurately estimate quantities with respect to over-excavation, and to provide supplemental recommendations for foundations, as warranted by the new data. The following letter provides a summary of our findings, conclusions, and recommendations.

Method of Study

On January 9, 2018, Mr. Peter Doumit, P.G. and Mr. David Glass, P.E., of IGES visited the site to assess further assess the subsurface conditions at the site. At the time of our visit IGES met with Mr. Tyler Orr, the Client's representative. Also on site was Mr. Greg Chambers, the excavator subcontracting for the Client. Several test pit locations had been surveyed and located with stakes by the project surveyor; elevation control was also provided.

At, or approximately near the pre-determined locations, test pits were excavated down to bedrock (Wasatch Formation). Utilizing a survey rod and known elevation points, the elevation of various earth strata was recorded, including:

- Contact between undocumented fill and underlying colluvium
- Contact between colluvium and bedrock

Since the presence of utilities precluded the ability to excavate the test pits at all of the exact pre-marked locations, for each test pit the location where the strata elevations were obtained was recorded with a hand-held GPS device.

Findings

The findings are summarized on the test pit logs/fence diagrams, attached. On the diagrams, the elevations of the various strata are recorded. Figure 1, attached, provides a *Geotechnical Map*, illustrating the locations of the test pits. These test pits have been located on the map based on GPS units and comparison with a Google Earth image – the project civil engineer should verify the accuracy of test pit location. It should be noted that the data obtained from Test Pit 4 was inconclusive, since this area appears to expose mostly fill from a utility trench.

To visualize the depth to various strata with respect to the proposed foundations, five cross-sections were prepared, designated A-A' through E-E', shown on Figure 1. Information regarding the elevation of the bottom of footings was evaluated based on Sheets S1.01, S1.02, S1.11, and S1.12 (Foundation Plans), prepared by Studio MA, dated June 1, 2017. The resultant cross-sections are illustrated on Sheet 1, attached. These sections illustrate the locations of footings with respect to the various strata contacts – the ground surface is not shown.

The building footprint is overlain by a few feet of undocumented fill. Underlying the fill, we observed coarse colluvium. This unit was of variable character, grading from clayey gravel to gravel and cobbles with minimal matrix material. For some colluvium, voids could be seen between the cobble-size rocks – this likely represents a buried talus deposit. This material appeared loose, and readily raveled from the test pit walls. Also, topsoil was observed underlying the undocumented fill; the thickness of the topsoil was variable, ranging from negligible to as much as 10 inches locally.

Conclusions and Recommendations

Based on our observations, placing the proposed townhomes on conventional spread footings is feasible. However, at some locations, the depth of undocumented fill underlying proposed foundations is as deep as $3\frac{1}{2}$ feet. In many locations, the foundations are underlain by a sliver of undocumented fill, and only partially penetrate into the underlying colluvium. At the currently proposed footing elevations, IGES does not anticipate the footings will bear directly on bedrock, except perhaps at very localized areas.

In consideration of our findings, IGES recommends the following:

- a) All undocumented fill and topsoil shall be removed from beneath structural elements. Removals shall extend 1 foot horizontally for every foot of depth below the bottom footing elevation.
- b) All foundation elements shall be underlain by a minimum of 2 feet of structural fill. It should be noted that the depth of structural fill may be greater, depending on the required over-excavation to remove deleterious earth materials, upwards of 4 feet in limited areas should be anticipated.
- c) Structural fill (as defined in IGES, 2017) shall consist of a coarse, granular material excavated site material is largely expected to meet this criterion. Material classifying as topsoil is not suitable for use as structural fill; this material, where encountered, should be segregated, and must be kept out of the soil stockpiles to be utilized as structural fill.
- d) In consideration that the entire structure will be supported by a relatively uniform bearing stratum (granular structural fill), the allowable bearing capacity may be

- increased to 3,700 psf. This is for live plus dead loads; the allowable bearing capacity may be increased by 1/3 for transient loads such as wind or seismic.
- e) Prior to placement of structural fill, the exposed subgrade shall be compacted in-place to approximately 92% of the Modified Proctor (ASTM D1557).
- f) An IGES representative should observe the foundation subgrade prior to placement of structural fill to assess removal of deleterious earth materials (undocumented fill, topsoil).

All other recommendations presented in our referenced geotechnical report remain valid and should be implemented into the design and construction of the project, except as superseded herein.

Closure

We appreciate the opportunity to provide you with our services. If you have any questions please contact the undersigned at your convenience (801) 748-4044.

Respectfully Submitted,

IGES, Inc.

David A. Glass, P.E.

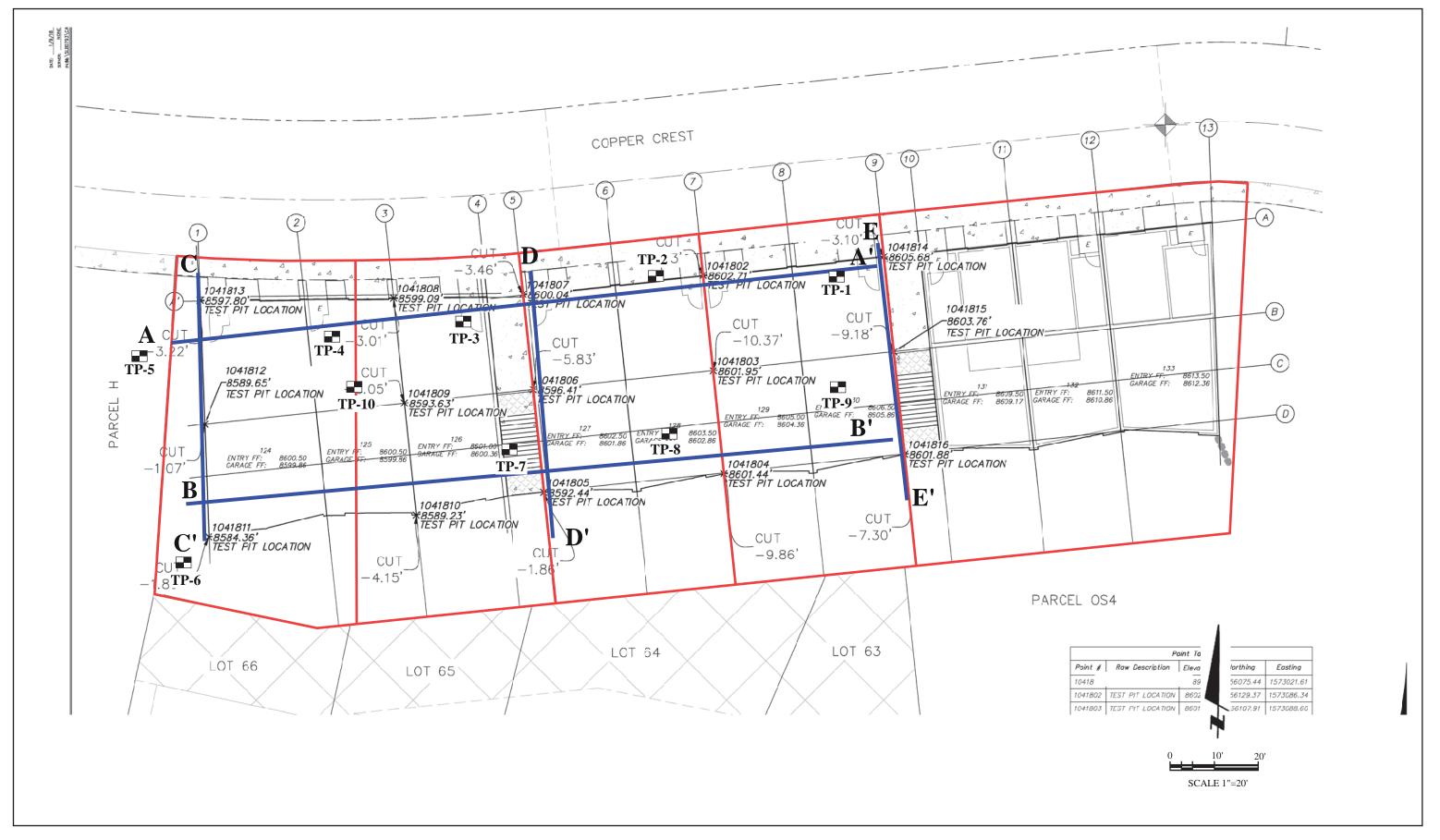
Senior Geotechnical Engineer

No. 6370734 DAVID A.

Attachment:

Figure 1 – Geotechnical Map Test Pit Logs/Fence Diagram

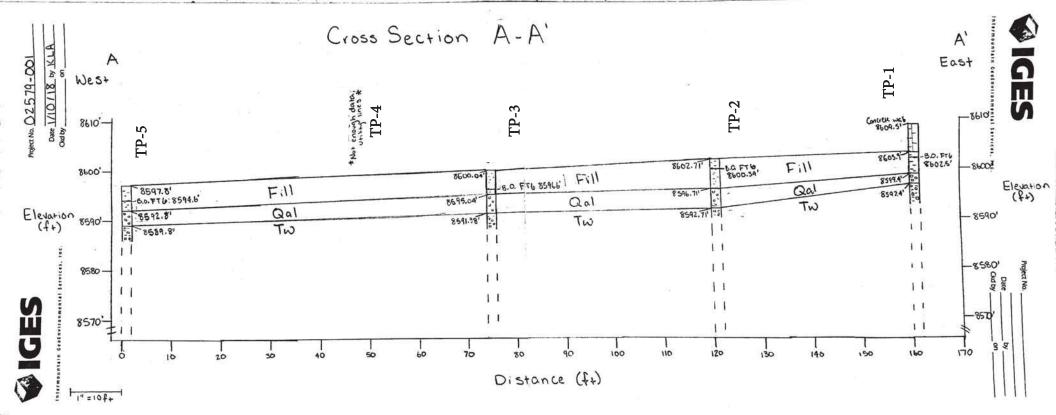
Sheet 1 – Geotechnical Cross-Sections

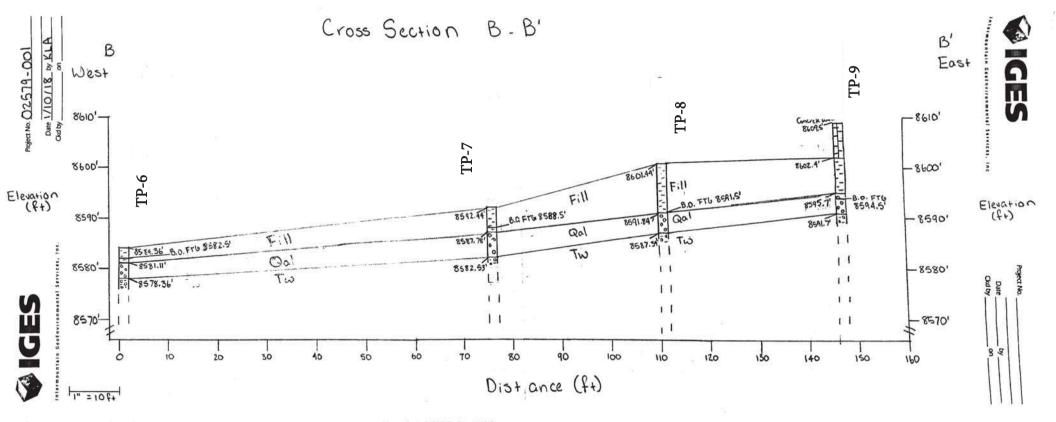


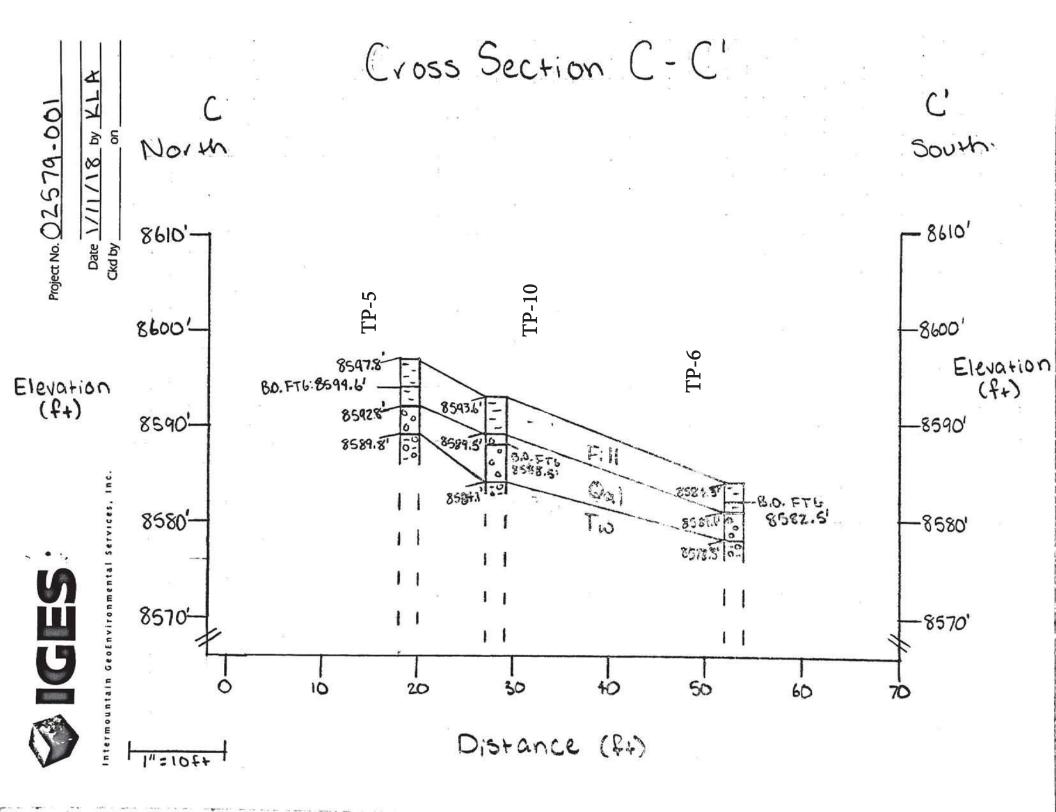
Basemap: Sheet 1, "Powdercat Test Pit Locations", prepared by Talisman, dated 01-09-18

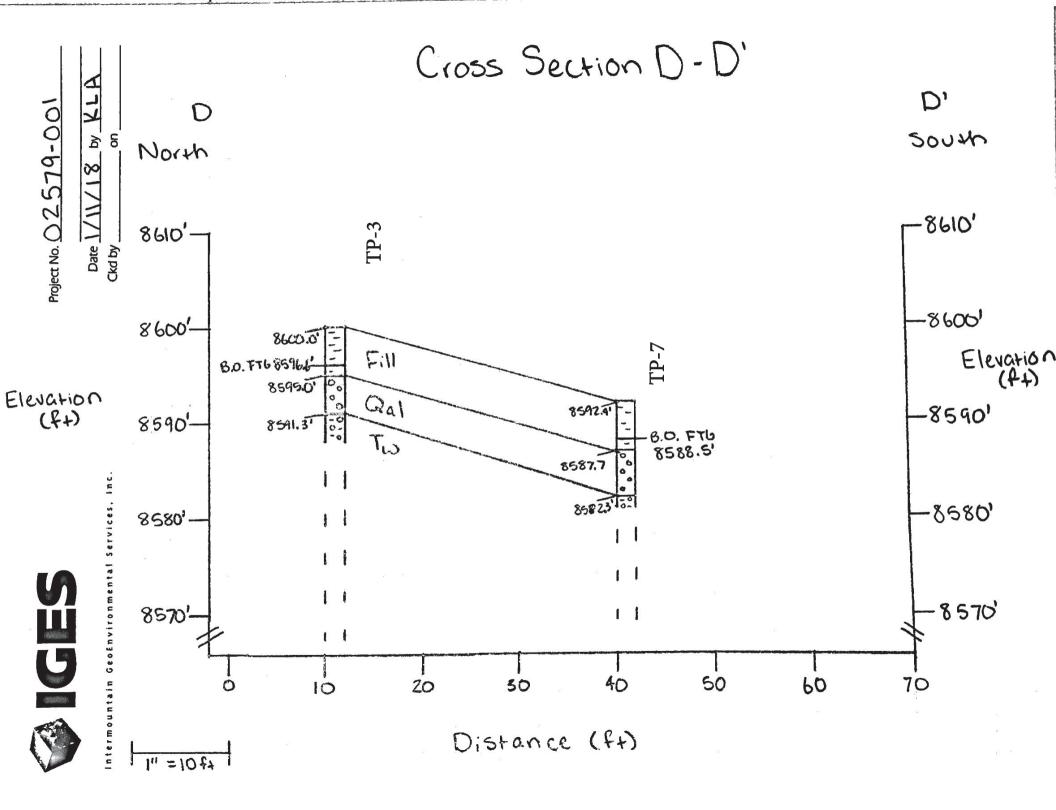


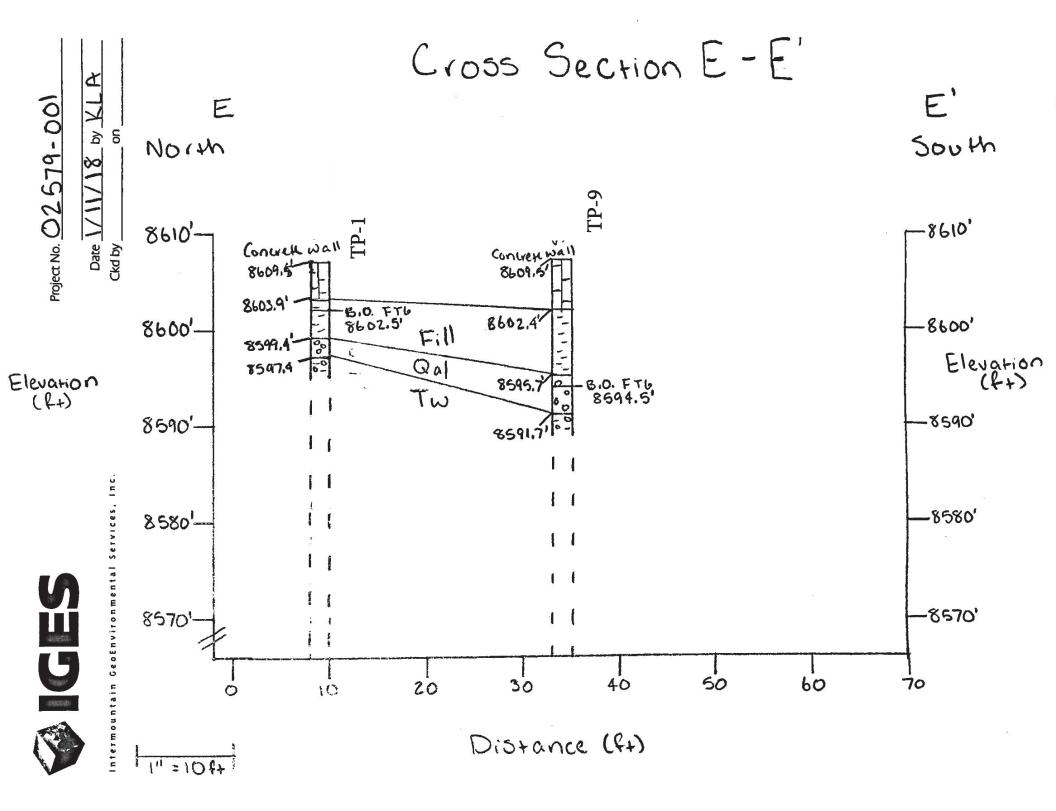
Supplemental Subsurface Data
Copper Crest West Townhomes
Summit Powder Mountain Resort
Weber County, Utah GEOTECHNICAL MAP

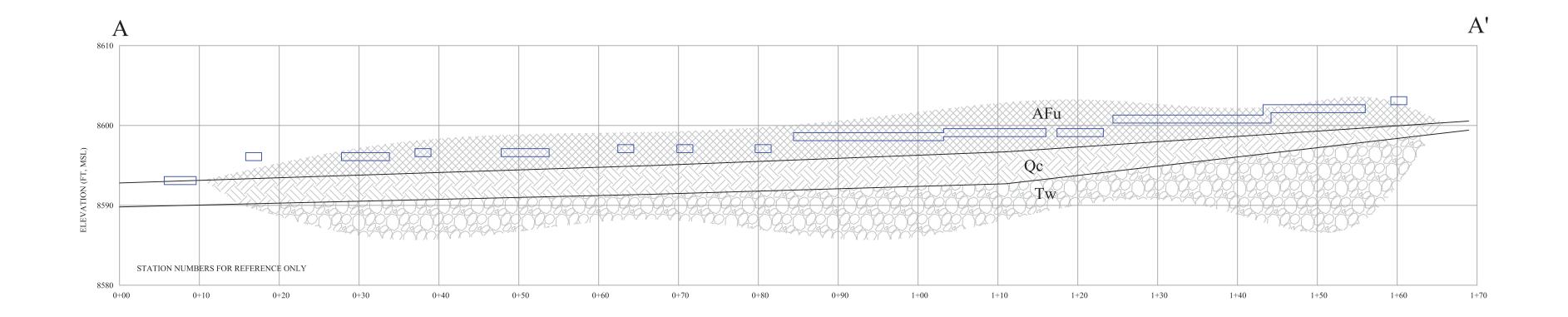


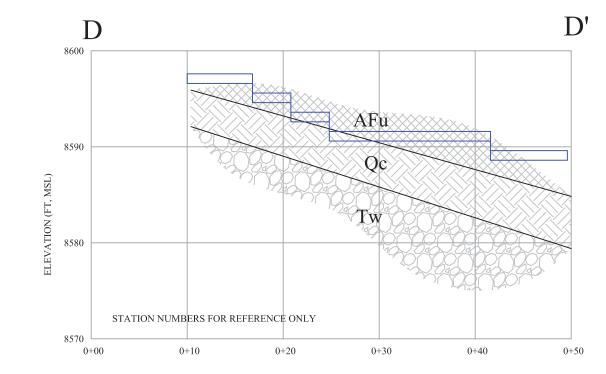


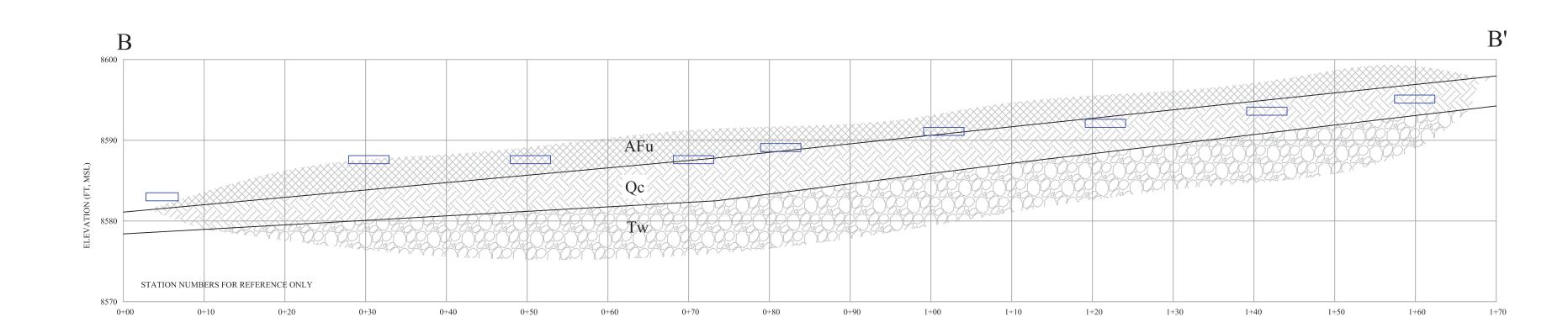


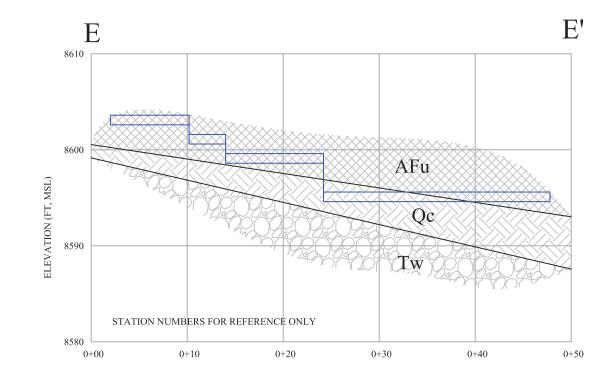


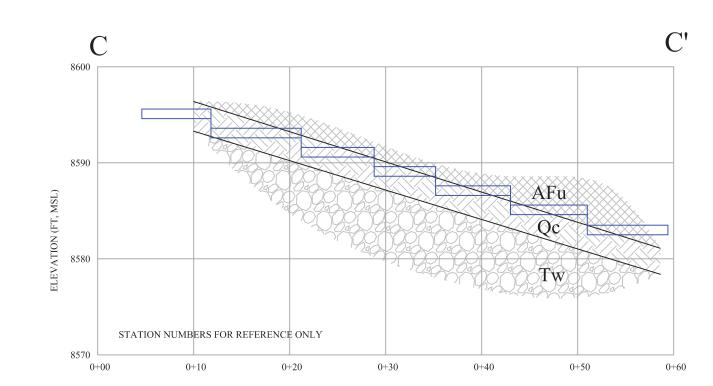












LEGEND

Afu - undocumented fill

Qc - Colluvium

Tw - Wasatch Formation (conglomerate)

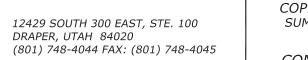
Proposed foundation element

Ground surface not shown









February 21, 2018

Powder Cat Townhomes, LLC c/o Mr. David Orr 11180 Sunrise Valley Drive, #300 Reston, VA 20191

IGES Project No. 02579-001

Subject: Additional Grading Recommendations

Copper Crest West Townhomes Summit Powder Mountain Resort

Weber County, Utah

Reference: IGES, Inc., 2017, Geotechnical and Geologic Hazard Investigation, Copper Crest

West, Summit Powder Mountain Resort, Weber County, Utah, Project No. 01628-

022, dated January 16, 2017.

IGES, Inc., 2018, Supplemental Subsurface Assessment, Copper Crest West Townhomes,

Summit Powder Mountain Resort, Weber County, Utah, Project No. 02579-001,

dated January 30, 2018.

Mr. Orr:

Based on on-going discussions with the Client regarding anticipated grading for the Copper Crest West project, the following recommendations are made:

- Over-excavation below structural elements should extend ½ feet laterally for every foot of over-excavation. The minimum lateral distance is 1 foot.
- Below slab-on-grade, where undocumented fill and/or topsoil is exposed on the subgrade, a minimum over-excavation of 2 feet below slab-on-grade *finish floor* is recommended. Prior to placing engineered fill, the exposed subgrade should be scarified a minimum of 6 inches, moisture-conditioned as necessary, and compacted to approximately 93% of the maximum dry density (modified Proctor). If particularly soft, loose, or otherwise deleterious material is exposed, particularly where the exposed soils appear consist of topsoil, additional over-excavation may be warranted.

All other recommendations presented in the referenced geotechnical reports remain valid and should be implemented into the design and construction of the project, except as superseded herein.

Closure

We appreciate the opportunity to provide you with our services. If you have any questions please contact the undersigned at your convenience (801) 748-4044.

Respectfully Submitted, IGES, Inc.

David A. Glass, P.E.

Senior Geotechnical Engineer

No. 6370734