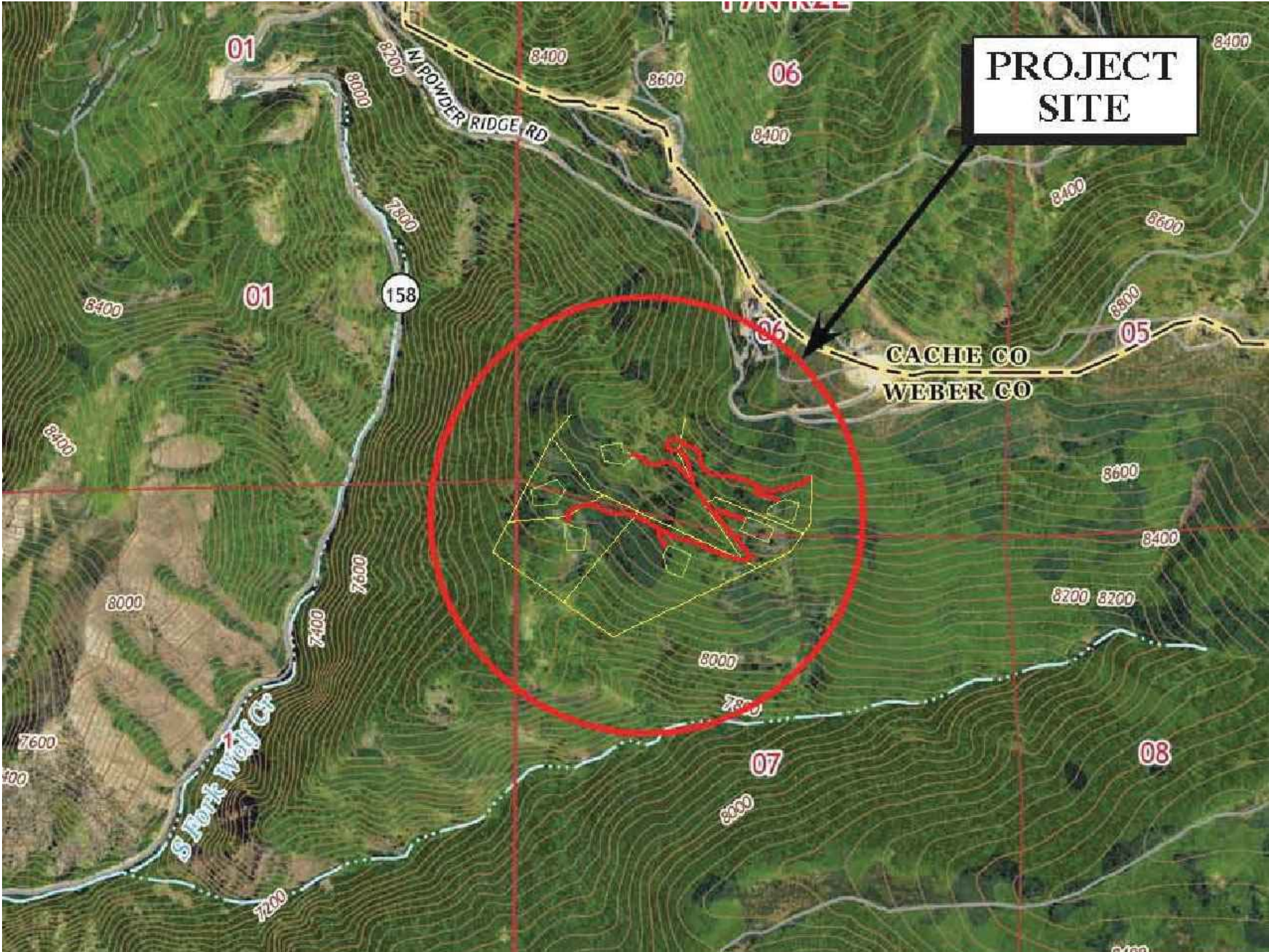




ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH



PROJECT PLAN VIEW

BASE MAP: IGES, 2015, GEOTECHNICAL INVESTIGATION, SUMMIT EDEN PHASE 1E, SUMMIT AT POWDER MOUNTAIN RESORT, WEBER COUNTY, UTAH, IGES PROJECT NO. 01628-001, DATED AUG 10, 2015, DRAFT, FIGURE A-1

| DESIGN PACKAGE CONTENTS    |             |                                |
|----------------------------|-------------|--------------------------------|
|                            | SHEET NO.   | DESCRIPTION                    |
| SHOP DRAWINGS              | 1           | COVER SHEET                    |
|                            | 2           | PLAN VIEW                      |
|                            | 3           | TYPICAL ROCKERY SECTION        |
|                            | 4           | ROCKERY SPECIFICATIONS & NOTES |
|                            | 5           | DESIGN CRITERIA                |
| DESIGN CALCULATION PACKAGE | SECTION 2.1 | ROCKERY STABILITY CALCULATIONS |
|                            | SECTION 2.2 | GLOBAL STABILITY CALCULATIONS  |

|               |  |
|---------------|--|
| PREPARED FOR: | SUMMIT MOUNTAIN HOLDING GROUP<br>3632 NORTH WOLF CREEK DRIVE<br>EDEN, UTAH 84310<br>ATTN: MR. RICK EVERSON (WATTS ENTERPRISES) |
| PREPARED BY:  | <br>SHUN LI, P.E.I.  |
| REVIEWED BY:  | <br>DAVID A. GLASS, P.E.   |



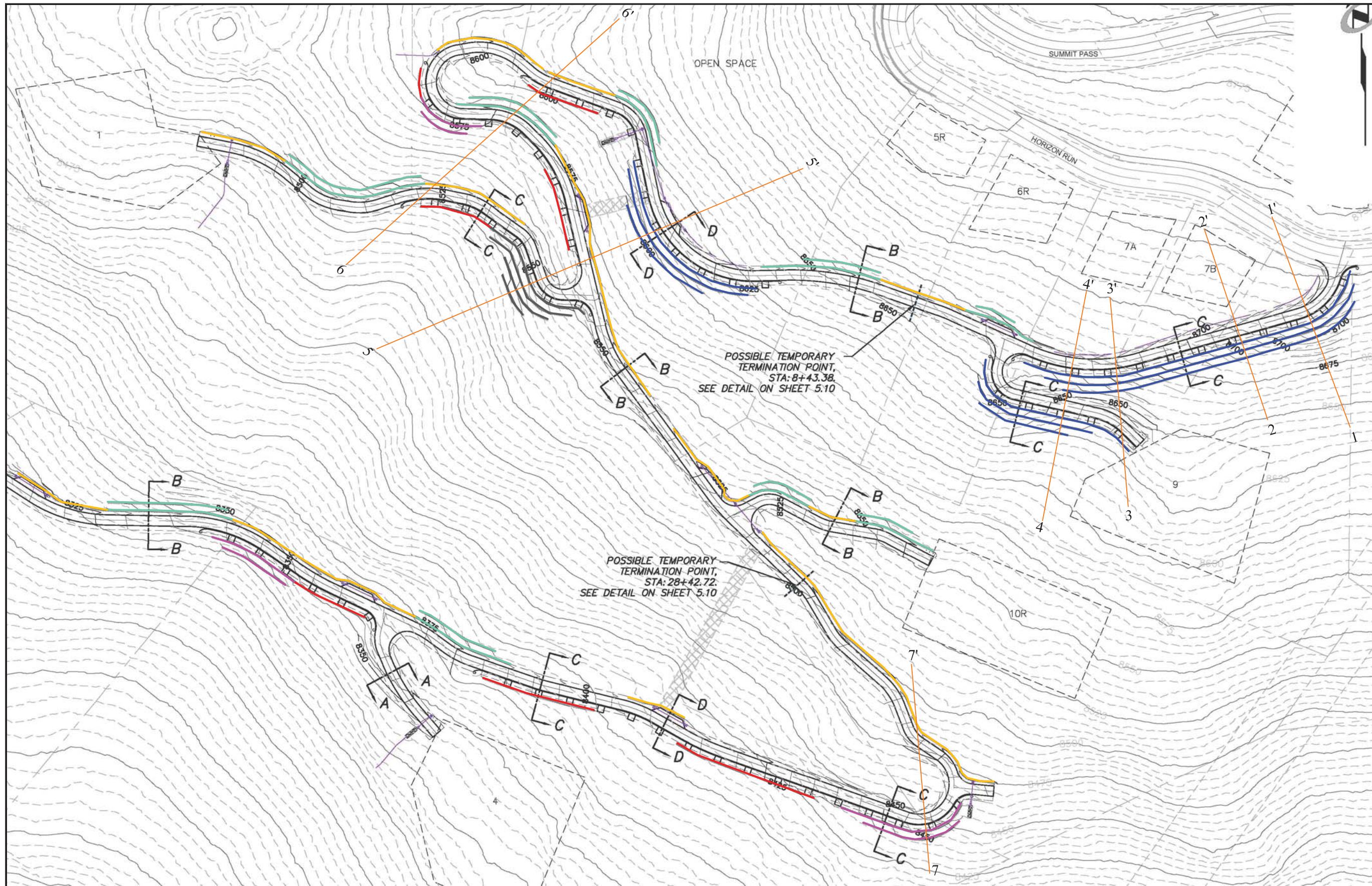
| REV       | DATE | BY | CHK |
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| REVISIONS |      |    |     |



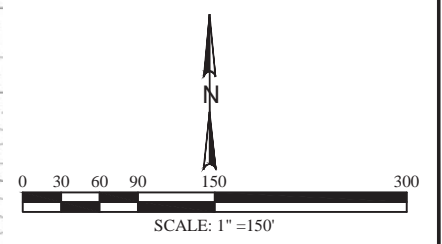
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 COVER SHEET

|                            |             |            |
|----------------------------|-------------|------------|
| DESIGNED BY: SL            | OCT 1, 2015 | PLOT SCALE |
| DRAWN BY: SL               | OCT 1, 2015 | 1=1        |
| CHECKED BY: DAG            | OCT 1, 2015 | DWG SCALE  |
| APPROVED BY: DAG           | OCT 1, 2015 | 1''=300'   |
| IGES PROJECT NO. 01628-011 | SHEET NO. 1 | REV. N/A   |



- 1' ——— 1'  
GLOBAL STABILITY ANALYSIS SECTION
- ROCKERY DESIGN 1
- ROCKERY DESIGN 2
- ROCKERY DESIGN 3
- ROCKERY DESIGN 4
- ROCKERY DESIGN 5
- ROCKERY DESIGN 6



**PROJECT PLAN VIEW**

BASE MAP: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, OVERALL GRADING  
 PLAN, SHEET 1.04, DATE SUBMITTED 7-7-2015, UPDATED 9-18-2015

| REV | DATE | BY | CHK |
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REVISIONS



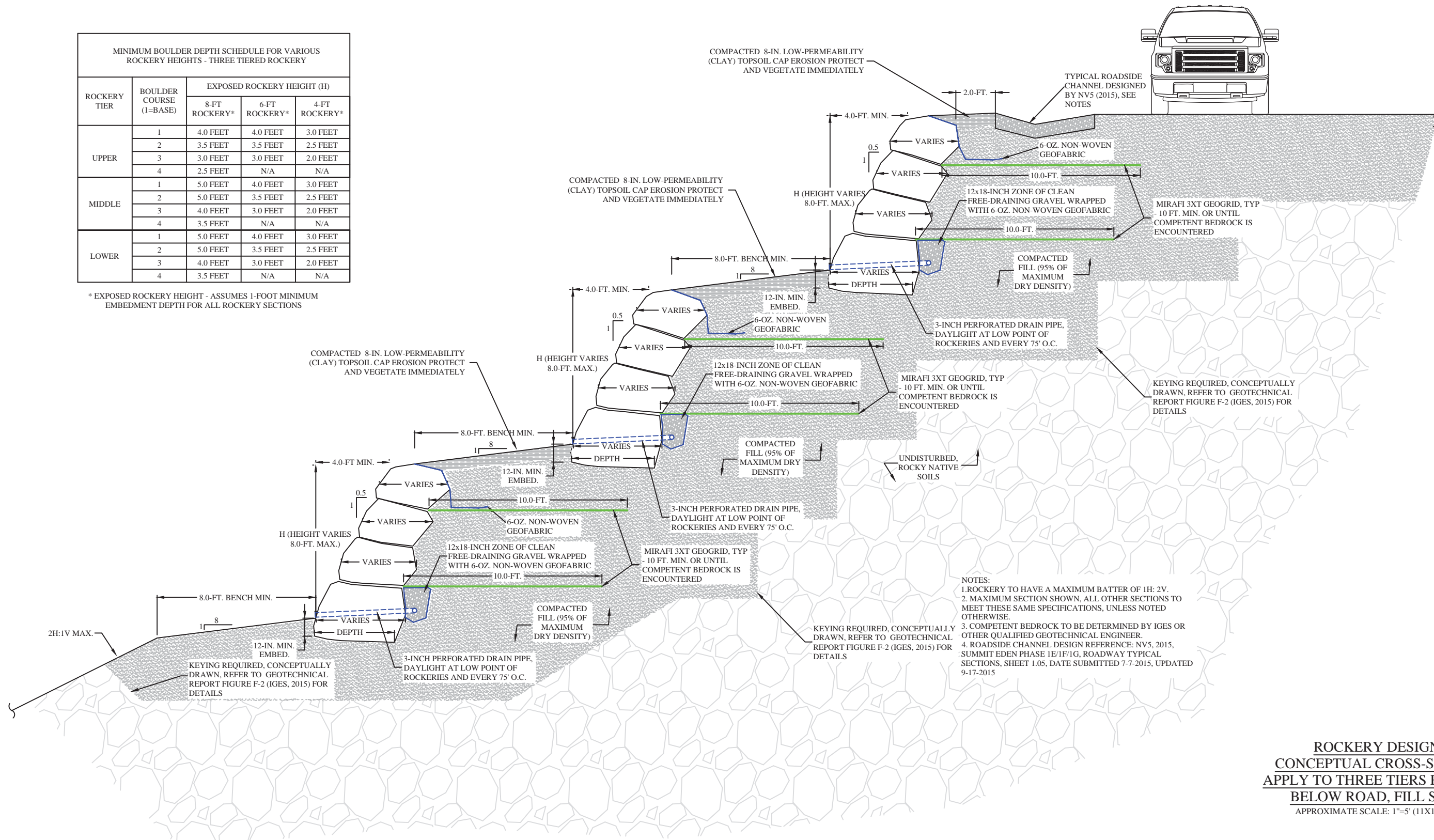
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 PLAN VIEW

|                            |             |            |         |
|----------------------------|-------------|------------|---------|
| DESIGNED BY: SL            | OCT 1, 2015 | PLOT SCALE | 1=1     |
| DRAWN BY: SL               | OCT 1, 2015 | DWG SCALE  | 1"=150' |
| CHECKED BY: DAG            | OCT 1, 2015 |            |         |
| APPROVED BY: DAG           | OCT 1, 2015 |            |         |
| IGES PROJECT NO. 01628-011 | SHEET NO. 2 | REV.       | N/A     |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - THREE TIERED ROCKERY |                         |                            |               |               |
|---|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER  | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|   |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| UPPER   | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 2.5 FEET                   | N/A           | N/A           |
| MIDDLE  | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 3.5 FEET                   | N/A           | N/A           |
| LOWER   | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 3.5 FEET                   | N/A           | N/A           |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



- NOTES:
1. ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.
  2. MAXIMUM SECTION SHOWN, ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.
  3. COMPETENT BEDROCK TO BE DETERMINED BY IGES OR OTHER QUALIFIED GEOTECHNICAL ENGINEER.
  4. ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 1**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO THREE TIERS ROCKERY**  
**BELOW ROAD, FILL SLOPE**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV | DATE | BY | CHK |
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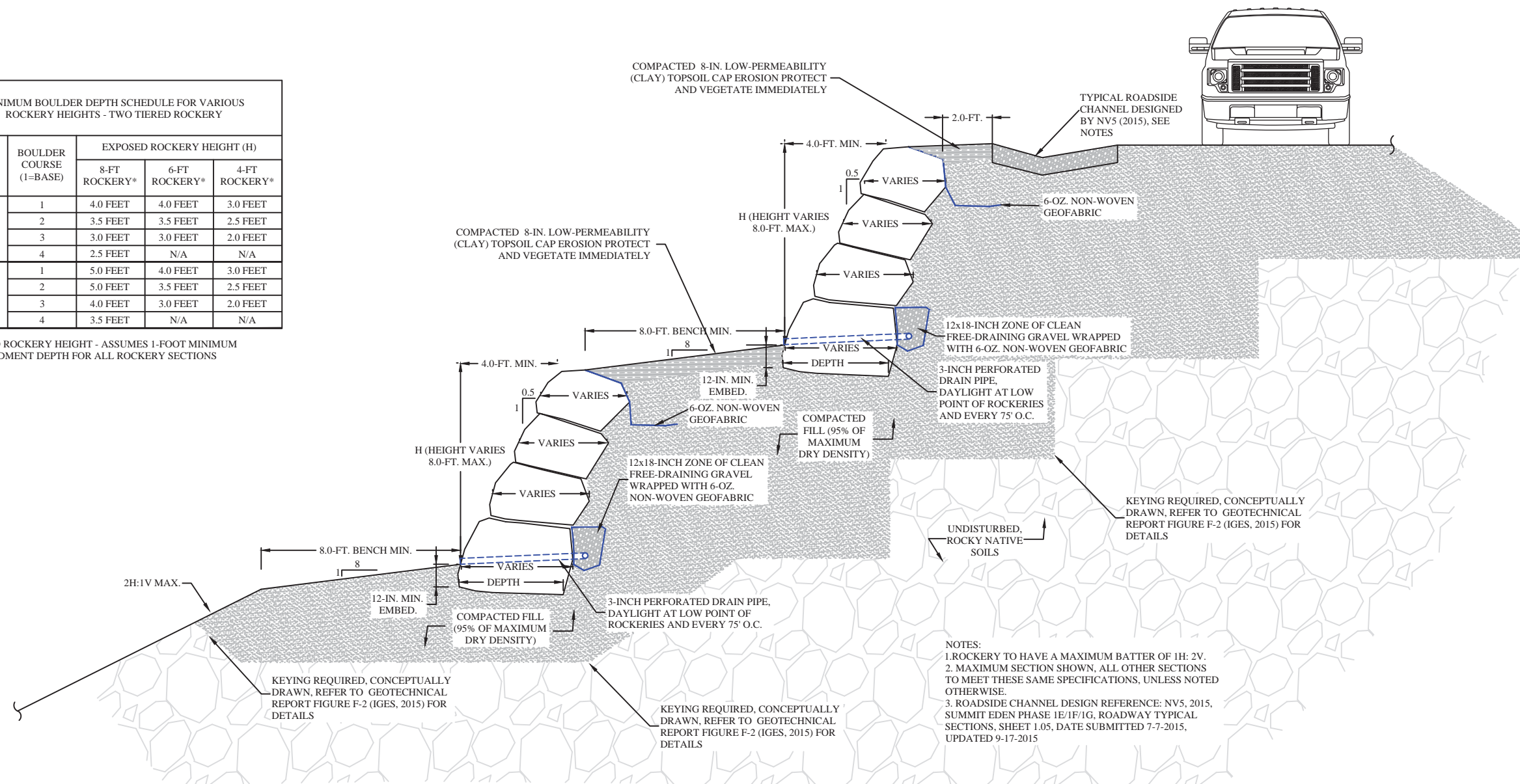
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                  |             |                  |           |
|------------------|-------------|------------------|-----------|
| DESIGNED BY: SL  | OCT 1, 2015 | PLOT SCALE       | 1=1       |
| DRAWN BY: SL     | OCT 1, 2015 | DWG SCALE        | 1"=5'     |
| CHECKED BY: DAG  | OCT 1, 2015 | IGES PROJECT NO. | 01628-011 |
| APPROVED BY: DAG | OCT 1, 2015 | SHEET NO.        | 3.a       |
| REV.             | N/A         |                  |           |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - TWO TIERED ROCKERY |                         |                            |               |               |
|---|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER  | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|   |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| UPPER   | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 2.5 FEET                   | N/A           | N/A           |
| LOWER   | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 3.5 FEET                   | N/A           | N/A           |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



NOTES:  
 1. ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.  
 2. MAXIMUM SECTION SHOWN, ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.  
 3. ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 2**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO TWO TIERS ROCKERY**  
**BELOW ROAD, FILL SLOPE**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV | DATE | BY | CHK |
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REVISIONS



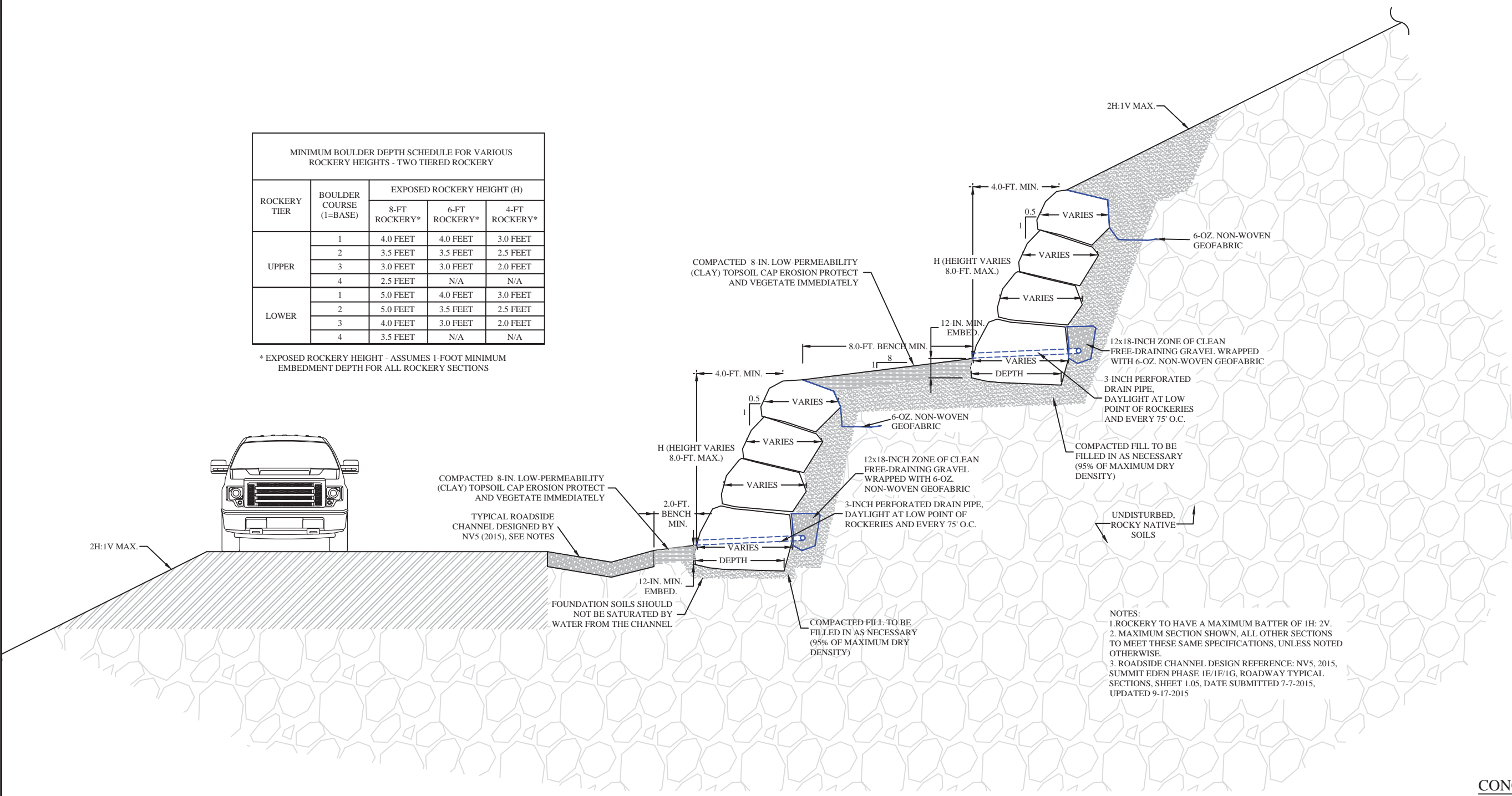
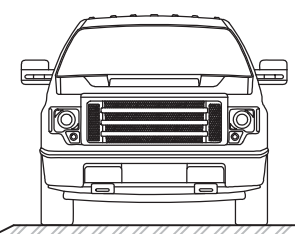
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                  |             |                  |           |
|------------------|-------------|------------------|-----------|
| DESIGNED BY: SL  | OCT 1, 2015 | PLOT SCALE       | 1=1       |
| DRAWN BY: SL     | OCT 1, 2015 | DWG SCALE        | 1"=5'     |
| CHECKED BY: DAG  | OCT 1, 2015 | IGES PROJECT NO. | 01628-011 |
| APPROVED BY: DAG | OCT 1, 2015 | SHEET NO.        | 3.b       |
| REV.             | N/A         |                  |           |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - TWO TIERED ROCKERY |                         |                            |               |               |
|---|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER  | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|   |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| UPPER   | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 2.5 FEET                   | N/A           | N/A           |
| LOWER   | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|   | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|   | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|   | 4                       | 3.5 FEET                   | N/A           | N/A           |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



- NOTES:
- ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.
  - MAXIMUM SECTION SHOWN, ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.
  - ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 3**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO TWO TIERS ROCKERY**  
**ABOVE ROAD, CUT SLOPE**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV | DATE | BY | CHK |
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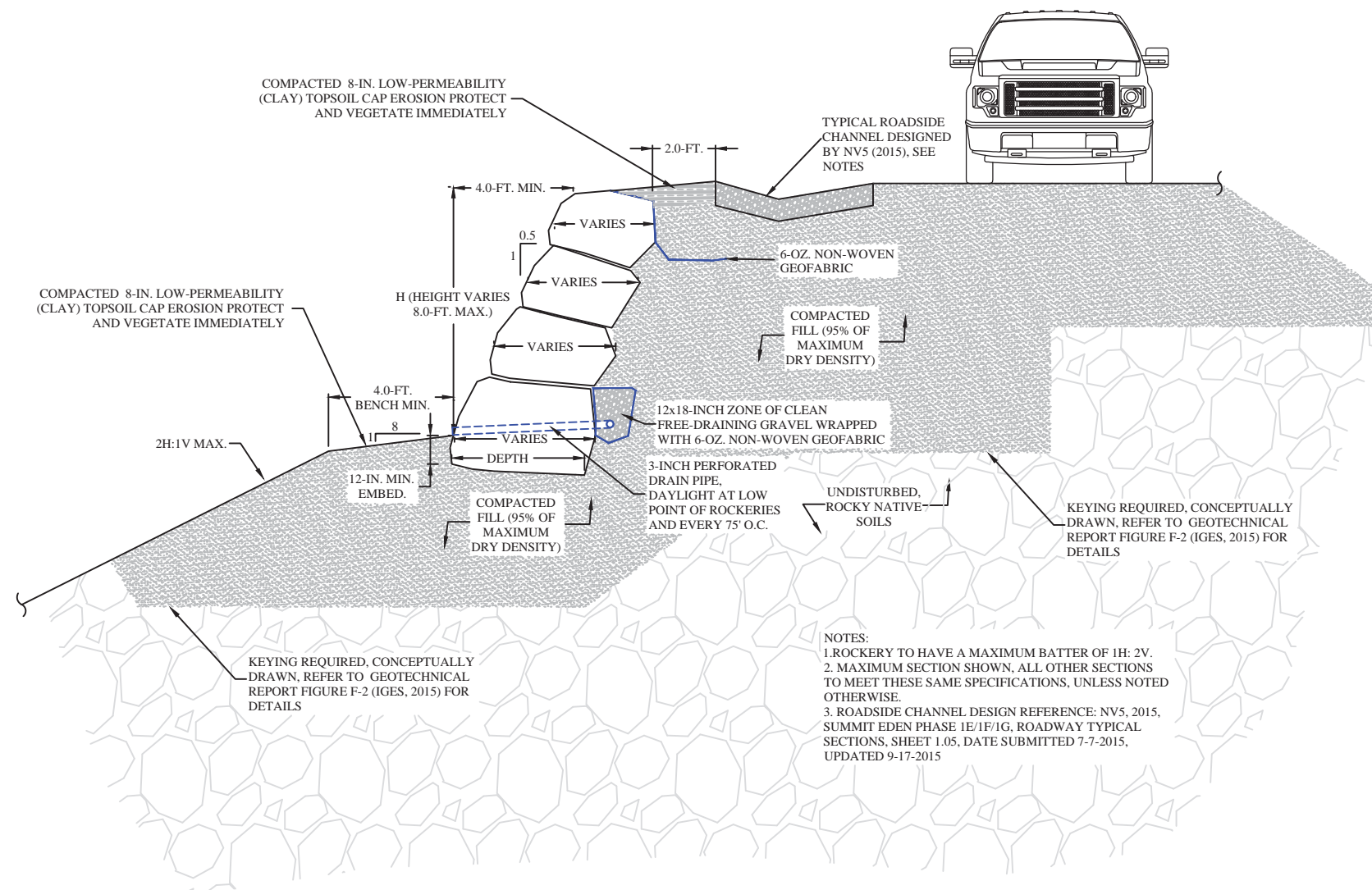
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                            |               |            |
|----------------------------|---------------|------------|
| DESIGNED BY: SL            | OCT 1, 2015   | PLOT SCALE |
| DRAWN BY: SL               | OCT 1, 2015   | 1=1        |
| CHECKED BY: DAG            | OCT 1, 2015   | DWG SCALE  |
| APPROVED BY: DAG           | OCT 1, 2015   | 1"=5'      |
| IGES PROJECT NO. 01628-011 | SHEET NO. 3.C | REV. N/A   |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - SINGLE TIERED ROCKERY |                         |                            |               |               |
|--|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER   | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|  |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| SINGLE   | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|  | 4                       | 2.5 FEET                   | N/A           | N/A           |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



NOTES:  
 1. ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.  
 2. MAXIMUM SECTION SHOWN, ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.  
 3. ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 4**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO SINGLE TIER ROCKERY**  
**BELOW ROAD, FILL SLOPE**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV       | DATE | BY | CHK |
|-----------|------|----|-----|
| REVISIONS |      |    |     |



**IGES**

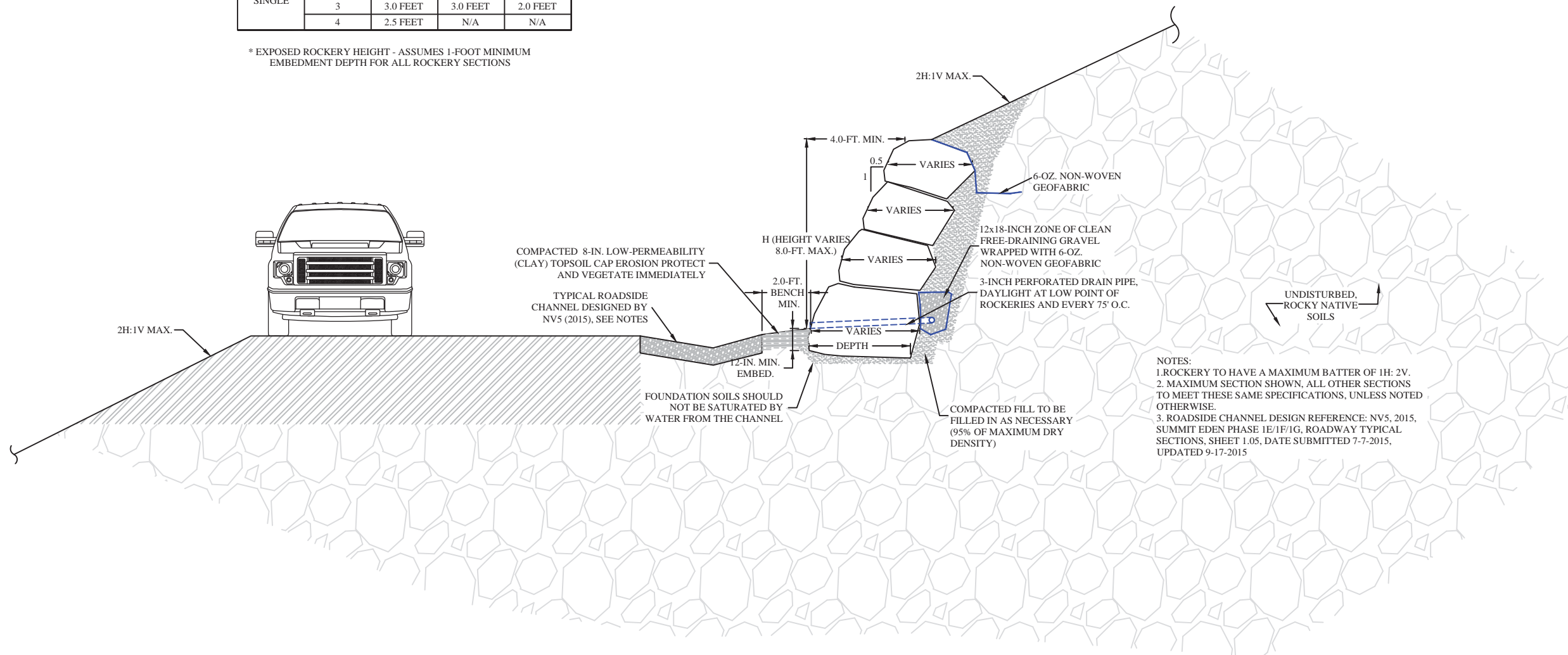
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                            |               |            |
|----------------------------|---------------|------------|
| DESIGNED BY: SL            | OCT 1, 2015   | PLOT SCALE |
| DRAWN BY: SL               | OCT 1, 2015   | 1=1        |
| CHECKED BY: DAG            | OCT 1, 2015   | DWG SCALE  |
| APPROVED BY: DAG           | OCT 1, 2015   | 1"=5'      |
| IGES PROJECT NO. 01628-011 | SHEET NO. 3.d | REV. N/A   |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - SINGLE TIERED ROCKERY |                         |                            |               |               |
|--|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER   | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|  |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| SINGLE   | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|  | 4                       | 2.5 FEET                   | N/A           | N/A           |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



- NOTES:
1. ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.
  2. MAXIMUM SECTION SHOWN. ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.
  3. ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 5**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO SINGLE TIER ROCKERY**  
**ABOVE ROAD, CUT SLOPE**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV | REVISIONS | DATE | BY | CHK |
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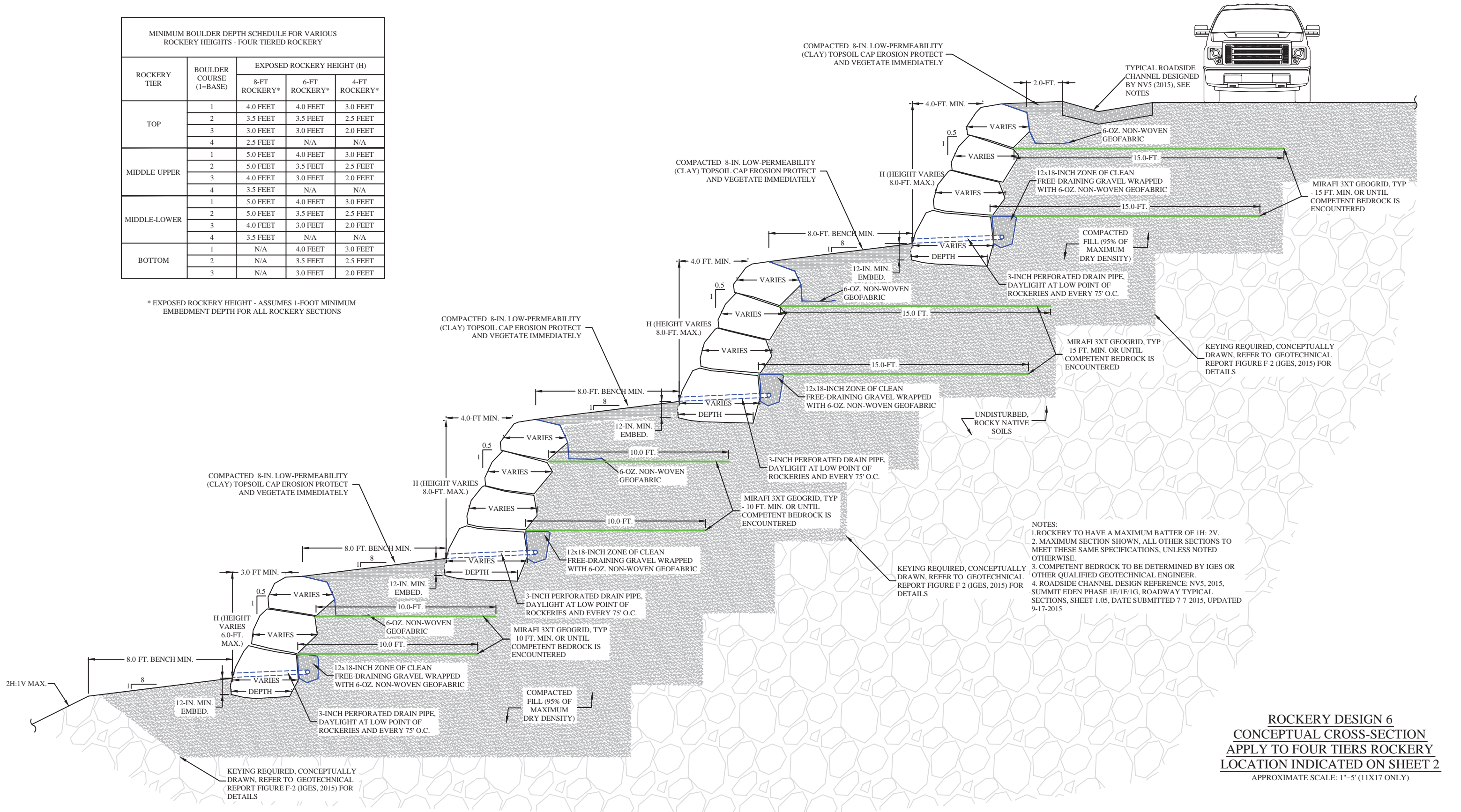
12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                            |               |            |
|----------------------------|---------------|------------|
| DESIGNED BY: SL            | OCT 1, 2015   | PLOT SCALE |
| DRAWN BY: SL               | OCT 1, 2015   | 1=1        |
| CHECKED BY: DAG            | OCT 1, 2015   | DWG SCALE  |
| APPROVED BY: DAG           | OCT 1, 2015   | 1"=5'      |
| IGES PROJECT NO. 01628-011 | SHEET NO. 3.e | REV. N/A   |

| MINIMUM BOULDER DEPTH SCHEDULE FOR VARIOUS ROCKERY HEIGHTS - FOUR TIERED ROCKERY |                         |                            |               |               |
|--|-------------------------|----------------------------|---------------|---------------|
| ROCKERY TIER   | BOULDER COURSE (1=BASE) | EXPOSED ROCKERY HEIGHT (H) |               |               |
|  |                         | 8-FT ROCKERY*              | 6-FT ROCKERY* | 4-FT ROCKERY* |
| TOP  | 1                       | 4.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | 3.5 FEET                   | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | 3.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|  | 4                       | 2.5 FEET                   | N/A           | N/A           |
| MIDDLE-UPPER   | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|  | 4                       | 3.5 FEET                   | N/A           | N/A           |
| MIDDLE-LOWER   | 1                       | 5.0 FEET                   | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | 5.0 FEET                   | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | 4.0 FEET                   | 3.0 FEET      | 2.0 FEET      |
|  | 4                       | 3.5 FEET                   | N/A           | N/A           |
| BOTTOM   | 1                       | N/A                        | 4.0 FEET      | 3.0 FEET      |
|  | 2                       | N/A                        | 3.5 FEET      | 2.5 FEET      |
|  | 3                       | N/A                        | 3.0 FEET      | 2.0 FEET      |

\* EXPOSED ROCKERY HEIGHT - ASSUMES 1-FOOT MINIMUM EMBEDMENT DEPTH FOR ALL ROCKERY SECTIONS



- NOTES:
1. ROCKERY TO HAVE A MAXIMUM BATTER OF 1H: 2V.
  2. MAXIMUM SECTION SHOWN, ALL OTHER SECTIONS TO MEET THESE SAME SPECIFICATIONS, UNLESS NOTED OTHERWISE.
  3. COMPETENT BEDROCK TO BE DETERMINED BY IGES OR OTHER QUALIFIED GEOTECHNICAL ENGINEER.
  4. ROADSIDE CHANNEL DESIGN REFERENCE: NV5, 2015, SUMMIT EDEN PHASE 1E/1F/1G, ROADWAY TYPICAL SECTIONS, SHEET 1.05, DATE SUBMITTED 7-7-2015, UPDATED 9-17-2015

**ROCKERY DESIGN 6**  
**CONCEPTUAL CROSS-SECTION**  
**APPLY TO FOUR TIERS ROCKERY**  
**LOCATION INDICATED ON SHEET 2**  
 APPROXIMATE SCALE: 1"=5' (11X17 ONLY)

| REV | DATE | BY | CHK |
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12429 SOUTH 300 EAST, STE. 100  
 DRAPER, UTAH 84020  
 (801) 748-4044 FAX: (801) 748-4045

ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 TYPICAL SECTION VIEW

|                  |             |                  |           |
|------------------|-------------|------------------|-----------|
| DESIGNED BY: SL  | OCT 1, 2015 | PLOT SCALE       | 1=1       |
| DRAWN BY: SL     | OCT 1, 2015 | DWG SCALE        | 1"=5'     |
| CHECKED BY: DAG  | OCT 1, 2015 | IGES PROJECT NO. | 01628-011 |
| APPROVED BY: DAG | OCT 1, 2015 | SHEET NO.        | 3.e       |
| REV.             | N/A         |                  |           |



**ROCKERY CONSTRUCTION SPECIFICATIONS:**

**GENERAL**

- DESIGN AND CONSTRUCTION INFORMATION IS BASED ON SITE GEOMETRY PROVIDED BY THE CLIENT, THE REFERENCED CONSTRUCTION PLAN, AND THE ENGINEERING ANALYSIS PERFORMED AS PART OF THE SCOPE OF WORK FOR THIS PROJECT.
- CONTRACTOR SHALL LOCATE AND FULLY RESOLVE ALL CONFLICTS WITH EXISTING AND/OR PROPOSED UTILITIES PRIOR TO ROCKERY CONSTRUCTION.
- THE FOLLOWING MEASURES SHALL BE IMPLEMENTED TO REDUCE THE POTENTIAL FOR SATURATION OF THE SOIL BEHIND THE ROCKERY .
- HARDSCAPE, VEGETATION, OR EROSION CONTROL MEASURES SHALL BE ESTABLISHED ABOVE AND BELOW THE ROCKERY IMMEDIATELY FOLLOWING CONSTRUCTION.
- CONDITIONS SUCH AS LEAKY OR BROKEN IRRIGATION LINES AND/OR RUNOFF FROM PRECIPITATION CAN LEAD TO UNDERMINING OR SATURATION OF THE SOIL BEHIND THE ROCKERY, WHICH CAN LEAD TO SLOPE OR ROCKERY DISTRESS AND/OR MOVEMENT. THESE CONDITIONS WERE NOT CONSIDERED IN THE ANALYSIS OF THE ROCKERY AND MUST BE PREVENTED.
- THE OWNER SHALL BE AWARE OF THE RISKS IF THESE OR OTHER CONDITIONS OCCUR THAT COULD SATURATE OR ERODE THE SOIL BEHIND THE ROCKERY.

**MATERIALS**

- THE FILL ZONE BEHIND AND BELOW THE ROCKERY SHALL CONSIST OF SUITABLE ROCKY NATIVE SOILS OR APPROVED GRANULAR BORROW BACKFILL SOILS AS SHOWN ON THE SECTION VIEWS.
- MATERIAL USED TO FILL IN THE SPACE BETWEEN THE ROCKS AND THE SOIL CUT SHALL CONSIST OF GRANULAR SOILS MEETING THE FOLLOWING CRITERIA:
  - GRANULAR MATERIALS CONTAINING LESS THAN 35% FINES
  - MAXIMUM NOMINAL PARTICLE SIZE OF 4 INCHES
  - REASONABLY FREE FROM ORGANIC OR OTHER DELETERIOUS MATERIALS
- ROCKS TO BE USED AS FACING SHALL BE DURABLE ANGULAR BOULDERS WITH A MINIMUM NOMINAL DIAMETER OF 18 INCHES. ROCK SIZES SHALL MEET ALL MINIMUM DIAMETERS IN ACCORDANCE WITH DESIGN DRAWINGS. ROCKS SHOULD FOLLOW FHWA GUIDELINES:
  - ROCKS SHALL BE HARD, ANGULAR, DURABLE, AND ABLE TO RESIST PHYSICAL, CLIMATIC, AND CHEMICAL DECOMPOSITION.
  - ROCKS SHALL BE ROUGHLY RECTANGULAR, TABULAR, OR CUBIC IN SHAPE; ROUNDED ROCKS AND COBBLES SHOULD NOT BE USED.
  - ROCKS SHOULD CONSIST OF INTACT BLOCKS WITHOUT OPEN FRACTURES, FOLIATION, OR OTHER PLANES OF WEAKNESS
- GEOTEXTILE FABRIC SHALL BE NON-WOVEN AND 6.0-OZ. MIN.

**COMPACTION**

- BACKFILL SHOULD BE COMPACTED TO 90% OF MAXIMUM DRY DENSITY (MDD) IN LANDSCAPED AREAS AND 95% OF MDD UNDER STRUCTURES AS DETERMINED BY ASTM D1557 (MODIFIED PROCTOR). THE MOISTURE CONTENT FOR ALL BACKFILL SHOULD BE AT OR SLIGHTLY ABOVE THE OPTIMUM MOISTURE CONTENT (OMC) AT THE TIME OF PLACEMENT AND COMPACTION BASED ON ASTM D1557 .
- ALL BACKFILL SHOULD BE PLACED IN MAXIMUM 4-INCH LOOSE LIFTS IF COMPACTED BY SMALL HAND-OPERATED COMPACTION EQUIPMENT, MAXIMUM 6-INCH LOOSE LIFTS IF COMPACTED BY LIGHT- TO MEDIUM-DUTY ROLLERS, AND MAXIMUM 10-INCH LOOSE LIFTS IF COMPACTED BY HEAVY-DUTY COMPACTION EQUIPMENT THAT IS CAPABLE OF EFFICIENTLY COMPACTING THE ENTIRE THICKNESS OF THE LIFT.
- ALL BACKFILL SHOULD BE COMPACTED ON A HORIZONTAL PLANE.

**INSTALLATION**

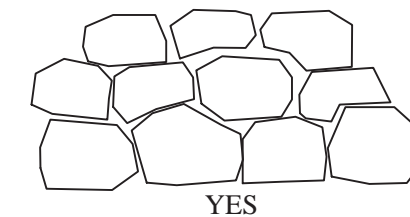
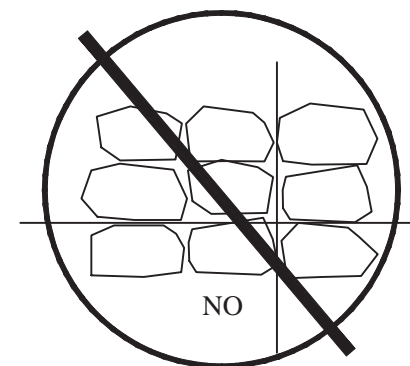
- ROCKS SHOULD BE STACKED IN GENERAL ACCORDANCE WITH THE ASSOCIATED ROCKERY CONTRACTORS (ARC) AND FHWA ROCKERY CONSTRUCTION GUIDELINES. ARC GUIDELINES ARE GIVEN ON THIS SHEET (SEE GUIDELINES TO THE RIGHT). FHWA GUIDELINES ARE SUMMARIZED AS FOLLOWS:
  - EACH ROCK SHOULD BEAR ON AT LEAST TWO OTHER ROCKS BELOW
  - EACH ROCK SHOULD HAVE AT LEAST THREE BEARING POINTS - TWO IN FRONT AND ONE IN BACK
  - THE FRONT-MOST BEARING POINTS FOR EACH ROCK SHOULD BE WITHIN 6 INCHES OF THE AVERAGE FACE OF THE ROCKERY

- THE REAR OF THE ROCKS SHOULD BE ALIGNED ALONG AN IMAGINARY VERTICAL PLANE. IF ROCKS LARGER THAN THE MINIMUM SPECIFIED DIAMETERS ARE USED, THEY CAN EXTEND BEYOND THIS IMAGINARY PLANE PROVIDED THEY DO NOT INTERFERE WITH ROCKERY DRAINAGE
- THE TOPS OF EACH ROCK SHOULD BE SLOPED BACK AT LEAST 5% TOWARDS THE BACK OF THE ROCKERY
- ROCK FACING SHOULD BE STACKED AT A MAXIMUM STEEPNESS OF 1 HORIZONTAL TO 2 VERTICAL.
- THE BOTTOM ROW OF ROCKS SHOULD BE BURIED (EMBEDDED) A MINIMUM DEPTH OF 12 INCHES FOR ALL ROCKERIES.
- ALL BACKFILL SOILS SHALL CONSIST OF FREE DRAINING GRANULAR SOILS.
- ROCKERY CONSTRUCTION SHOULD BE OBSERVED AT REGULAR INTERVALS BY IGES TO ACCOMMODATE FINAL CONSTRUCTION OBSERVATION AND ACCEPTANCE LETTER.
- THE CONTRACTOR IS RESPONSIBLE FOR ARRANGING THE CONSTRUCTION OBSERVATIONS AND QUALITY CONTROL.

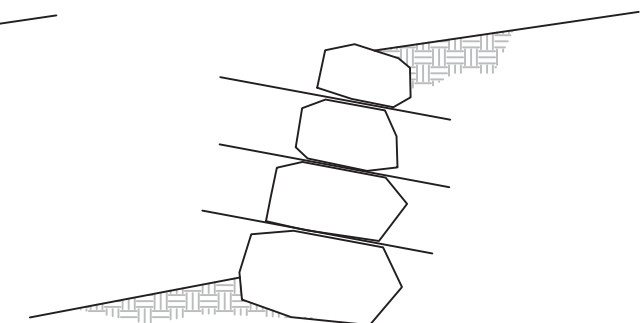
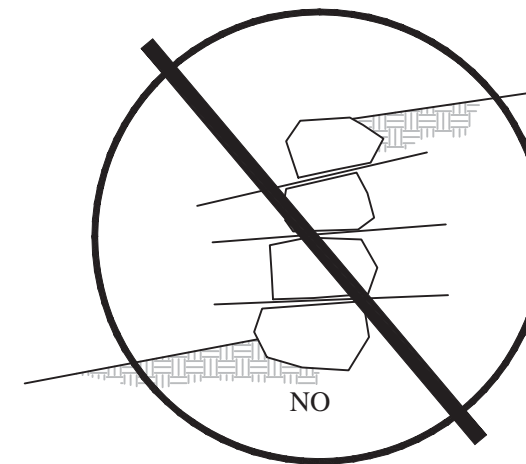
**ROCK STACKING CONSTRUCTION GUIDELINES:**

ROCKS SHOULD BE STACKED IN GENERAL ACCORDANCE WITH FHWA AND THE ASSOCIATED ROCKERY CONTRACTORS (ARC) ROCKERY CONSTRUCTION GUIDELINES, SUMMARIZED AS FOLLOWS:

- ROCKS SHOULD BE PLACED SO THAT THERE ARE NO CONTINUOUS JOINT PLANES IN EITHER THE VERTICAL OR LATERAL DIRECTION (SEE DETAIL A)
- WHEREVER POSSIBLE, EACH ROCK SHOULD BEAR ON AT LEAST TWO ROCKS BELOW IT.
- THE UPPER PLANE OF EACH ROCK BETWEEN COURSES (THE TOP SURFACE OF ROCK), SHOULD SLOPE BACK TOWARDS THE SLOPE FACE AND AWAY FROM THE FACE OF THE ROCK WALL (SEE DETAIL B)



**DETAIL A**



**DETAIL B**

| REV | REVISIONS | DATE | BY | CHK |
|-----|-----------|------|----|-----|
|     |           |      |    |     |
|     |           |      |    |     |
|     |           |      |    |     |



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ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 SPECIFICATIONS & GUIDELINES

|                            |             |            |
|----------------------------|-------------|------------|
| DESIGNED BY: SL            | OCT 1, 2015 | PLOT SCALE |
| DRAWN BY: SL               | OCT 1, 2015 | 1=1        |
| CHECKED BY: DAG            | OCT 1, 2015 | DWG SCALE  |
| APPROVED BY: DAG           | OCT 1, 2015 | NTS        |
| IGES PROJECT NO. 01628-011 | SHEET NO. 4 | REV. N/A   |

| ASSUMED SOIL CONDITIONS USED IN DESIGN |                |          |             |
|--|----------------|----------|-------------|
| EARTH MATERIALS                        | FRICTION ANGLE | COHESION | UNIT WEIGHT |
| STRUCTURAL FILL                        | 36°            | 50 PSF   | 130 PCF     |
| ROCKY COLLUVIUM                        | 44°            | 0 PSF    | 135 PCF     |

SOURCES & NOTES:

- IGES, 2015, GEOTECHNICAL INVESTIGATION, SUMMIT EDEN PHASE 1E, SUMMIT AT POWDER MOUNTAIN RESORT, WEBER COUNTY, UTAH, IGES PROJECT NO. 01628-001, DATED AUG 10, 2015, DRAFT
- COHESION WAS USED IN GLOBAL STABILITY ANALYSES ONLY

| ROCKERY ANALYSIS USED IN DESIGN |   |
|---------------------------------|---|
| ANALYSIS                        | DESIGN REFERENCES/SOFTWARE  |
| EXTERNAL/INTERNAL STABILITY     | MACK, D.A., SANDERS, S.H., MILLHONE, W.L., FIPPIN, R.L., AND KENNEDY, D.G., 2006, ROCKERY DESIGN AND CONSTRUCTION GUIDELINES, SANDERS & ASSOCIATES GEOSTRUCTURAL ENGINEERING, INC., REPORT NO. FHWA-CFL/TD-06-006, REPORT DATED NOVEMBER 2006 |
| GLOBAL STABILITY                | SLIDE: ROCSCIENCE, INC., 1998-2015, VERSION 6.034, BUILD DATE MARCH 10, 2015  |

| SEISMIC PARAMETERS USED IN DESIGN |  |                                    |   |
|-----------------------------------|--|------------------------------------|---|
| SEISMIC CRITERIA                  | PEAK GROUND ACCELERATION (A <sub>s</sub> ) | GLOBAL STABILITY (k <sub>s</sub> ) | EXTERNAL/INTERNAL STABILITY (k <sub>s</sub> ) |
| 7% IN 75 YEARS                    | 0.26g                                      | 0.10g (GLOBAL)                     | 0.10g   |

SOURCES & NOTES:

- U.S. GEOLOGICAL SURVEY, 2012, U.S. SEISMIC DESIGNMAPS WEB APPLICATION, SITE: <http://earthquake.usgs.gov/designmaps/us/application.php>, ACCESSED 8-13-2015
- A MAXIMUM ALLOWABLE SEISMIC DISPLACEMENT THRESHOLD OF 3 INCHES WAS USED TO ESTABLISH THE HORIZONTAL SEISMIC ACCELERATION COEFFICIENT IN ACCORDANCE WITH AASHTO LRFD METHODOLOGY (SEE BRIDGE DESIGN MANUAL CHAPTER 11-20).

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| REV       | DATE | BY | CHK |
|-----------|------|----|-----|
| REVISIONS |      |    |     |



**IGES**<sup>®</sup>

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ROCKERY DESIGN PACKAGE  
 PHASE 1E, 1F, AND 1G - SUMMIT POWDER MOUNTAIN  
 WEBER COUNTY, UTAH  
 DESIGN CRITERIA

|                            |             |            |     |
|----------------------------|-------------|------------|-----|
| DESIGNED BY: SL            | OCT 1, 2015 | PLOT SCALE |     |
| DRAWN BY: SL               | OCT 1, 2015 |            | 1=1 |
| CHECKED BY: DAG            | OCT 1, 2015 | DWG SCALE  | NTS |
| APPROVED BY: DAG           | OCT 1, 2015 |            |     |
| IGES PROJECT NO. 01628-011 | SHEET NO. 5 | REV.       | N/A |

# **SECTION 2.1**

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 1

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: LOWER TIER - 8-FT EXPOSED**

**SURCHARGE: MIDDLE TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |                             |
|---------|------|-----------------------------|
| $q_s$ = | 1040 | psf                         |
| $x_s$ = | 8    | ft (Distance from soil cut) |
| $W_s$ = | 8    | ft (Width of Strip Load)    |

|         |      |                                   |
|---------|------|-----------------------------------|
| $F_s$ = | 1108 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5  | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 1

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: MIDDLE TIER - 8-FT EXPOSED**

**SURCHARGE: UPPER TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |       |                             |
|---------|------|-------|-----------------------------|
| $q_s$ = | 1040 | psf   |                             |
| $x_s$ = | 8    | ft    | (Distance from soil cut)    |
| $W_s$ = | 8    | ft    | (Width of Strip Load)       |
| $F_s$ = | 1108 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 5.5  | ft    | (Surcharge load centroid)   |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 1

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: UPPER TIER - 8-FT EXPOSED**

**SURCHARGE: TRAFFIC**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.192 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 1.8  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.251 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.2         | OK |
| Overturning              | 2.0         | 7.2         | OK |
| Individual Rock Sliding  | 1.5         | 2.3         | OK |
| Bearing Capacity         | 2.0         | 9.4         | OK |
| Seismic Overturning      | 1.5         | 1.9         | OK |
| Seismic Sliding          | 1.1         | 1.6         | OK |
| Seismic Bearing Capacity | 1.5         | 9.4         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 250 | psf                               |
| $x_s$ = | 7   | ft (Distance from soil cut)       |
| $W_s$ = | 9   | ft (Width of Strip Load)          |
| $F_s$ = | 327 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |             |       |                          |            |
|-------------|--------|-------------|--------|-----|-------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,638  | psf | $e_{s,s}$ = | 0.331 | <b>FS<sub>BC</sub></b>   | <b>9.4</b> |
| $e_s$ =     | -0.358 | $q_{ult}$ = | 15,357 | psf |             | 1,630 | <b>FS<sub>BC,s</sub></b> | <b>9.4</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,293          | 2,046            | 2,985          | 3,058            | 4,695          | 8,119            | 14,748         | 15,234           | 2.5              | 3.2              | 1.6                | 1.9                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 594            | 980              | 1,383          | 1,405            | 1,326          | 3,142            | 9,474          | 9,638            | 2.3              | 7.2              | 1.4                | 3.1                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 285            | 482              | 781            | 790              | 421            | 1,478            | 5,932          | 5,987            | 2.7              | 14.1             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 81             | 143              | 283            | 284              | 54             | 468              | 2,362          | 2,370            | 3.5              | 43.5             | 2.0                | 5.1                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 2

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: LOWER TIER - 8-FT EXPOSED**

**SURCHARGE: UPPER TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |                             |
|---------|------|-----------------------------|
| $q_s$ = | 1040 | psf                         |
| $x_s$ = | 8    | ft (Distance from soil cut) |
| $W_s$ = | 8    | ft (Width of Strip Load)    |

|         |      |                                   |
|---------|------|-----------------------------------|
| $F_s$ = | 1108 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5  | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>μ</sub> | F <sub>μ,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 2

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: UPPER TIER - 8-FT EXPOSED**

**SURCHARGE: TRAFFIC**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.192 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 1.8  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.251 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.2         | OK |
| Overturning              | 2.0         | 7.2         | OK |
| Individual Rock Sliding  | 1.5         | 2.3         | OK |
| Bearing Capacity         | 2.0         | 9.4         | OK |
| Seismic Overturning      | 1.5         | 1.9         | OK |
| Seismic Sliding          | 1.1         | 1.6         | OK |
| Seismic Bearing Capacity | 1.5         | 9.4         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 250 | psf                               |
| $x_s$ = | 7   | ft (Distance from soil cut)       |
| $W_s$ = | 9   | ft (Width of Strip Load)          |
| $F_s$ = | 327 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |             |       |                          |            |
|-------------|--------|-------------|--------|-----|-------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,638  | psf | $e_{s,s}$ = | 0.331 | <b>FS<sub>BC</sub></b>   | <b>9.4</b> |
| $e_s$ =     | -0.358 | $q_{ult}$ = | 15,357 | psf |             | 1,630 | <b>FS<sub>BC,s</sub></b> | <b>9.4</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,293          | 2,046            | 2,985          | 3,058            | 4,695          | 8,119            | 14,748         | 15,234           | 2.5              | 3.2              | 1.6                | 1.9                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 594            | 980              | 1,383          | 1,405            | 1,326          | 3,142            | 9,474          | 9,638            | 2.3              | 7.2              | 1.4                | 3.1                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 285            | 482              | 781            | 790              | 421            | 1,478            | 5,932          | 5,987            | 2.7              | 14.1             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 81             | 143              | 283            | 284              | 54             | 468              | 2,362          | 2,370            | 3.5              | 43.5             | 2.0                | 5.1                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)



PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 3

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: LOWER TIER - 8-FT EXPOSED**

**SURCHARGE: UPPER TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |     |                          |         |      |       |                             |
|---------|------|-----|--------------------------|---------|------|-------|-----------------------------|
| $q_s$ = | 1040 | psf |                          | $F_s$ = | 1108 | lb/ft | (Horizontal Surcharge Load) |
| $x_s$ = | 8    | ft  | (Distance from soil cut) | $y_s$ = | 5.5  | ft    | (Surcharge load centroid)   |
| $W_s$ = | 8    | ft  | (Width of Strip Load)    |         |      |       |                             |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 3

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: UPPER TIER - 8-FT EXPOSED**

**SURCHARGE: N/A**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.279 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 26.6 | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| A =        | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| d =        | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.440 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.4         | OK |
| External Overturning     | 2.0         | 3.6         | OK |
| Overturning              | 2.0         | 9.0         | OK |
| Individual Rock Sliding  | 1.5         | 2.5         | OK |
| Bearing Capacity         | 2.0         | 7.3         | OK |
| Seismic Overturning      | 1.5         | 1.6         | OK |
| Seismic Sliding          | 1.1         | 1.3         | OK |
| Seismic Bearing Capacity | 1.5         | 6.5         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |   |     |                          |
|---------|---|-----|--------------------------|
| $q_s$ = | 0 | psf |                          |
| $x_s$ = | 7 | ft  | (Distance from soil cut) |
| $W_s$ = | 9 | ft  | (Width of Strip Load)    |

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $F_s$ = | 0   | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft    | (Surcharge load centroid)   |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |       |                          |            |
|-------------|--------|-------------|--------|-----|---------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,967  | psf | $e_{s,s}$ =   | 0.617 | <b>FS<sub>BC</sub></b>   | <b>7.3</b> |
| $e_s$ =     | -0.526 | $q_{ult}$ = | 14,400 | psf | $q_{max,s}$ = | 2,236 | <b>FS<sub>BC,s</sub></b> | <b>6.5</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,408          | 2,687            | 3,079          | 3,263            | 4,225          | 10,484           | 15,336         | 16,566           | 2.4              | 3.6              | 1.3                | 1.6                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 565            | 1,161            | 1,412          | 1,470            | 1,073          | 3,610            | 9,676          | 10,090           | 2.5              | 9.0              | 1.3                | 2.8                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 225            | 506              | 792            | 816              | 270            | 1,509            | 6,000          | 6,138            | 3.5              | 22.2             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 39             | 116              | 285            | 289              | 20             | 447              | 2,372          | 2,391            | 7.3              | 121.3            | 2.5                | 5.4                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 4

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: 8-FT EXPOSED**

**SURCHARGE: TRAFFIC**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.192 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 1.8  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.251 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.2         | OK |
| Overturning              | 2.0         | 7.2         | OK |
| Individual Rock Sliding  | 1.5         | 2.3         | OK |
| Bearing Capacity         | 2.0         | 9.4         | OK |
| Seismic Overturning      | 1.5         | 1.9         | OK |
| Seismic Sliding          | 1.1         | 1.6         | OK |
| Seismic Bearing Capacity | 1.5         | 9.4         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 250 | psf                               |
| $x_s$ = | 7   | ft (Distance from soil cut)       |
| $W_s$ = | 9   | ft (Width of Strip Load)          |
| $F_s$ = | 327 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |             |       |                          |            |
|-------------|--------|-------------|--------|-----|-------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,638  | psf | $e_{s,s}$ = | 0.331 | <b>FS<sub>BC</sub></b>   | <b>9.4</b> |
| $e_s$ =     | -0.358 | $q_{ult}$ = | 15,357 | psf |             | 1,630 | <b>FS<sub>BC,s</sub></b> | <b>9.4</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,293          | 2,046            | 2,985          | 3,058            | 4,695          | 8,119            | 14,748         | 15,234           | 2.5              | 3.2              | 1.6                | 1.9                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 594            | 980              | 1,383          | 1,405            | 1,326          | 3,142            | 9,474          | 9,638            | 2.3              | 7.2              | 1.4                | 3.1                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 285            | 482              | 781            | 790              | 421            | 1,478            | 5,932          | 5,987            | 2.7              | 14.1             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 81             | 143              | 283            | 284              | 54             | 468              | 2,362          | 2,370            | 3.5              | 43.5             | 2.0                | 5.1                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1G/1F - ROCKERY DESIGN 5

PROJECT NO.: 01628-011

DATE: 8/18/2015

**SECTION: 8-FT EXPOSED**

**SURCHARGE: N/A**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.279 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 26.6 | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| A =        | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| d =        | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.440 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.4         | OK |
| External Overturning     | 2.0         | 3.6         | OK |
| Overturning              | 2.0         | 9.0         | OK |
| Individual Rock Sliding  | 1.5         | 2.5         | OK |
| Bearing Capacity         | 2.0         | 7.3         | OK |
| Seismic Overturning      | 1.5         | 1.6         | OK |
| Seismic Sliding          | 1.1         | 1.3         | OK |
| Seismic Bearing Capacity | 1.5         | 6.5         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $x_s$ = | 7   | ft    | (Distance from soil cut)    |
| $W_s$ = | 9   | ft    | (Width of Strip Load)       |
| $F_s$ = | 0   | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft    | (Surcharge load centroid)   |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |             |       |                          |            |
|-------------|--------|-------------|--------|-----|-------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,967  | psf | $e_{s,s}$ = | 0.617 | <b>FS<sub>BC</sub></b>   | <b>7.3</b> |
| $e_s$ =     | -0.526 | $q_{ult}$ = | 14,400 | psf |             | 2,236 | <b>FS<sub>BC,s</sub></b> | <b>6.5</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,408          | 2,687            | 3,079          | 3,263            | 4,225          | 10,484           | 15,336         | 16,566           | 2.4              | 3.6              | 1.3                | 1.6                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 565            | 1,161            | 1,412          | 1,470            | 1,073          | 3,610            | 9,676          | 10,090           | 2.5              | 9.0              | 1.3                | 2.8                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 225            | 506              | 792            | 816              | 270            | 1,509            | 6,000          | 6,138            | 3.5              | 22.2             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 39             | 116              | 285            | 289              | 20             | 447              | 2,372          | 2,391            | 7.3              | 121.3            | 2.5                | 5.4                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 6

PROJECT NO.: 01628-011

DATE: 9/28/2015

**SECTION: MIDDLE-LOWER TIER - 8-FT EXPOSED**

**SURCHARGE: MIDDLE-UPPER TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |       |                             |
|---------|------|-------|-----------------------------|
| $q_s$ = | 1040 | psf   |                             |
| $x_s$ = | 8    | ft    | (Distance from soil cut)    |
| $W_s$ = | 8    | ft    | (Width of Strip Load)       |
| $F_s$ = | 1108 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 5.5  | ft    | (Surcharge load centroid)   |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 6

PROJECT NO.: 01628-011

DATE: 9/28/2015

**SECTION: MIDDLE-UPPER TIER - 8-FT EXPOSED**

**SURCHARGE: TOP TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.7         | OK |
| Overturning              | 2.0         | 4.5         | OK |
| Individual Rock Sliding  | 1.5         | 1.6         | OK |
| Bearing Capacity         | 2.0         | 5.2         | OK |
| Seismic Overturning      | 1.5         | 2.3         | OK |
| Seismic Sliding          | 1.1         | 1.7         | OK |
| Seismic Bearing Capacity | 1.5         | 8.8         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |       |                             |
|---------|-----|-------|-----------------------------|
| $q_s$ = | 0   | psf   |                             |
| $F_s$ = | 0.0 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft    | (Surcharge load centroid)   |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |     |                          |
|---------|------|-----|--------------------------|
| $q_s$ = | 1040 | psf |                          |
| $x_s$ = | 8    | ft  | (Distance from soil cut) |
| $W_s$ = | 8    | ft  | (Width of Strip Load)    |

|         |      |       |                             |
|---------|------|-------|-----------------------------|
| $F_s$ = | 1108 | lb/ft | (Horizontal Surcharge Load) |
| $y_s$ = | 5.5  | ft    | (Surcharge load centroid)   |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |        |                          |            |
|-------------|--------|-------------|--------|-----|---------------|--------|--------------------------|------------|
| $e_{max}$ = | 0.833  | $q_{max}$ = | 2,969  | psf | $e_{s,s}$ =   | -0.147 | <b>FS<sub>BC</sub></b>   | <b>5.2</b> |
| $e_s$ =     | -0.847 | $q_{ult}$ = | 15,417 | psf | $q_{max,s}$ = | 1,756  | <b>FS<sub>BC,s</sub></b> | <b>8.8</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 5.0     | 0.7 | 3.5                 | 9.0       | 7,052        | 32,045             | 2,128          | 3,237            | 5,153          | 5,234            | 9,153          | 14,962           | 33,790         | 34,446           | 2.5              | 3.7              | 1.7                | 2.3                |
| 2       | 5.0     | 0.6 | 2.75                | 7.7       | 4,558        | 23,531             | 1,678          | 2,425            | 2,630          | 2,676            | 5,481          | 10,046           | 24,720         | 25,185           | 1.6              | 4.5              | 1.1                | 2.5                |
| 3       | 4.0     | 0.7 | 2.8                 | 4.9       | 2,599        | 14,837             | 905            | 1,287            | 1,480          | 1,499            | 1,972          | 4,618            | 15,222         | 15,371           | 1.6              | 7.7              | 1.2                | 3.3                |
| 4       | 3.5     | 0.6 | 2.1                 | 2.1       | 1,024        | 6,450              | 314            | 441              | 572            | 576              | 310            | 1,405            | 6,510          | 6,533            | 1.8              | 21.0             | 1.3                | 4.7                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**11.2** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 6

PROJECT NO.: 01628-011

DATE: 9/28/2015

**SECTION: TOP TIER - 8-FT EXPOSED**

**SURCHARGE: TRAFFIC**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 9     | ft  | Total Height of Rockery           |
| $H_R$ =        | 8     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.192 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 1.8  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.251 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.5         | OK |
| External Overturning     | 2.0         | 3.2         | OK |
| Overturning              | 2.0         | 7.2         | OK |
| Individual Rock Sliding  | 1.5         | 2.3         | OK |
| Bearing Capacity         | 2.0         | 9.4         | OK |
| Seismic Overturning      | 1.5         | 1.9         | OK |
| Seismic Sliding          | 1.1         | 1.6         | OK |
| Seismic Bearing Capacity | 1.5         | 9.4         | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 4.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 250 | psf                               |
| $x_s$ = | 7   | ft (Distance from soil cut)       |
| $W_s$ = | 9   | ft (Width of Strip Load)          |
| $F_s$ = | 327 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5.5 | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |             |       |                          |            |
|-------------|--------|-------------|--------|-----|-------------|-------|--------------------------|------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,638  | psf | $e_{s,s}$ = | 0.331 | <b>FS<sub>BC</sub></b>   | <b>9.4</b> |
| $e_s$ =     | -0.358 | $q_{ult}$ = | 15,357 | psf |             | 1,630 | <b>FS<sub>BC,s</sub></b> | <b>9.4</b> |

# Rocks = 4 (R\* - Boulder Height to Width Ratio)

| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 9.0       | 3,971        | 13,383             | 1,293          | 2,046            | 2,985          | 3,058            | 4,695          | 8,119            | 14,748         | 15,234           | 2.5              | 3.2              | 1.6                | 1.9                |
| 2       | 3.5     | 0.6 | 2.1                 | 5.7       | 2,396        | 9,035              | 594            | 980              | 1,383          | 1,405            | 1,326          | 3,142            | 9,474          | 9,638            | 2.3              | 7.2              | 1.4                | 3.1                |
| 3       | 3.0     | 0.7 | 2.1                 | 3.6       | 1,373        | 5,785              | 285            | 482              | 781            | 790              | 421            | 1,478            | 5,932          | 5,987            | 2.7              | 14.1             | 1.6                | 4.1                |
| 4       | 2.5     | 0.6 | 1.5                 | 1.5       | 506          | 2,341              | 81             | 143              | 283            | 284              | 54             | 468              | 2,362          | 2,370            | 3.5              | 43.5             | 2.0                | 5.1                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**8.5** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)

PROJECT: SUMMIT EDEN PHASE 1E/1F/1G - ROCKERY DESIGN 6

PROJECT NO.: 01628-011

DATE: 9/28/2015

**SECTION: BOTTOM TIER 6-FT EXPOSED**

**SURCHARGE: MIDDLE-LOWER TIER ROCKERY AND SOIL**



**Rockery Geometry & Soil Data:**

|                |       |     |                                   |
|----------------|-------|-----|-----------------------------------|
| $H_{total}$ =  | 7     | ft  | Total Height of Rockery           |
| $H_R$ =        | 6     | ft  | Exposed Height of Rockery         |
| $\phi_s$ =     | 36    | deg | Soil Friction Angle - Effective   |
| $c_s$ =        | 0     | psf | Cohesion Intercept of soil        |
| $\gamma_s$ =   | 130   | pcf | Unit weight of the soil           |
| $\gamma_R$ =   | 150   | pcf | Unit weight of the rock           |
| $\delta$ =     | 24.0  | deg | Interface Friction Angle          |
| $\psi$ =       | 7.1   | deg | Back Cut Inclination              |
| $\mu$ =        | 0.70  |     | Frictional Component              |
| $\mu_{rock}$ = | 0.55  |     | Rock-to-Rock Friction             |
| $K_A$ =        | 0.202 |     | Active Earth Pressure Coefficient |
| $v$ =          | 63.4  | deg | Rockery Face Angle                |

**Slope Geometry:**

|                            |            |      |     |                 |
|----------------------------|------------|------|-----|-----------------|
| <u>Backslope:</u>          | $\beta$ =  | 7.1  | deg | Backslope Angle |
| <u>Soil Cut Angle:</u>     | $\alpha$ = | 82.9 | deg | Soil Cut Angle  |
| <u>Rockery Face Slope:</u> | 1          | H    | 2   | V               |

**Seismic Earth Pressure Coefficient:**

|            |       |  |
|------------|-------|--|
| $A$ =      | 0.26  | Peak Ground acceleration (7% in 75 years)      |
| $d$ =      | 3     | in (Allowable Displacement)                    |
| $k_h$ =    | 0.10  | Use 1/2 of A? <b>N</b>                         |
| $k_v$ =    | 0     | (If "N" then use displacement-factored $k_h$ ) |
| $\theta$ = | 5.90  |  |
| $K_{AE}$ = | 0.269 | (Mack et al., 2006)                            |

| Failure Mechanism        | FS Required | FS Obtained | OK |
|--------------------------|-------------|-------------|----|
| External Sliding         | 1.5         | 2.7         | OK |
| External Overturning     | 2.0         | 3.3         | OK |
| Overturning              | 2.0         | 7.1         | OK |
| Individual Rock Sliding  | 1.5         | 2.1         | OK |
| Bearing Capacity         | 2.0         | 11.4        | OK |
| Seismic Overturning      | 1.5         | 2.1         | OK |
| Seismic Sliding          | 1.1         | 1.8         | OK |
| Seismic Bearing Capacity | 1.5         | 12.3        | OK |

**Surcharge:**

Uniform: Uniform Applied Surcharge

|         |     |                                   |
|---------|-----|-----------------------------------|
| $q_s$ = | 0   | psf                               |
| $F_s$ = | 0.0 | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 3.5 | ft (Surcharge load centroid)      |

Strip: Strip Load (Boussinesq Equation for Strip Loading)

|         |      |                                   |
|---------|------|-----------------------------------|
| $q_s$ = | 1040 | psf                               |
| $x_s$ = | 8    | ft (Distance from soil cut)       |
| $W_s$ = | 4    | ft (Width of Strip Load)          |
| $F_s$ = | 470  | lb/ft (Horizontal Surcharge Load) |
| $y_s$ = | 5    | ft (Surcharge load centroid)      |

**Factor of Safety against Bearing Capacity:**

|             |        |             |        |     |               |       |                          |             |
|-------------|--------|-------------|--------|-----|---------------|-------|--------------------------|-------------|
| $e_{max}$ = | 0.667  | $q_{max}$ = | 1,377  | psf | $e_{s,s}$ =   | 0.214 | <b>FS<sub>BC</sub></b>   | <b>11.4</b> |
| $e_s$ =     | -0.294 | $q_{ult}$ = | 15,719 | psf | $q_{max,s}$ = | 1,282 | <b>FS<sub>BC,s</sub></b> | <b>12.3</b> |

# Rocks = 3 (R\* - Boulder Height to Width Ratio)

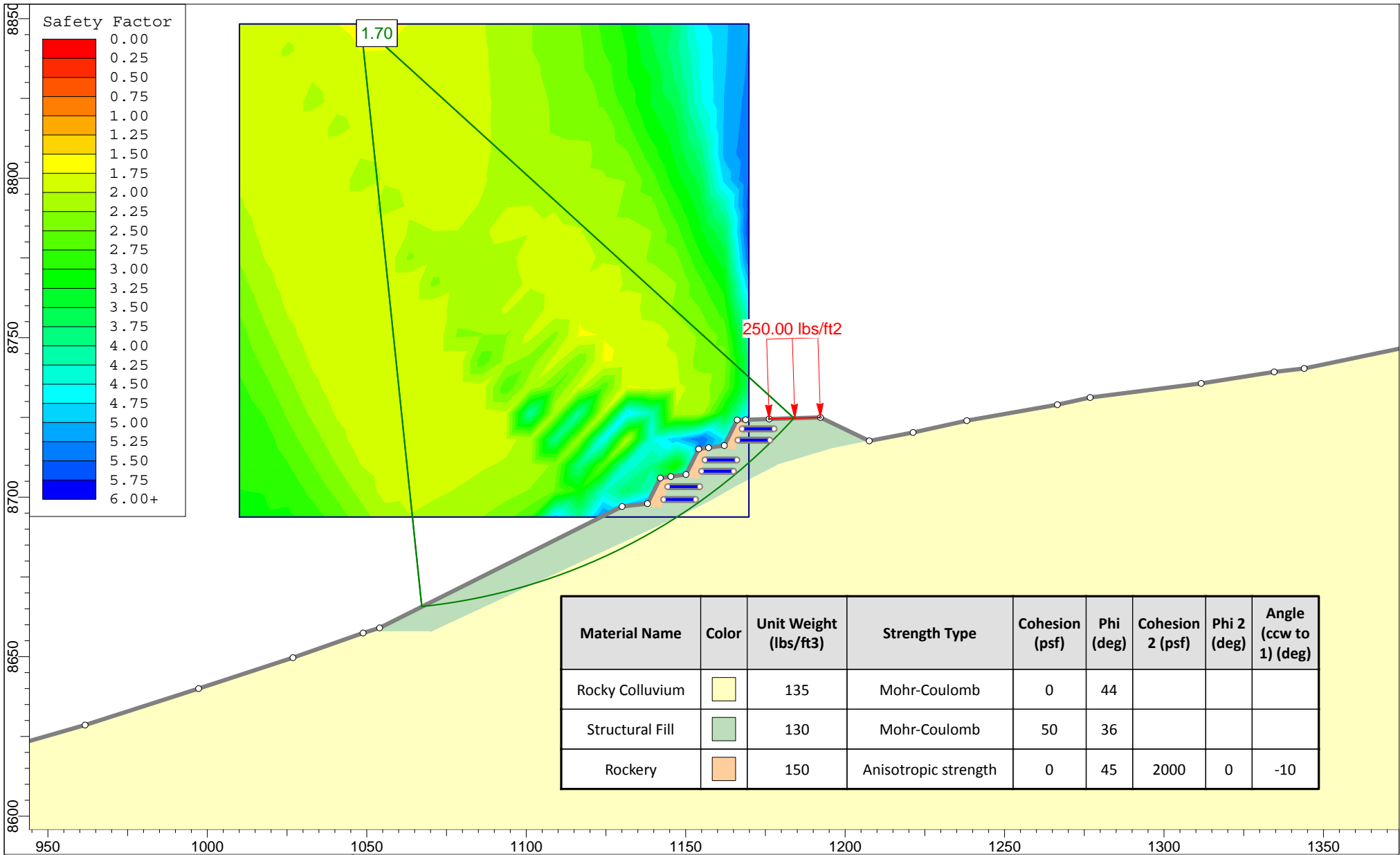
| Boulder | B' (ft) | R*  | H <sub>R</sub> (ft) | H-H' (ft) | $\Sigma W_i$ | $\Sigma W_i * x_i$ | F <sub>H</sub> | F <sub>H,s</sub> | F <sub>u</sub> | F <sub>u,s</sub> | M <sub>o</sub> | M <sub>o,s</sub> | M <sub>r</sub> | M <sub>r,s</sub> | FS <sub>SL</sub> | FS <sub>OT</sub> | FS <sub>SL,s</sub> | FS <sub>OT,s</sub> |
|---------|---------|-----|---------------------|-----------|--------------|--------------------|----------------|------------------|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|--------------------|--------------------|
| 1       | 4.0     | 0.7 | 2.8                 | 7.0       | 3,636        | 11,672             | 1,087          | 1,693            | 2,676          | 2,725            | 3,789          | 6,046            | 12,558         | 12,874           | 2.7              | 3.3              | 1.8                | 2.1                |
| 2       | 3.5     | 0.7 | 2.45                | 4.6       | 2,061        | 7,492              | 566            | 876              | 1,177          | 1,193            | 1,090          | 2,417            | 7,783          | 7,897            | 2.1              | 7.1              | 1.4                | 3.3                |
| 3       | 3.0     | 0.7 | 2.1                 | 2.1       | 866          | 3,595              | 197            | 307              | 486            | 489              | 187            | 777              | 3,647          | 3,667            | 2.5              | 19.5             | 1.6                | 4.7                |
| 4       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 5       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 6       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 7       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |
| 8       | 0.0     | 0.0 | 0.0                 | N/A       | 0            | 0                  | N/A            | N/A              | 0              | N/A              | N/A            | N/A              | N/A            | N/A              | N/A              | N/A              | N/A                | N/A                |

**7.4** Total Estimated Height of Rockery

(See Mack, et. al [2006], Rockery Design and Construction Guidelines, Report No. FHWA-CFL/TD-06-006, Report Dated November 2006 - for term definitions and equations)



## **SECTION 2.2**



| Material Name   | Color | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|-------|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |       | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |       | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |       | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |

|  |   |                                 |                              |
|--|---|---------------------------------|------------------------------|
|  | <i>Project</i><br><b>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G</b>                   |                                 |                              |
|  | <i>Analysis Description</i><br><b>GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 1-1'</b> |                                 |                              |
|  | <i>Drawn By</i><br>SL   | <i>Scale</i><br>1:500           | <i>Company</i><br>IGES, INC. |
|  | <i>Date</i><br>9-25-2015  | <i>File Name</i><br>Static.slim |                              |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m\alpha < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---




1 Distributed Load present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Support Properties


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### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent

Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material  | Adhesion (psf) | Friction Angle (deg) |
|---|----------------|----------------------|
|  Structural Fill | 50             | 36                   |

**Global Minimums**

---

**Method: spencer**

FS: 1.703070  
 Center: 1048.112, 8848.310  
 Radius: 183.664  
 Left Slip Surface Endpoint: 1067.248, 8665.645  
 Right Slip Surface Endpoint: 1183.995, 8724.745  
 Resisting Moment=2.28096e+007 lb-ft  
 Driving Moment=1.33932e+007 lb-ft  
 Resisting Horizontal Force=109008 lb  
 Driving Horizontal Force=64006.8 lb  
 Total Slice Area=1175.56 ft<sup>2</sup>

**Valid / Invalid Surfaces**

---

**Method: spencer**

Number of Valid Surfaces: 4286  
 Number of Invalid Surfaces: 554

**Error Codes:**

Error Code -103 reported for 60 surfaces  
 Error Code -106 reported for 5 surfaces  
 Error Code -108 reported for 116 surfaces  
 Error Code -111 reported for 272 surfaces  
 Error Code -112 reported for 101 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).

-111 = safety factor equation did not converge

-112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

### Global Minimum Query (spencer) - Safety Factor: 1.70307

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 4.91546    | 599.858      | Structural Fill | 50                  | 36                            | 94.251             | 160.516              | 152.112                  | 0                   | 152.112                       |
| 2            | 4.91546    | 1756.43      | Structural Fill | 50                  | 36                            | 202.268            | 344.477              | 405.314                  | 0                   | 405.314                       |
| 3            | 4.91546    | 2826.19      | Structural Fill | 50                  | 36                            | 296.032            | 504.164              | 625.102                  | 0                   | 625.102                       |
| 4            | 4.91546    | 3808.02      | Structural Fill | 50                  | 36                            | 376.502            | 641.21               | 813.731                  | 0                   | 813.731                       |
| 5            | 4.91546    | 4700.54      | Structural Fill | 50                  | 36                            | 444.525            | 757.057              | 973.182                  | 0                   | 973.182                       |
| 6            | 4.91546    | 5502.15      | Structural Fill | 50                  | 36                            | 500.849            | 852.981              | 1105.21                  | 0                   | 1105.21                       |
| 7            | 4.91546    | 6210.99      | Structural Fill | 50                  | 36                            | 546.137            | 930.109              | 1211.37                  | 0                   | 1211.37                       |
| 8            | 4.64238    | 6439.98      | Rocky Colluvium | 0                   | 44                            | 751.396            | 1279.68              | 1325.15                  | 0                   | 1325.15                       |
| 9            | 4.64238    | 6919.81      | Rocky Colluvium | 0                   | 44                            | 782.839            | 1333.23              | 1380.6                   | 0                   | 1380.6                        |
| 10           | 4.64238    | 7312.19      | Rocky Colluvium | 0                   | 44                            | 802.134            | 1366.09              | 1414.63                  | 0                   | 1414.63                       |
| 11           | 4.64238    | 7614.53      | Rocky Colluvium | 0                   | 44                            | 809.949            | 1379.4               | 1428.41                  | 0                   | 1428.41                       |
| 12           | 4.64238    | 7823.87      | Rocky Colluvium | 0                   | 44                            | 806.884            | 1374.18              | 1423                     | 0                   | 1423                          |
| 13           | 4.64238    | 7936.86      | Rocky Colluvium | 0                   | 44                            | 793.473            | 1351.34              | 1399.35                  | 0                   | 1399.35                       |
| 14           | 4.64238    | 7530.43      | Rocky Colluvium | 0                   | 44                            | 729.588            | 1242.54              | 1286.69                  | 0                   | 1286.69                       |
| 15           | 4.64238    | 6469.13      | Rocky Colluvium | 0                   | 44                            | 607.174            | 1034.06              | 1070.8                   | 0                   | 1070.8                        |
| 16           | 4.64238    | 8973.17      | Rocky Colluvium | 0                   | 44                            | 815.474            | 1388.81              | 1438.15                  | 0                   | 1438.15                       |
| 17           | 4.64238    | 8413.92      | Rocky Colluvium | 0                   | 44                            | 739.928            | 1260.15              | 1304.92                  | 0                   | 1304.92                       |
| 18           | 4.48943    | 7580.95      | Structural Fill | 50                  | 36                            | 536.428            | 913.574              | 1188.61                  | 0                   | 1188.61                       |
| 19           | 4.48943    | 9809.03      | Structural Fill | 50                  | 36                            | 666.25             | 1134.67              | 1492.92                  | 0                   | 1492.92                       |
| 20           | 4.48943    | 7956.1       | Structural Fill | 50                  | 36                            | 529.666            | 902.058              | 1172.76                  | 0                   | 1172.76                       |
| 21           | 4.48943    | 8482.76      | Structural Fill | 50                  | 36                            | 545.709            | 929.38               | 1210.36                  | 0                   | 1210.36                       |
| 22           | 4.48943    | 8845.63      | Structural Fill | 50                  | 36                            | 549.723            | 936.216              | 1219.77                  | 0                   | 1219.77                       |
| 23           | 4.48943    | 6381.05      | Structural Fill | 50                  | 36                            | 390.598            | 665.216              | 846.772                  | 0                   | 846.772                       |
| 24           | 4.48943    | 3953.67      | Structural Fill | 50                  | 36                            | 289.719            | 493.411              | 610.303                  | 0                   | 610.303                       |
| 25           | 4.48943    | 1349.21      | Structural Fill | 50                  | 36                            | 156.031            | 265.731              | 296.928                  | 0                   | 296.928                       |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.70307

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 1067.25           | 8665.65                    | 0                             | 0                            | 0                                |
| 2            | 1072.16           | 8666.23                    | 375.276                       | 203.386                      | 28.4561                          |
| 3            | 1077.08           | 8666.94                    | 1080.01                       | 585.324                      | 28.456                           |
| 4            | 1081.99           | 8667.8                     | 2003.13                       | 1085.62                      | 28.456                           |
| 5            | 1086.91           | 8668.79                    | 3048.43                       | 1652.14                      | 28.4561                          |
| 6            | 1091.83           | 8669.92                    | 4133.11                       | 2240                         | 28.4561                          |
| 7            | 1096.74           | 8671.2                     | 5186.63                       | 2810.97                      | 28.4561                          |
| 8            | 1101.66           | 8672.62                    | 6149.7                        | 3332.92                      | 28.4561                          |
| 9            | 1106.3            | 8674.11                    | 7677.4                        | 4160.88                      | 28.4561                          |
| 10           | 1110.94           | 8675.73                    | 9079.12                       | 4920.56                      | 28.4561                          |
| 11           | 1115.58           | 8677.49                    | 10315.3                       | 5590.51                      | 28.4561                          |
| 12           | 1120.23           | 8679.4                     | 11355.1                       | 6154.04                      | 28.456                           |
| 13           | 1124.87           | 8681.45                    | 12176.2                       | 6599.06                      | 28.4561                          |
| 14           | 1129.51           | 8683.67                    | 12764.6                       | 6917.95                      | 28.4561                          |
| 15           | 1134.15           | 8686.05                    | 13095.9                       | 7097.52                      | 28.4561                          |
| 16           | 1138.8            | 8688.59                    | 13189.4                       | 7148.17                      | 28.4561                          |
| 17           | 1143.44           | 8691.32                    | 13058.1                       | 7077.03                      | 28.4561                          |
| 18           | 1148.08           | 8694.24                    | 12693.7                       | 6879.51                      | 28.456                           |
| 19           | 1152.57           | 8697.24                    | 11529.7                       | 6248.7                       | 28.4562                          |
| 20           | 1157.06           | 8700.45                    | 9739.39                       | 5278.4                       | 28.4561                          |
| 21           | 1161.55           | 8703.86                    | 8114.44                       | 4397.73                      | 28.4561                          |
| 22           | 1166.04           | 8707.5                     | 6159.84                       | 3338.41                      | 28.4561                          |
| 23           | 1170.53           | 8711.39                    | 3891.61                       | 2109.11                      | 28.4561                          |
| 24           | 1175.02           | 8715.54                    | 2132.76                       | 1155.88                      | 28.4561                          |
| 25           | 1179.51           | 8719.98                    | 750.193                       | 406.578                      | 28.4561                          |
| 26           | 1184              | 8724.74                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y      |
|---------|--------|
| 1192.24 | 8725   |
| 1176.19 | 8724.5 |

### External Boundary

| X       | Y      |
|---------|--------|
| 1176.19 | 8724.5 |

|         |         |
|---------|---------|
| 1168.79 | 8724.28 |
| 1166.15 | 8724.2  |
| 1162.13 | 8716.16 |
| 1157.2  | 8715.51 |
| 1154.09 | 8715.09 |
| 1150.1  | 8707.12 |
| 1145.36 | 8706.46 |
| 1142.04 | 8706.01 |
| 1138.02 | 8697.98 |
| 1130.07 | 8697.08 |
| 1054.01 | 8659.02 |
| 1048.84 | 8657.42 |
| 1026.85 | 8649.69 |
| 997.268 | 8640    |
| 961.646 | 8628.56 |
| 941.224 | 8622.71 |
| 918.085 | 8616.03 |
| 918.063 | 8511.08 |
| 1374.81 | 8511.08 |
| 1374.81 | 8746.76 |
| 1343.95 | 8740.33 |
| 1334.56 | 8739.27 |
| 1311.67 | 8735.66 |
| 1276.84 | 8731.24 |
| 1266.54 | 8728.99 |
| 1238.16 | 8723.97 |
| 1221.32 | 8720.27 |
| 1207.57 | 8717.63 |
| 1192.24 | 8725    |

### Material Boundary

| X       | Y       |
|---------|---------|
| 1054.01 | 8659.02 |
| 1054.98 | 8657.88 |
| 1069.98 | 8657.88 |
| 1149.54 | 8694.92 |
| 1157.71 | 8699    |
| 1166.21 | 8703.85 |
| 1178.29 | 8710    |
| 1189.81 | 8713.38 |
| 1195.91 | 8715.24 |
| 1207.57 | 8717.63 |

### Material Boundary

|  |  |
|--|--|
|  |  |
|--|--|



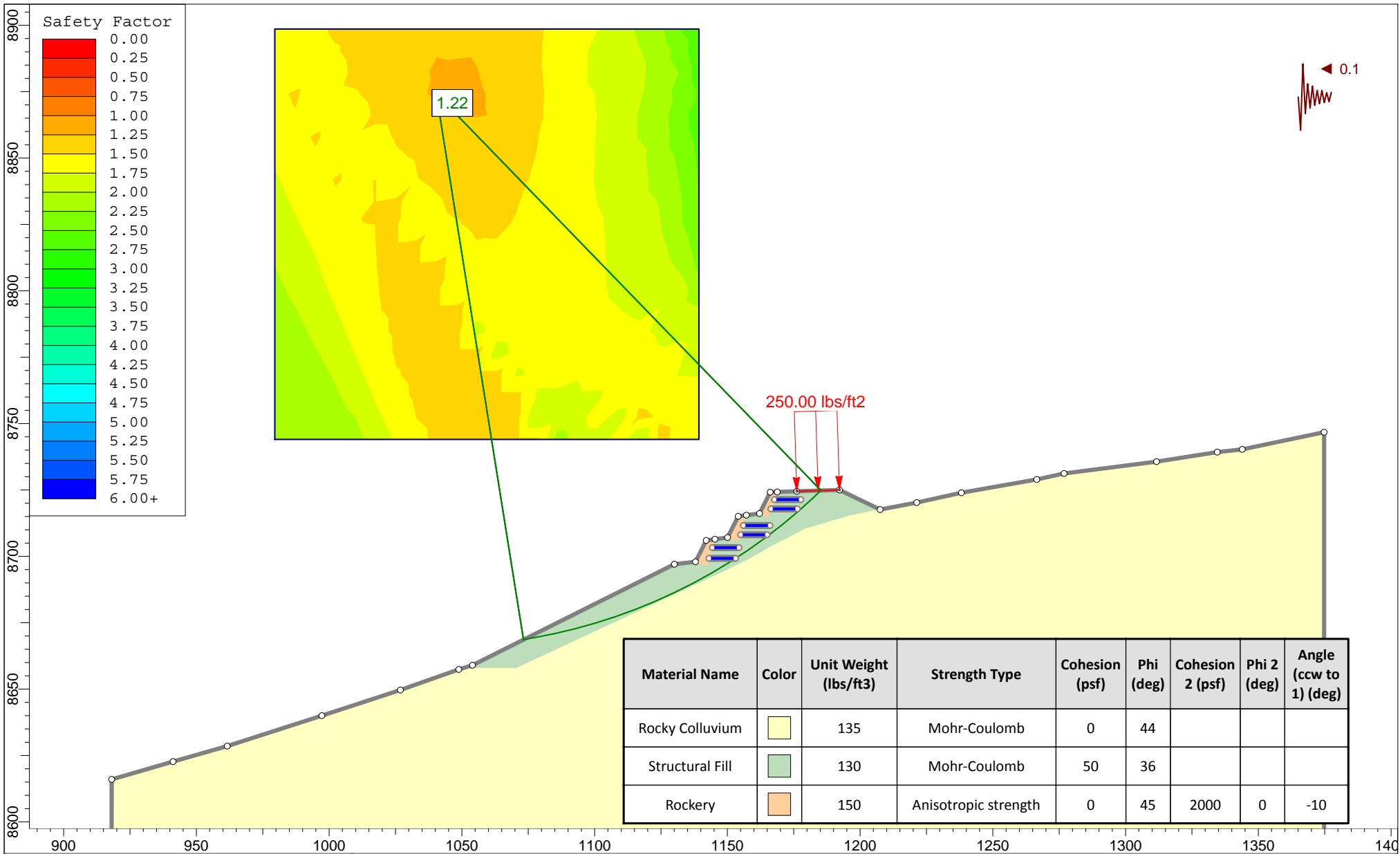
| X       | Y       |
|---------|---------|
| 1138.02 | 8697.98 |
| 1137.57 | 8697.09 |
| 1142.24 | 8696.61 |
| 1145.36 | 8706.46 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 1150.1  | 8707.12 |
| 1149.63 | 8706.17 |
| 1154.26 | 8705.59 |
| 1157.2  | 8715.51 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 1162.13 | 8716.16 |
| 1161.68 | 8715.27 |
| 1165.28 | 8714.88 |
| 1168.79 | 8724.28 |



|                             |           |              |       |  |               |  |  |
|-----------------------------|-----------|--------------|-------|--|---------------|--|--|
| <i>Project</i>              |           |              |       | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G       |               |  |  |
| <i>Analysis Description</i> |           |              |       | GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 1-1' |               |  |  |
| <i>Drawn By</i>             | SL        | <i>Scale</i> | 1:600 | <i>Company</i>   | IGES, INC.    |  |  |
| <i>Date</i>                 | 9-25-2015 |              |       | <i>File Name</i>   | P-static.slim |  |  |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: P-static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---




Seismic Load Coefficient (Horizontal): 0.1  
 1 Distributed Load present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Support Properties


---

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear

Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

#### Pullout Strength Dependency:

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

## Global Minimums

---

### Method: spencer

FS: 1.217890  
 Center: 1040.399, 8874.208  
 Radius: 208.176  
 Left Slip Surface Endpoint: 1073.227, 8668.637  
 Right Slip Surface Endpoint: 1185.349, 8724.787  
 Resisting Moment=1.81994e+007 lb-ft  
 Driving Moment=1.49433e+007 lb-ft  
 Resisting Horizontal Force=76656.7 lb  
 Driving Horizontal Force=62942.2 lb  
 Total Slice Area=967.383 ft<sup>2</sup>

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 4565  
 Number of Invalid Surfaces: 275

#### Error Codes:

Error Code -106 reported for 28 surfaces  
 Error Code -108 reported for 86 surfaces  
 Error Code -111 reported for 157 surfaces  
 Error Code -112 reported for 4 surfaces

#### Error Codes

The following errors were encountered during the computation:

- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep

seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.21789

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 4.4849     | 430.714      | Structural Fill | 50                  | 36                            | 120.775            | 147.091              | 133.634                  | 0                   | 133.634                       |
| 2            | 4.4849     | 1262.56      | Structural Fill | 50                  | 36                            | 239.611            | 291.82               | 332.836                  | 0                   | 332.836                       |
| 3            | 4.4849     | 2034.85      | Structural Fill | 50                  | 36                            | 342.393            | 416.997              | 505.129                  | 0                   | 505.129                       |
| 4            | 4.4849     | 2746.78      | Structural Fill | 50                  | 36                            | 430.254            | 524.002              | 652.408                  | 0                   | 652.408                       |
| 5            | 4.4849     | 3397.43      | Structural Fill | 50                  | 36                            | 504.222            | 614.087              | 776.4                    | 0                   | 776.4                         |
| 6            | 4.4849     | 3985.76      | Structural Fill | 50                  | 36                            | 565.232            | 688.391              | 878.668                  | 0                   | 878.668                       |
| 7            | 4.4849     | 4510.6       | Structural Fill | 50                  | 36                            | 614.135            | 747.949              | 960.645                  | 0                   | 960.645                       |
| 8            | 4.4849     | 4970.67      | Structural Fill | 50                  | 36                            | 651.708            | 793.709              | 1023.63                  | 0                   | 1023.63                       |
| 9            | 4.4849     | 5364.51      | Structural Fill | 50                  | 36                            | 678.662            | 826.536              | 1068.81                  | 0                   | 1068.81                       |
| 10           | 4.4849     | 5690.52      | Structural Fill | 50                  | 36                            | 695.651            | 847.226              | 1097.29                  | 0                   | 1097.29                       |
| 11           | 4.4849     | 5946.9       | Structural Fill | 50                  | 36                            | 703.273            | 856.509              | 1110.06                  | 0                   | 1110.06                       |
| 12           | 4.4849     | 6131.69      | Structural Fill | 50                  | 36                            | 702.081            | 855.057              | 1108.07                  | 0                   | 1108.07                       |
| 13           | 4.4849     | 6188.95      | Structural Fill | 50                  | 36                            | 687.016            | 836.71               | 1082.81                  | 0                   | 1082.81                       |
| 14           | 4.4849     | 5442.3       | Structural Fill | 50                  | 36                            | 591.384            | 720.241              | 922.507                  | 0                   | 922.507                       |
| 15           | 4.4849     | 5322.34      | Structural Fill | 50                  | 36                            | 561.923            | 684.36               | 873.12                   | 0                   | 873.12                        |
| 16           | 4.4849     | 7954.76      | Structural Fill | 50                  | 36                            | 792.956            | 965.733              | 1260.4                   | 0                   | 1260.4                        |
| 17           | 4.4849     | 6517.03      | Structural Fill | 50                  | 36                            | 637.255            | 776.107              | 999.4                    | 0                   | 999.4                         |
| 18           | 4.4849     | 7459.67      | Structural Fill | 50                  | 36                            | 700.665            | 853.333              | 1105.69                  | 0                   | 1105.69                       |
| 19           | 4.4849     | 8579.99      | Structural Fill | 50                  | 36                            | 774.194            | 942.883              | 1228.95                  | 0                   | 1228.95                       |
| 20           | 4.4849     | 6901.18      | Structural Fill | 50                  | 36                            | 610.616            | 743.663              | 954.744                  | 0                   | 954.744                       |
| 21           | 4.4849     | 8839.21      | Structural Fill | 50                  | 36                            | 745.394            | 907.808              | 1180.67                  | 0                   | 1180.67                       |
| 22           | 4.4849     | 7781.89      | Structural Fill | 50                  | 36                            | 639.015            | 778.25               | 1002.35                  | 0                   | 1002.35                       |
| 23           | 4.4849     | 5678.41      | Structural Fill | 50                  | 36                            | 464.677            | 565.926              | 710.111                  | 0                   | 710.111                       |
| 24           | 4.4849     | 3501.38      | Structural Fill | 50                  | 36                            | 377.004            | 459.149              | 563.145                  | 0                   | 563.145                       |
| 25           | 4.4849     | 1190.51      | Structural Fill | 50                  | 36                            | 204.159            | 248.643              | 273.409                  | 0                   | 273.409                       |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.21789

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 1073.23           | 8668.64                    | 0                             | 0                            | 0                                |
| 2            | 1077.71           | 8669.4                     | 397.097                       | 274.017                      | 34.6076                          |
| 3            | 1082.2            | 8670.27                    | 1058.43                       | 730.366                      | 34.6075                          |
| 4            | 1086.68           | 8671.24                    | 1902.82                       | 1313.04                      | 34.6076                          |
| 5            | 1091.17           | 8672.32                    | 2859.74                       | 1973.36                      | 34.6076                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 6  | 1095.65 | 8673.5  | 3868.35 | 2669.35 | 34.6076 |
| 7  | 1100.14 | 8674.79 | 4876.69 | 3365.15 | 34.6075 |
| 8  | 1104.62 | 8676.19 | 5840.99 | 4030.57 | 34.6076 |
| 9  | 1109.11 | 8677.7  | 6725.06 | 4640.62 | 34.6076 |
| 10 | 1113.59 | 8679.32 | 7499.76 | 5175.2  | 34.6076 |
| 11 | 1118.08 | 8681.07 | 8142.62 | 5618.8  | 34.6075 |
| 12 | 1122.56 | 8682.93 | 8637.47 | 5960.28 | 34.6076 |
| 13 | 1127.05 | 8684.92 | 8974.16 | 6192.6  | 34.6075 |
| 14 | 1131.53 | 8687.04 | 9148.46 | 6312.88 | 34.6076 |
| 15 | 1136.02 | 8689.29 | 9184.62 | 6337.84 | 34.6076 |
| 16 | 1140.5  | 8691.68 | 9091.18 | 6273.36 | 34.6076 |
| 17 | 1144.99 | 8694.21 | 8666.57 | 5980.36 | 34.6076 |
| 18 | 1149.47 | 8696.89 | 8197.69 | 5656.8  | 34.6075 |
| 19 | 1153.95 | 8699.73 | 7461.4  | 5148.73 | 34.6076 |
| 20 | 1158.44 | 8702.73 | 6391.8  | 4410.65 | 34.6075 |
| 21 | 1162.92 | 8705.91 | 5413.29 | 3735.43 | 34.6075 |
| 22 | 1167.41 | 8709.27 | 3913.04 | 2700.19 | 34.6076 |
| 23 | 1171.89 | 8712.82 | 2444.61 | 1686.9  | 34.6076 |
| 24 | 1176.38 | 8716.58 | 1295.62 | 894.038 | 34.6075 |
| 25 | 1180.86 | 8720.56 | 431.144 | 297.51  | 34.6075 |
| 26 | 1185.35 | 8724.79 | 0       | 0       | 0       |

## List Of Coordinates

---

### Distributed Load

| X       | Y      |
|---------|--------|
| 1192.24 | 8725   |
| 1176.19 | 8724.5 |

### External Boundary

| X       | Y       |
|---------|---------|
| 1176.19 | 8724.5  |
| 1168.79 | 8724.28 |
| 1166.15 | 8724.2  |
| 1162.13 | 8716.16 |
| 1157.2  | 8715.51 |
| 1154.09 | 8715.09 |
| 1150.1  | 8707.12 |
| 1145.36 | 8706.46 |
| 1142.04 | 8706.01 |
| 1138.02 | 8697.98 |
| 1130.07 | 8697.08 |
| 1054.01 | 8659.02 |
| 1048.84 | 8657.42 |

|         |         |
|---------|---------|
| 1026.85 | 8649.69 |
| 997.268 | 8640    |
| 961.646 | 8628.56 |
| 941.224 | 8622.71 |
| 918.085 | 8616.03 |
| 918.063 | 8511.08 |
| 1374.81 | 8511.08 |
| 1374.81 | 8746.76 |
| 1343.95 | 8740.33 |
| 1334.56 | 8739.27 |
| 1311.67 | 8735.66 |
| 1276.84 | 8731.24 |
| 1266.54 | 8728.99 |
| 1238.16 | 8723.97 |
| 1221.32 | 8720.27 |
| 1207.57 | 8717.63 |
| 1192.24 | 8725    |

### Material Boundary

| X       | Y       |
|---------|---------|
| 1054.01 | 8659.02 |
| 1054.98 | 8657.88 |
| 1069.98 | 8657.88 |
| 1149.54 | 8694.92 |
| 1157.71 | 8699    |
| 1166.21 | 8703.85 |
| 1178.29 | 8710    |
| 1189.81 | 8713.38 |
| 1195.91 | 8715.24 |
| 1207.57 | 8717.63 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 1138.02 | 8697.98 |
| 1137.57 | 8697.09 |
| 1142.24 | 8696.61 |
| 1145.36 | 8706.46 |

### Material Boundary

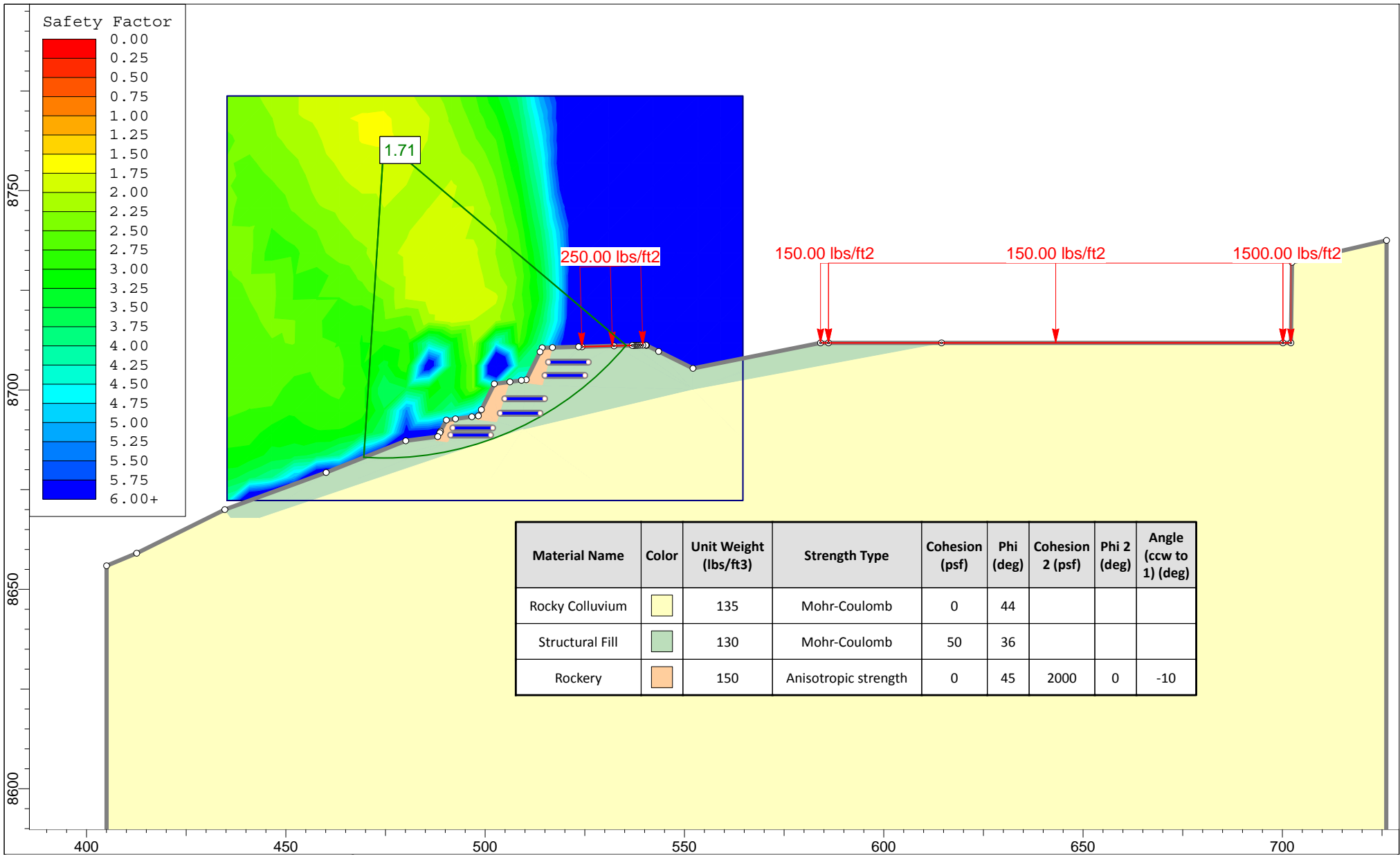
| X       | Y       |
|---------|---------|
| 1150.1  | 8707.12 |
| 1149.63 | 8706.17 |
| 1154.26 | 8705.59 |



|        |         |
|--------|---------|
| 1157.2 | 8715.51 |
|--------|---------|

### Material Boundary

| X       | Y       |
|---------|---------|
| 1162.13 | 8716.16 |
| 1161.68 | 8715.27 |
| 1165.28 | 8714.88 |
| 1168.79 | 8724.28 |



|  |                      |           |           |   |         |            |
|--|----------------------|-----------|-----------|---|---------|------------|
|  | Project              |           |           | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G      |         |            |
|  | Analysis Description |           |           | GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 2-2' |         |            |
|  | Drawn By             | SL        | Scale     | 1:400   | Company | IGES, INC. |
|  | Date                 | 9-25-2015 | File Name | Static.slim   |         |            |

## ***Slide Analysis Information***

### ***SLIDE - An Interactive Slope Stability Program***

#### ***Project Summary***

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File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

#### ***General Settings***

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Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

#### ***Analysis Options***

---

##### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

#### ***Groundwater Analysis***

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

#### ***Random Numbers***

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

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Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

4 Distributed Loads present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 150  
 Orientation: Normal to boundary

### Distributed Load 3




Distribution: Constant  
 Magnitude [psf]: 150  
 Orientation: Normal to boundary

### Distributed Load 4

Distribution: Constant  
 Magnitude [psf]: 1500  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |

|                        |      |      |      |
|------------------------|------|------|------|
| Friction Angle 1 [deg] |      |      | 45   |
| Friction Angle 2 [deg] |      |      | 0    |
| Angle from 1 [deg]     |      |      | -10  |
| Water Surface          | None | None | None |
| Ru Value               | 0    | 0    | 0    |


## Support Properties

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### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

#### Pullout Strength Dependency:

| Material  | Adhesion (psf) | Friction Angle (deg) |
|---|----------------|----------------------|
|  Structural Fill | 50             | 36                   |

## Global Minimums

---

### Method: spencer

FS: 1.707330  
 Center: 474.649, 8762.474  
 Radius: 79.553  
 Left Slip Surface Endpoint: 469.575, 8683.083  
 Right Slip Surface Endpoint: 535.423, 8711.139  
 Resisting Moment=4.26176e+006 lb-ft  
 Driving Moment=2.49615e+006 lb-ft  
 Resisting Horizontal Force=47569.1 lb  
 Driving Horizontal Force=27861.7 lb  
 Total Slice Area=531.088 ft<sup>2</sup>

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 3528  
 Number of Invalid Surfaces: 1488

**Error Codes:**

Error Code -103 reported for 7 surfaces  
 Error Code -105 reported for 1 surface  
 Error Code -106 reported for 15 surfaces  
 Error Code -107 reported for 141 surfaces  
 Error Code -108 reported for 130 surfaces  
 Error Code -109 reported for 2 surfaces  
 Error Code -111 reported for 277 surfaces  
 Error Code -112 reported for 915 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 105 = More than two surface / slope intersections with no valid slip surface.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 109 = Soiltype for slice base not located. This error should occur very rarely, if at all. It may occur if a very low number of slices is combined with certain soil geometries, such that the midpoint of a slice base is actually outside the soil region, even though the slip surface is wholly within the soil region.
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-}\alpha = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

**Global Minimum Query (spencer) - Safety Factor: 1.70733**

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.6339     | 200.509      | Structural Fill | 50                  | 36                            | 78.6656            | 134.308              | 116.04                   | 0                   | 116.04                        |
| 2            | 2.6339     | 586.572      | Structural Fill | 50                  | 36                            | 154.089            | 263.08               | 293.28                   | 0                   | 293.28                        |
| 3            | 2.6339     | 942.745      | Structural Fill | 50                  | 36                            | 218.694            | 373.383              | 445.096                  | 0                   | 445.096                       |
| 4            | 2.6339     | 1269.02      | Structural Fill | 50                  | 36                            | 273.455            | 466.878              | 573.782                  | 0                   | 573.782                       |
| 5            | 2.6339     | 1443.54      | Structural Fill | 50                  | 36                            | 297.038            | 507.142              | 629.204                  | 0                   | 629.204                       |
| 6            | 2.6339     | 1468.45      | Structural Fill | 50                  | 36                            | 292.643            | 499.639              | 618.876                  | 0                   | 618.876                       |
| 7            | 2.6339     | 1465.59      | Structural Fill | 50                  | 36                            | 283.623            | 484.238              | 597.676                  | 0                   | 597.676                       |
| 8            | 2.6339     | 2332.45      | Structural Fill | 50                  | 36                            | 419.142            | 715.613              | 916.137                  | 0                   | 916.137                       |
| 9            | 2.6339     | 2804.23      | Structural Fill | 50                  | 36                            | 482.78             | 824.264              | 1065.68                  | 0                   | 1065.68                       |
| 10           | 2.6339     | 2585.23      | Structural Fill | 50                  | 36                            | 434.568            | 741.951              | 952.388                  | 0                   | 952.388                       |
| 11           | 2.6339     | 2470.28      | Structural Fill | 50                  | 36                            | 404.578            | 690.748              | 881.912                  | 0                   | 881.912                       |
| 12           | 2.6339     | 3513.94      | Structural Fill | 50                  | 36                            | 545.918            | 932.063              | 1214.05                  | 0                   | 1214.05                       |
| 13           | 2.6339     | 4957.13      | Structural Fill | 50                  | 36                            | 735.083            | 1255.03              | 1658.59                  | 0                   | 1658.59                       |

|    |        |         |                 |    |    |         |         |         |   |         |
|----|--------|---------|-----------------|----|----|---------|---------|---------|---|---------|
| 14 | 2.6339 | 4593.75 | Structural Fill | 50 | 36 | 662.942 | 1131.86 | 1489.05 | 0 | 1489.05 |
| 15 | 2.6339 | 4138.71 | Structural Fill | 50 | 36 | 582.04  | 993.735 | 1298.94 | 0 | 1298.94 |
| 16 | 2.6339 | 4136.88 | Structural Fill | 50 | 36 | 563.887 | 962.742 | 1256.28 | 0 | 1256.28 |
| 17 | 2.6339 | 5567.81 | Structural Fill | 50 | 36 | 725.302 | 1238.33 | 1635.6  | 0 | 1635.6  |
| 18 | 2.6339 | 5822.29 | Structural Fill | 50 | 36 | 732.536 | 1250.68 | 1652.59 | 0 | 1652.59 |
| 19 | 2.6339 | 5038.24 | Structural Fill | 50 | 36 | 616.284 | 1052.2  | 1379.41 | 0 | 1379.41 |
| 20 | 2.6339 | 4442.58 | Structural Fill | 50 | 36 | 527.719 | 900.99  | 1171.29 | 0 | 1171.29 |
| 21 | 2.6339 | 3791.21 | Structural Fill | 50 | 36 | 453.346 | 774.011 | 996.514 | 0 | 996.514 |
| 22 | 2.6339 | 3078.68 | Structural Fill | 50 | 36 | 416.454 | 711.024 | 909.822 | 0 | 909.822 |
| 23 | 2.6339 | 2298.18 | Structural Fill | 50 | 36 | 321.688 | 549.227 | 687.128 | 0 | 687.128 |
| 24 | 2.6339 | 1441.06 | Structural Fill | 50 | 36 | 226.079 | 385.991 | 462.454 | 0 | 462.454 |
| 25 | 2.6339 | 496.065 | Structural Fill | 50 | 36 | 129.571 | 221.221 | 235.665 | 0 | 235.665 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.70733

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 469.575           | 8683.08                    | 0                             | 0                            | 0                                |
| 2            | 472.209           | 8682.96                    | 221.804                       | 98.2702                      | 23.8957                          |
| 3            | 474.843           | 8682.92                    | 638.868                       | 283.05                       | 23.8957                          |
| 4            | 477.477           | 8682.97                    | 1193.04                       | 528.577                      | 23.8958                          |
| 5            | 480.111           | 8683.11                    | 1834.98                       | 812.984                      | 23.8956                          |
| 6            | 482.745           | 8683.33                    | 2476.18                       | 1097.07                      | 23.8957                          |
| 7            | 485.379           | 8683.65                    | 3053.29                       | 1352.76                      | 23.8957                          |
| 8            | 488.013           | 8684.05                    | 3559.69                       | 1577.12                      | 23.8957                          |
| 9            | 490.646           | 8684.55                    | 4211.35                       | 1865.84                      | 23.8958                          |
| 10           | 493.28            | 8685.13                    | 4857.89                       | 2152.28                      | 23.8957                          |
| 11           | 495.914           | 8685.82                    | 5353.47                       | 2371.85                      | 23.8957                          |
| 12           | 498.548           | 8686.6                     | 5732.11                       | 2539.61                      | 23.8957                          |
| 13           | 501.182           | 8687.48                    | 6102.22                       | 2703.58                      | 23.8957                          |
| 14           | 503.816           | 8688.46                    | 6406.86                       | 2838.55                      | 23.8957                          |
| 15           | 506.45            | 8689.55                    | 6526.91                       | 2891.74                      | 23.8957                          |
| 16           | 509.084           | 8690.76                    | 6494.32                       | 2877.3                       | 23.8957                          |
| 17           | 511.718           | 8692.08                    | 6315.68                       | 2798.16                      | 23.8957                          |
| 18           | 514.352           | 8693.54                    | 5853.71                       | 2593.48                      | 23.8957                          |
| 19           | 516.985           | 8695.12                    | 5164.46                       | 2288.11                      | 23.8957                          |
| 20           | 519.619           | 8696.85                    | 4403.45                       | 1950.95                      | 23.8958                          |
| 21           | 522.253           | 8698.74                    | 3586.69                       | 1589.08                      | 23.8957                          |
| 22           | 524.887           | 8700.79                    | 2737.68                       | 1212.93                      | 23.8958                          |
| 23           | 527.521           | 8703.03                    | 1812.3                        | 802.938                      | 23.8957                          |
| 24           | 530.155           | 8705.48                    | 992.447                       | 439.703                      | 23.8957                          |
| 25           | 532.789           | 8708.17                    | 361.388                       | 160.113                      | 23.8957                          |
| 26           | 535.423           | 8711.14                    | 0                             | 0                            | 0                                |

## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 539.566 | 8711.25 |
| 538.921 | 8711.23 |
| 538.381 | 8711.22 |
| 537.923 | 8711.2  |
| 537.53  | 8711.19 |
| 537.188 | 8711.18 |
| 536.888 | 8711.18 |
| 532.333 | 8711.06 |
| 524.325 | 8710.85 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 586.154 | 8711.81 |
| 584.154 | 8711.81 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 700.154 | 8711.81 |
| 614.503 | 8711.81 |
| 586.154 | 8711.81 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 702.154 | 8711.81 |
| 700.154 | 8711.81 |

### External Boundary

| X       | Y       |
|---------|---------|
| 480.098 | 8687.26 |
| 460.119 | 8679.32 |
| 434.697 | 8670    |
| 412.587 | 8659.07 |
| 405.046 | 8655.94 |
| 405.046 | 8531.43 |
| 726.028 | 8531.43 |
| 726.153 | 8737.51 |
| 702.425 | 8732.02 |



|         |         |
|---------|---------|
| 702.154 | 8711.81 |
| 700.154 | 8711.81 |
| 614.503 | 8711.81 |
| 586.154 | 8711.81 |
| 584.154 | 8711.81 |
| 552.154 | 8705.43 |
| 543.525 | 8709.69 |
| 540.491 | 8711.19 |
| 540.34  | 8711.27 |
| 539.566 | 8711.25 |
| 538.921 | 8711.23 |
| 538.381 | 8711.22 |
| 537.923 | 8711.2  |
| 537.53  | 8711.19 |
| 537.188 | 8711.18 |
| 536.888 | 8711.18 |
| 532.333 | 8711.06 |
| 524.325 | 8710.85 |
| 523.452 | 8710.83 |
| 516.903 | 8710.66 |
| 514.316 | 8710.6  |
| 513.799 | 8709.56 |
| 510.312 | 8702.58 |
| 509.115 | 8702.42 |
| 506.237 | 8702.04 |
| 502.304 | 8701.53 |
| 499.073 | 8695.06 |
| 498.3   | 8693.51 |
| 496.671 | 8693.3  |
| 492.566 | 8692.76 |
| 490.293 | 8692.46 |
| 488.823 | 8689.65 |
| 488.635 | 8689.29 |
| 488.119 | 8688.31 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 488.119 | 8688.31 |
| 487.655 | 8687.37 |
| 490.86  | 8686.94 |
| 492.566 | 8692.76 |

### Material Boundary

| X | Y |
|---|---|
|---|---|

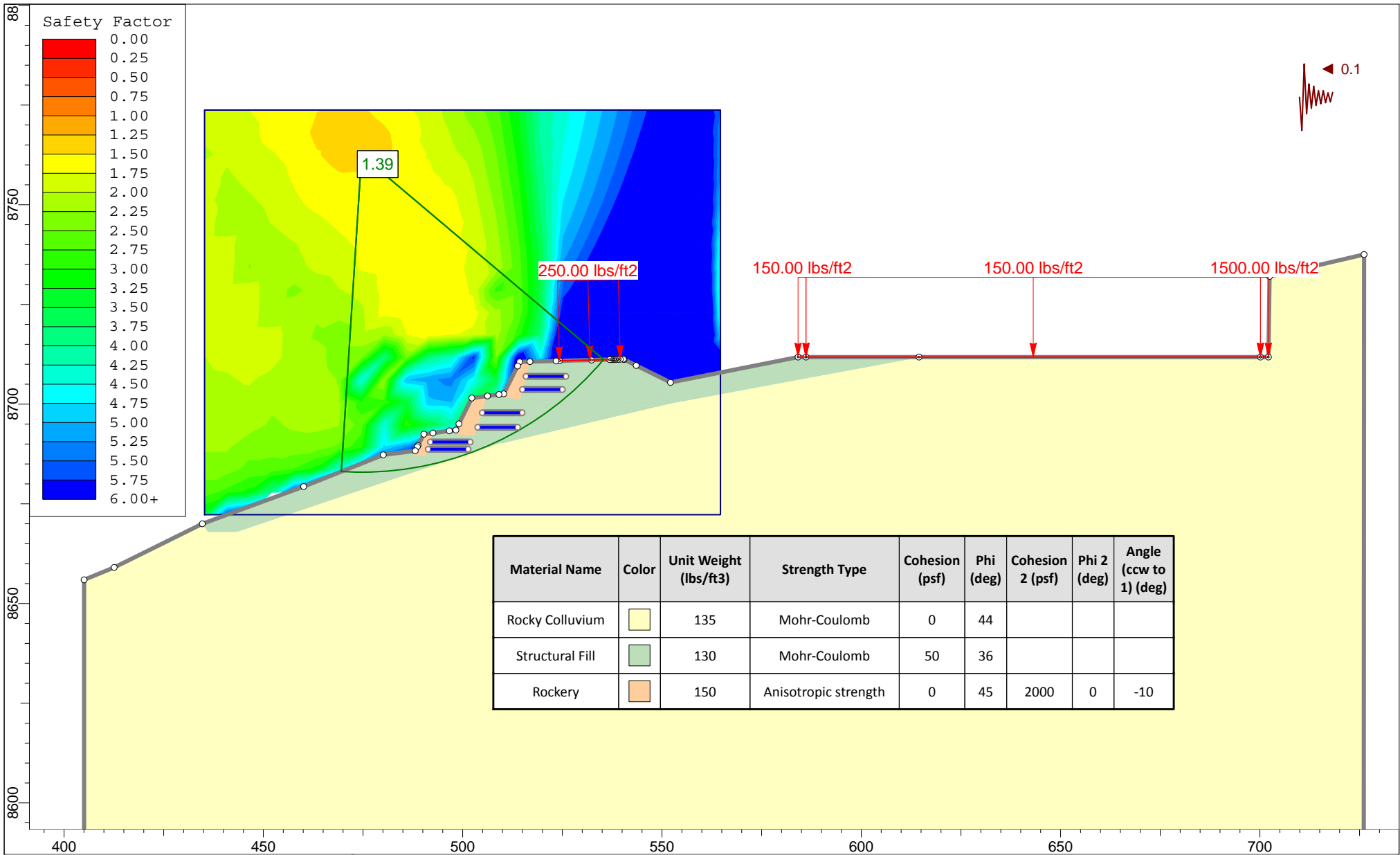
|         |         |
|---------|---------|
| 498.3   | 8693.51 |
| 497.854 | 8692.61 |
| 503.091 | 8692.02 |
| 506.237 | 8702.04 |


### Material Boundary

| X       | Y       |
|---------|---------|
| 510.312 | 8702.58 |
| 509.865 | 8701.68 |
| 514.323 | 8701.1  |
| 516.903 | 8710.66 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 434.697 | 8670    |
| 436.308 | 8667.85 |
| 443.393 | 8667.85 |
| 509.561 | 8690.19 |
| 551.948 | 8700.19 |
| 614.503 | 8711.81 |



|  |   |                                   |                              |
|--|---|-----------------------------------|------------------------------|
|  | <b>Project</b><br>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G                    |                                   |                              |
|  | <b>Analysis Description</b><br>GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 2-2' |                                   |                              |
|  | <b>Drawn By</b><br>SL   | <b>Scale</b><br>1:400             | <b>Company</b><br>IGES, INC. |
|  | <b>Date</b><br>9-25-2015  | <b>File Name</b><br>P-Static.slim |                              |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 4 Distributed Loads present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 150  
 Orientation: Normal to boundary

### Distributed Load 3




Distribution: Constant  
 Magnitude [psf]: 150  
 Orientation: Normal to boundary

### Distributed Load 4

Distribution: Constant  
 Magnitude [psf]: 1500  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |


|                        |      |      |      |
|------------------------|------|------|------|
| Cohesion 2 [psf]       |      |      | 2000 |
| Friction Angle 1 [deg] |      |      | 45   |
| Friction Angle 2 [deg] |      |      | 0    |
| Angle from 1 [deg]     |      |      | -10  |
| Water Surface          | None | None | None |
| Ru Value               | 0    | 0    | 0    |

## Support Properties

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

#### Pullout Strength Dependency:

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

## Global Minimums

### Method: spencer

FS: 1.389560  
 Center: 474.649, 8762.474  
 Radius: 79.553  
 Left Slip Surface Endpoint: 469.575, 8683.083  
 Right Slip Surface Endpoint: 535.423, 8711.139  
 Resisting Moment=4.1106e+006 lb-ft  
 Driving Moment=2.95819e+006 lb-ft  
 Resisting Horizontal Force=46117.2 lb  
 Driving Horizontal Force=33188.2 lb  
 Total Slice Area=531.088 ft<sup>2</sup>

## Valid / Invalid Surfaces

### Method: spencer

Number of Valid Surfaces: 3206  
 Number of Invalid Surfaces: 1810

**Error Codes:**

Error Code -103 reported for 7 surfaces  
 Error Code -105 reported for 1 surface  
 Error Code -106 reported for 15 surfaces  
 Error Code -107 reported for 83 surfaces  
 Error Code -108 reported for 204 surfaces  
 Error Code -109 reported for 2 surfaces  
 Error Code -111 reported for 444 surfaces  
 Error Code -112 reported for 1054 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 105 = More than two surface / slope intersections with no valid slip surface.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 109 = Soiltype for slice base not located. This error should occur very rarely, if at all. It may occur if a very low number of slices is combined with certain soil geometries, such that the midpoint of a slice base is actually outside the soil region, even though the slip surface is wholly within the soil region.
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-}\alpha = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.38956

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.6339     | 200.509      | Structural Fill | 50                  | 36                            | 110.659            | 153.767              | 142.824                  | 0                   | 142.824                       |
| 2            | 2.6339     | 586.572      | Structural Fill | 50                  | 36                            | 210.805            | 292.926              | 334.359                  | 0                   | 334.359                       |
| 3            | 2.6339     | 942.745      | Structural Fill | 50                  | 36                            | 293.533            | 407.882              | 492.58                   | 0                   | 492.58                        |
| 4            | 2.6339     | 1269.02      | Structural Fill | 50                  | 36                            | 361.122            | 501.8                | 621.851                  | 0                   | 621.851                       |
| 5            | 2.6339     | 1443.54      | Structural Fill | 50                  | 36                            | 386.806            | 537.49               | 670.97                   | 0                   | 670.97                        |
| 6            | 2.6339     | 1468.45      | Structural Fill | 50                  | 36                            | 376.39             | 523.016              | 651.052                  | 0                   | 651.052                       |
| 7            | 2.6339     | 1465.59      | Structural Fill | 50                  | 36                            | 360.621            | 501.104              | 620.892                  | 0                   | 620.892                       |
| 8            | 2.6339     | 2332.45      | Structural Fill | 50                  | 36                            | 525.42             | 730.103              | 936.081                  | 0                   | 936.081                       |
| 9            | 2.6339     | 2804.23      | Structural Fill | 50                  | 36                            | 598.28             | 831.346              | 1075.43                  | 0                   | 1075.43                       |
| 10           | 2.6339     | 2585.23      | Structural Fill | 50                  | 36                            | 533.473            | 741.293              | 951.484                  | 0                   | 951.484                       |
| 11           | 2.6339     | 2470.28      | Structural Fill | 50                  | 36                            | 492.151            | 683.874              | 872.454                  | 0                   | 872.454                       |
| 12           | 2.6339     | 3513.94      | Structural Fill | 50                  | 36                            | 656.732            | 912.569              | 1187.22                  | 0                   | 1187.22                       |

|    |        |         |                 |    |    |         |         |         |   |         |
|----|--------|---------|-----------------|----|----|---------|---------|---------|---|---------|
| 13 | 2.6339 | 4957.13 | Structural Fill | 50 | 36 | 875.191 | 1216.13 | 1605.04 | 0 | 1605.04 |
| 14 | 2.6339 | 4593.75 | Structural Fill | 50 | 36 | 782.888 | 1087.87 | 1428.51 | 0 | 1428.51 |
| 15 | 2.6339 | 4138.71 | Structural Fill | 50 | 36 | 682.092 | 947.808 | 1235.73 | 0 | 1235.73 |
| 16 | 2.6339 | 4136.88 | Structural Fill | 50 | 36 | 655.567 | 910.949 | 1184.99 | 0 | 1184.99 |
| 17 | 2.6339 | 5567.81 | Structural Fill | 50 | 36 | 835.351 | 1160.77 | 1528.85 | 0 | 1528.85 |
| 18 | 2.6339 | 5822.29 | Structural Fill | 50 | 36 | 836.898 | 1162.92 | 1531.81 | 0 | 1531.81 |
| 19 | 2.6339 | 5038.24 | Structural Fill | 50 | 36 | 699.077 | 971.41  | 1268.21 | 0 | 1268.21 |
| 20 | 2.6339 | 4442.58 | Structural Fill | 50 | 36 | 594.329 | 825.856 | 1067.88 | 0 | 1067.88 |
| 21 | 2.6339 | 3791.21 | Structural Fill | 50 | 36 | 507.98  | 705.869 | 902.728 | 0 | 902.728 |
| 22 | 2.6339 | 3078.68 | Structural Fill | 50 | 36 | 466.813 | 648.665 | 823.991 | 0 | 823.991 |
| 23 | 2.6339 | 2298.18 | Structural Fill | 50 | 36 | 359.134 | 499.038 | 618.047 | 0 | 618.047 |
| 24 | 2.6339 | 1441.06 | Structural Fill | 50 | 36 | 252.383 | 350.702 | 413.882 | 0 | 413.882 |
| 25 | 2.6339 | 496.065 | Structural Fill | 50 | 36 | 146.764 | 203.938 | 211.878 | 0 | 211.878 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.38956

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 469.575           | 8683.08                    | 0                             | 0                            | 0                                |
| 2            | 472.209           | 8682.96                    | 289.658                       | 165.394                      | 29.7263                          |
| 3            | 474.843           | 8682.92                    | 799.542                       | 456.536                      | 29.7262                          |
| 4            | 477.477           | 8682.97                    | 1454.96                       | 830.78                       | 29.7263                          |
| 5            | 480.111           | 8683.11                    | 2195.24                       | 1253.48                      | 29.7263                          |
| 6            | 482.745           | 8683.33                    | 2920.13                       | 1667.39                      | 29.7263                          |
| 7            | 485.379           | 8683.65                    | 3561.85                       | 2033.81                      | 29.7263                          |
| 8            | 488.013           | 8684.05                    | 4116.05                       | 2350.25                      | 29.7262                          |
| 9            | 490.646           | 8684.55                    | 4805.87                       | 2744.14                      | 29.7263                          |
| 10           | 493.28            | 8685.13                    | 5471.99                       | 3124.49                      | 29.7262                          |
| 11           | 495.914           | 8685.82                    | 5971.53                       | 3409.73                      | 29.7263                          |
| 12           | 498.548           | 8686.6                     | 6342.41                       | 3621.5                       | 29.7263                          |
| 13           | 501.182           | 8687.48                    | 6678.24                       | 3813.26                      | 29.7263                          |
| 14           | 503.816           | 8688.46                    | 6911.07                       | 3946.2                       | 29.7262                          |
| 15           | 506.45            | 8689.55                    | 6955.77                       | 3971.73                      | 29.7263                          |
| 16           | 509.084           | 8690.76                    | 6850.75                       | 3911.76                      | 29.7263                          |
| 17           | 511.718           | 8692.08                    | 6595.96                       | 3766.28                      | 29.7263                          |
| 18           | 514.352           | 8693.54                    | 6024.01                       | 3439.7                       | 29.7263                          |
| 19           | 516.985           | 8695.12                    | 5220.93                       | 2981.13                      | 29.7262                          |
| 20           | 519.619           | 8696.85                    | 4368.13                       | 2494.19                      | 29.7262                          |
| 21           | 522.253           | 8698.74                    | 3478.89                       | 1986.44                      | 29.7263                          |
| 22           | 524.887           | 8700.79                    | 2588.58                       | 1478.07                      | 29.7262                          |
| 23           | 527.521           | 8703.03                    | 1681.51                       | 960.141                      | 29.7263                          |
| 24           | 530.155           | 8705.48                    | 900.685                       | 514.289                      | 29.7263                          |
| 25           | 532.789           | 8708.17                    | 326.041                       | 186.169                      | 29.7263                          |
| 26           | 535.423           | 8711.14                    | 0                             | 0                            | 0                                |



## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 539.566 | 8711.25 |
| 538.921 | 8711.23 |
| 538.381 | 8711.22 |
| 537.923 | 8711.2  |
| 537.53  | 8711.19 |
| 537.188 | 8711.18 |
| 536.888 | 8711.18 |
| 532.333 | 8711.06 |
| 524.325 | 8710.85 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 586.154 | 8711.81 |
| 584.154 | 8711.81 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 700.154 | 8711.81 |
| 614.503 | 8711.81 |
| 586.154 | 8711.81 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 702.154 | 8711.81 |
| 700.154 | 8711.81 |

### External Boundary

| X       | Y       |
|---------|---------|
| 480.098 | 8687.26 |
| 460.119 | 8679.32 |
| 434.697 | 8670    |
| 412.587 | 8659.07 |
| 405.046 | 8655.94 |
| 405.046 | 8531.43 |
| 726.028 | 8531.43 |
| 726.153 | 8737.51 |

|         |         |
|---------|---------|
| 702.425 | 8732.02 |
| 702.154 | 8711.81 |
| 700.154 | 8711.81 |
| 614.503 | 8711.81 |
| 586.154 | 8711.81 |
| 584.154 | 8711.81 |
| 552.154 | 8705.43 |
| 543.525 | 8709.69 |
| 540.491 | 8711.19 |
| 540.34  | 8711.27 |
| 539.566 | 8711.25 |
| 538.921 | 8711.23 |
| 538.381 | 8711.22 |
| 537.923 | 8711.2  |
| 537.53  | 8711.19 |
| 537.188 | 8711.18 |
| 536.888 | 8711.18 |
| 532.333 | 8711.06 |
| 524.325 | 8710.85 |
| 523.452 | 8710.83 |
| 516.903 | 8710.66 |
| 514.316 | 8710.6  |
| 513.799 | 8709.56 |
| 510.312 | 8702.58 |
| 509.115 | 8702.42 |
| 506.237 | 8702.04 |
| 502.304 | 8701.53 |
| 499.073 | 8695.06 |
| 498.3   | 8693.51 |
| 496.671 | 8693.3  |
| 492.566 | 8692.76 |
| 490.293 | 8692.46 |
| 488.823 | 8689.65 |
| 488.635 | 8689.29 |
| 488.119 | 8688.31 |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 488.119 | 8688.31 |
| 487.655 | 8687.37 |
| 490.86  | 8686.94 |
| 492.566 | 8692.76 |

**Material Boundary**

|  |  |
|--|--|
|  |  |
|--|--|

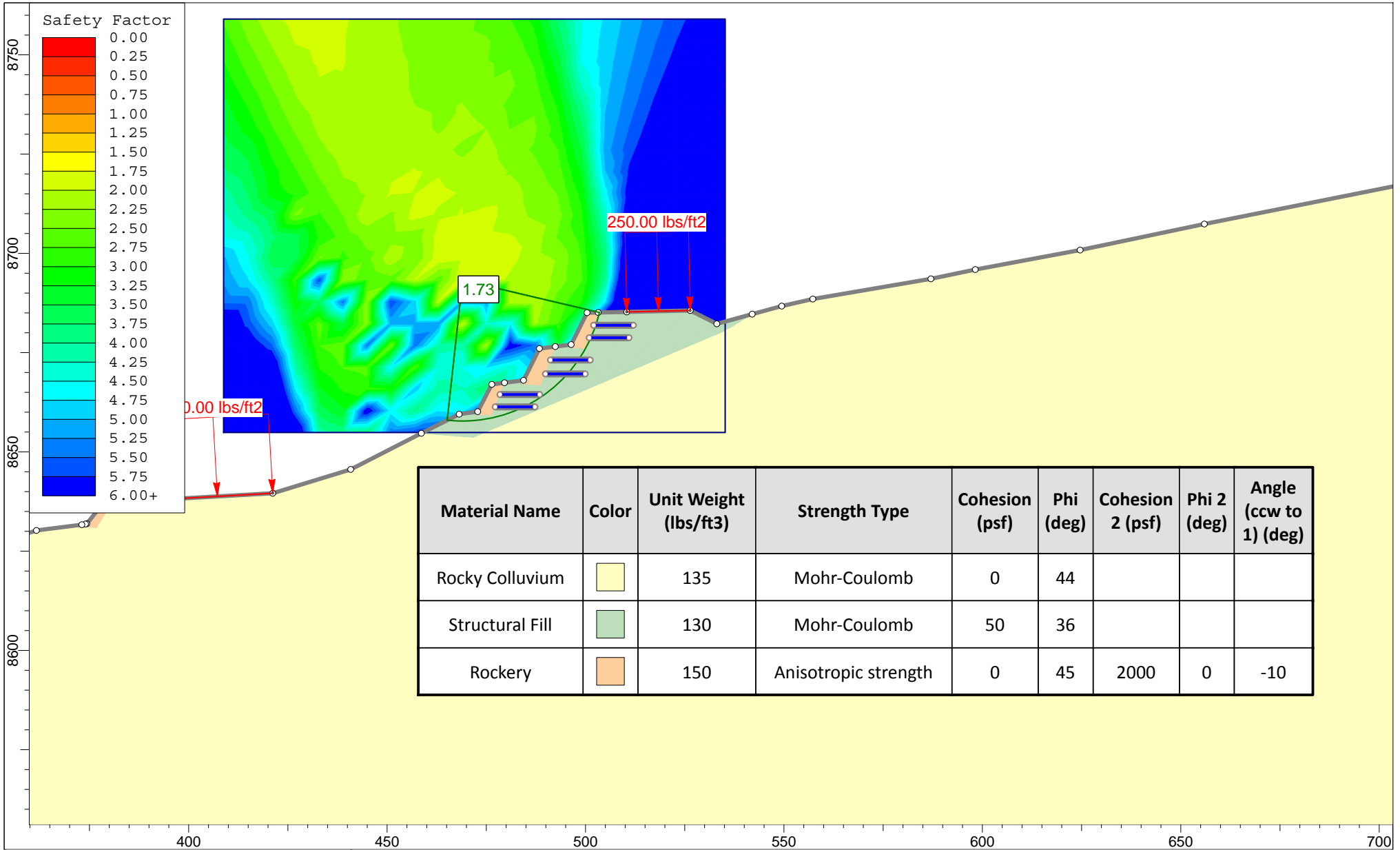
| X       | Y       |
|---------|---------|
| 498.3   | 8693.51 |
| 497.854 | 8692.61 |
| 503.091 | 8692.02 |
| 506.237 | 8702.04 |




### Material Boundary


| X       | Y       |
|---------|---------|
| 510.312 | 8702.58 |
| 509.865 | 8701.68 |
| 514.323 | 8701.1  |
| 516.903 | 8710.66 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 434.697 | 8670    |
| 436.308 | 8667.85 |
| 443.393 | 8667.85 |
| 509.561 | 8690.19 |
| 551.948 | 8700.19 |
| 614.503 | 8711.81 |



| Material Name   | Color   | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|---|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |    | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |   | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |  | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |

|  |                      |           |           |   |         |            |
|--|----------------------|-----------|-----------|---|---------|------------|
|  | Project              |           |           | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G      |         |            |
|  | Analysis Description |           |           | GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 3-3' |         |            |
|  | Drawn By             | SL        | Scale     | 1:400   | Company | IGES, INC. |
|  | Date                 | 9-25-2015 | File Name | Static.slim   |         |            |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m\alpha < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |


## Support Properties

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### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

**Global Minimums**

---

**Method: spencer**

FS: 1.728260  
 Center: 468.985, 8693.256  
 Radius: 35.494  
 Left Slip Surface Endpoint: 465.128, 8657.972  
 Right Slip Surface Endpoint: 503.534, 8685.117  
 Resisting Moment=1.11574e+006 lb-ft  
 Driving Moment=645588 lb-ft  
 Resisting Horizontal Force=28557.2 lb  
 Driving Horizontal Force=16523.7 lb  
 Total Slice Area=255.003 ft<sup>2</sup>

**Valid / Invalid Surfaces**

---

**Method: spencer**

Number of Valid Surfaces: 3871  
 Number of Invalid Surfaces: 969

**Error Codes:**

Error Code -103 reported for 496 surfaces  
 Error Code -107 reported for 30 surfaces  
 Error Code -108 reported for 66 surfaces  
 Error Code -111 reported for 125 surfaces  
 Error Code -112 reported for 252 surfaces

**Error Codes**

The following errors were encountered during the computation:

-103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between

them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.

-107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.

-108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).

-111 = safety factor equation did not converge

-112 = The coefficient  $M\text{-}\alpha = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.72826

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 1.53624    | 91.0256      | Structural Fill | 50                  | 36                            | 79.6193            | 137.603              | 120.575                  | 0                   | 120.575                       |
| 2            | 1.53624    | 266.354      | Structural Fill | 50                  | 36                            | 144.026            | 248.914              | 273.782                  | 0                   | 273.782                       |
| 3            | 1.53624    | 368.8        | Structural Fill | 50                  | 36                            | 174.05             | 300.804              | 345.202                  | 0                   | 345.202                       |
| 4            | 1.53624    | 404.091      | Structural Fill | 50                  | 36                            | 177.447            | 306.674              | 353.282                  | 0                   | 353.282                       |
| 5            | 1.53624    | 429.457      | Structural Fill | 50                  | 36                            | 177.178            | 306.21               | 352.642                  | 0                   | 352.642                       |
| 6            | 1.53624    | 774.534      | Structural Fill | 50                  | 36                            | 276.226            | 477.39               | 588.252                  | 0                   | 588.252                       |
| 7            | 1.53624    | 1417.42      | Structural Fill | 50                  | 36                            | 453.284            | 783.393              | 1009.43                  | 0                   | 1009.43                       |
| 8            | 1.53624    | 1869.07      | Structural Fill | 50                  | 36                            | 559.168            | 966.388              | 1261.3                   | 0                   | 1261.3                        |
| 9            | 1.53624    | 1755.73      | Structural Fill | 50                  | 36                            | 503.094            | 869.478              | 1127.91                  | 0                   | 1127.91                       |
| 10           | 1.53624    | 1608.49      | Structural Fill | 50                  | 36                            | 442.721            | 765.137              | 984.303                  | 0                   | 984.303                       |
| 11           | 1.53624    | 1532.18      | Structural Fill | 50                  | 36                            | 404.28             | 698.701              | 892.861                  | 0                   | 892.861                       |
| 12           | 1.53624    | 1449.56      | Structural Fill | 50                  | 36                            | 366.98             | 634.237              | 804.134                  | 0                   | 804.134                       |
| 13           | 1.53624    | 1442.97      | Structural Fill | 50                  | 36                            | 496.763            | 858.536              | 1112.86                  | 0                   | 1112.86                       |
| 14           | 1.53624    | 1915.15      | Structural Fill | 50                  | 36                            | 432.186            | 746.929              | 959.239                  | 0                   | 959.239                       |
| 15           | 1.53624    | 2449.95      | Structural Fill | 50                  | 36                            | 518.378            | 895.892              | 1164.27                  | 0                   | 1164.27                       |
| 16           | 1.53624    | 2694.54      | Structural Fill | 50                  | 36                            | 538.755            | 931.109              | 1212.75                  | 0                   | 1212.75                       |
|              |            |              | Structural      |                     |                               |                    |                      |                          |                     |                               |



|    |         |         |                    |    |    |         |         |         |   |         |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|
|    |         |         | Fill               |    |    |         |         |         |   |         |
| 18 | 1.53624 | 2076.52 | Structural<br>Fill | 50 | 36 | 377.339 | 652.14  | 828.773 | 0 | 828.773 |
| 19 | 1.53624 | 1803.38 | Structural<br>Fill | 50 | 36 | 311.413 | 538.203 | 671.952 | 0 | 671.952 |
| 20 | 1.53624 | 1528.34 | Structural<br>Fill | 50 | 36 | 348.52  | 602.333 | 760.222 | 0 | 760.222 |
| 21 | 1.53624 | 1379.45 | Structural<br>Fill | 50 | 36 | 211.707 | 365.884 | 434.776 | 0 | 434.776 |
| 22 | 1.53624 | 1644.98 | Structural<br>Fill | 50 | 36 | 307.545 | 531.517 | 662.752 | 0 | 662.752 |
| 23 | 1.53624 | 1859.2  | Structural<br>Fill | 50 | 36 | 225.394 | 389.539 | 467.334 | 0 | 467.334 |
| 24 | 1.53624 | 1472.93 | Structural<br>Fill | 50 | 36 | 176.045 | 304.252 | 349.949 | 0 | 349.949 |
| 25 | 1.53624 | 525.724 | Structural<br>Fill | 50 | 36 | 68.683  | 118.702 | 94.5603 | 0 | 94.5603 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.72826

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 465.128           | 8657.97                    | 0                             | 0                            | 0                                |
| 2            | 466.664           | 8657.84                    | 138.575                       | 83.7852                      | 31.158                           |
| 3            | 468.2             | 8657.77                    | 378.393                       | 228.783                      | 31.1579                          |
| 4            | 469.737           | 8657.77                    | 646.189                       | 390.698                      | 31.1579                          |
| 5            | 471.273           | 8657.84                    | 895.695                       | 541.554                      | 31.1579                          |
| 6            | 472.809           | 8657.97                    | 1121.23                       | 677.913                      | 31.1578                          |
| 7            | 474.345           | 8658.17                    | 1427.9                        | 863.335                      | 31.1579                          |
| 8            | 475.881           | 8658.44                    | 1852.79                       | 1120.23                      | 31.1579                          |
| 9            | 477.418           | 8658.78                    | 2283.71                       | 1380.77                      | 31.1579                          |
| 10           | 478.954           | 8659.19                    | 2591.87                       | 1567.1                       | 31.1581                          |
| 11           | 480.49            | 8659.68                    | 2792.38                       | 1688.33                      | 31.158                           |
| 12           | 482.026           | 8660.24                    | 2908.22                       | 1758.36                      | 31.1579                          |
| 13           | 483.563           | 8660.89                    | 2950.44                       | 1783.89                      | 31.1579                          |
| 14           | 485.099           | 8661.63                    | 4003.85                       | 2420.8                       | 31.1579                          |
| 15           | 486.635           | 8662.46                    | 3871.1                        | 2340.54                      | 31.1579                          |
| 16           | 488.171           | 8663.39                    | 3581.75                       | 2165.59                      | 31.1579                          |
| 17           | 489.708           | 8664.44                    | 3142.81                       | 1900.2                       | 31.1579                          |
| 18           | 491.244           | 8665.61                    | 2652.25                       | 1603.6                       | 31.1579                          |
| 19           | 492.78            | 8666.92                    | 2146.15                       | 1297.6                       | 31.1579                          |
| 20           | 494.316           | 8668.39                    | 1634.39                       | 988.184                      | 31.158                           |
| 21           | 495.853           | 8670.06                    | 2011.42                       | 1216.14                      | 31.1579                          |
| 22           | 497.389           | 8671.97                    | 1506.9                        | 911.098                      | 31.1579                          |
| 23           | 498.925           | 8674.19                    | 1617.28                       | 977.838                      | 31.1579                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 24 | 500.461 | 8676.85 | 720.617 | 435.698 | 31.1579 |
| 25 | 501.998 | 8680.22 | 150.992 | 91.2925 | 31.1579 |
| 26 | 503.534 | 8685.12 | 0       | 0       | 0       |

## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 526.379 | 8685.61 |
| 510.378 | 8685.26 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 421.181 | 8639.59 |
| 393.295 | 8638    |

### External Boundary

| X       | Y       |
|---------|---------|
| 440.831 | 8645.59 |
| 421.181 | 8639.59 |
| 393.295 | 8638    |
| 380.649 | 8637.31 |
| 378.561 | 8637.19 |
| 374.318 | 8631.91 |
| 373.988 | 8631.83 |
| 373.068 | 8631.67 |
| 361.645 | 8630.22 |
| 359.063 | 8629.4  |
| 355.702 | 8629.09 |
| 346.687 | 8627.67 |
| 336.161 | 8625    |
| 332.942 | 8624.55 |
| 328.731 | 8623.66 |
| 320.329 | 8621.56 |
| 313.544 | 8619.77 |
| 308.424 | 8619    |
| 301.704 | 8618.47 |
| 293.567 | 8617.14 |
| 284.996 | 8615.9  |
| 275.351 | 8614.1  |
| 267.191 | 8613.02 |
| 267.191 | 8509.63 |
| 734.667 | 8509.63 |

|         |         |
|---------|---------|
| 734.667 | 8722.08 |
| 709.533 | 8718.07 |
| 655.938 | 8707.4  |
| 624.624 | 8700.84 |
| 598.226 | 8695.91 |
| 587.034 | 8693.6  |
| 557.261 | 8688.49 |
| 549.449 | 8686.73 |
| 541.984 | 8684.7  |
| 533.081 | 8682.27 |
| 526.379 | 8685.61 |
| 510.378 | 8685.26 |
| 503.19  | 8685.11 |
| 500.375 | 8685.05 |
| 496.374 | 8677.04 |
| 492.368 | 8676.54 |
| 488.372 | 8676.03 |
| 484.371 | 8668.03 |
| 479.585 | 8667.42 |
| 476.368 | 8667.02 |
| 472.836 | 8660.14 |
| 468.161 | 8659.51 |
| 458.639 | 8654.69 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 458.639 | 8654.69 |
| 471.723 | 8653.68 |
| 504.285 | 8667.49 |
| 535.195 | 8680.55 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 535.195 | 8680.55 |
| 541.984 | 8684.7  |

### Material Boundary

| X       | Y       |
|---------|---------|
| 472.836 | 8660.14 |
| 472.4   | 8659.27 |
| 476.399 | 8659.17 |
| 479.585 | 8667.42 |

**Material Boundary**

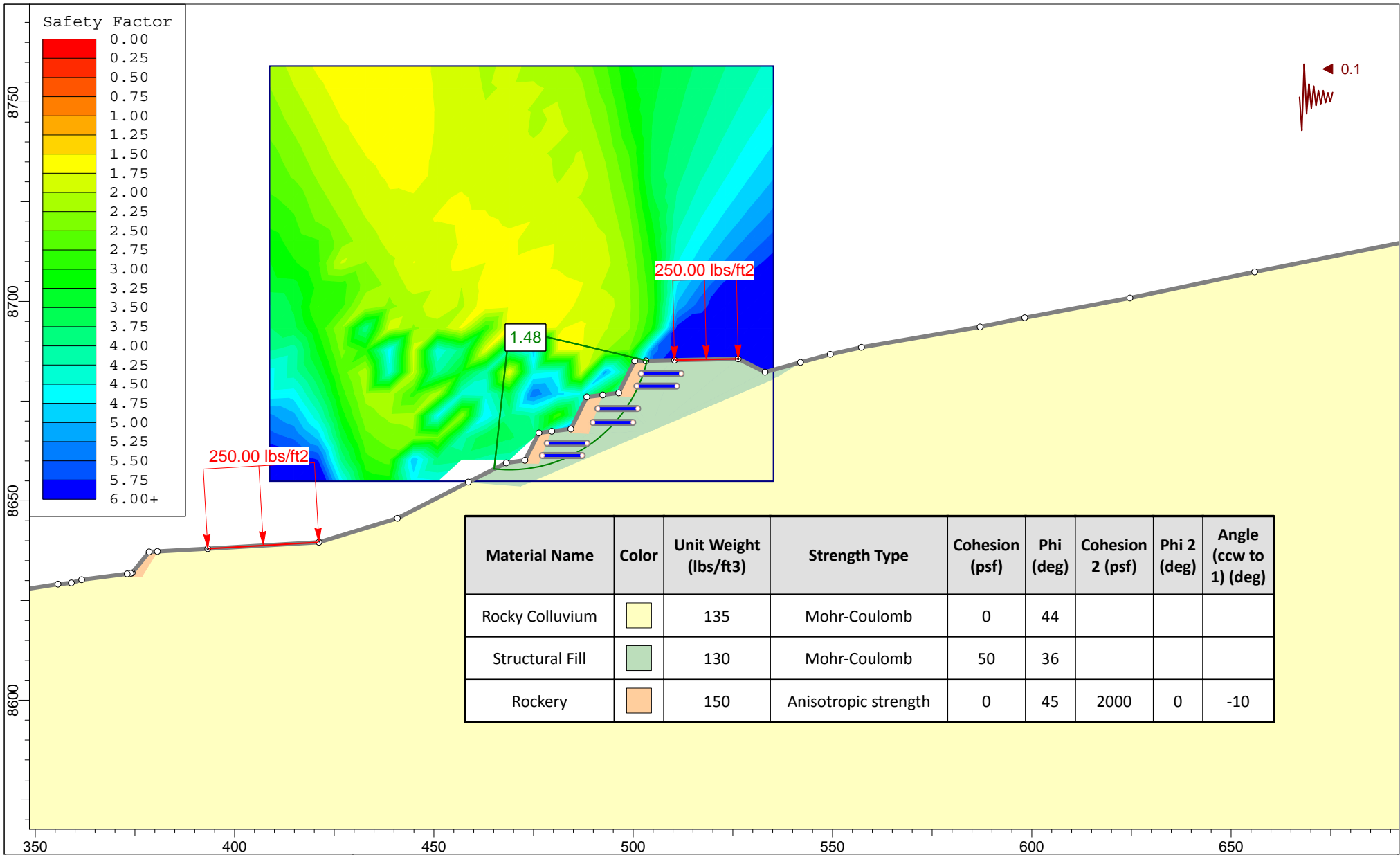
| X       | Y       |
|---------|---------|
| 484.371 | 8668.03 |
| 483.923 | 8667.13 |
| 488.916 | 8666.85 |
| 492.368 | 8676.54 |


**Material Boundary**

| X       | Y       |
|---------|---------|
| 496.374 | 8677.04 |
| 495.927 | 8676.15 |
| 499.919 | 8675.91 |
| 503.19  | 8685.11 |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 374.318 | 8631.91 |
| 373.743 | 8631.17 |
| 376.736 | 8630.96 |
| 380.649 | 8637.31 |



|  |                      |           |       |  |               |            |
|--|----------------------|-----------|-------|--|---------------|------------|
|  | Project              |           |       | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G       |               |            |
|  | Analysis Description |           |       | GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 3-3' |               |            |
|  | Drawn By             | SL        | Scale | 1:400  | Company       | IGES, INC. |
|  | Date                 | 9-25-2015 |       | File Name  | P-Static.slim |            |

## *Slide Analysis Information*

# *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

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File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

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Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

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Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present




### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties


| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |

## Support Properties

## Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

### Pullout Strength Dependency:

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

## Global Minimums

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### Method: spencer

FS: 1.483730  
 Center: 468.985, 8693.256  
 Radius: 35.494  
 Left Slip Surface Endpoint: 465.128, 8657.972  
 Right Slip Surface Endpoint: 503.534, 8685.117  
 Resisting Moment=1.08422e+006 lb-ft  
 Driving Moment=730739 lb-ft  
 Resisting Horizontal Force=28057.1 lb  
 Driving Horizontal Force=18909.9 lb  
 Total Slice Area=255.003 ft<sup>2</sup>

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 3445  
 Number of Invalid Surfaces: 1395

#### Error Codes:

Error Code -103 reported for 496 surfaces  
 Error Code -107 reported for 9 surfaces  
 Error Code -108 reported for 107 surfaces  
 Error Code -111 reported for 358 surfaces  
 Error Code -112 reported for 425 surfaces

#### Error Codes

The following errors were encountered during the computation:



- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.48373

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 1.53624    | 91.0256      | Structural Fill | 50                  | 36                            | 113.26             | 168.048              | 162.48                   | 0                   | 162.48                        |
| 2            | 1.53624    | 266.354      | Structural Fill | 50                  | 36                            | 195.964            | 290.758              | 331.376                  | 0                   | 331.376                       |
| 3            | 1.53624    | 368.8        | Structural Fill | 50                  | 36                            | 229.734            | 340.863              | 400.339                  | 0                   | 400.339                       |
| 4            | 1.53624    | 404.091      | Structural Fill | 50                  | 36                            | 228.499            | 339.031              | 397.817                  | 0                   | 397.817                       |
| 5            | 1.53624    | 429.457      | Structural Fill | 50                  | 36                            | 223.158            | 331.106              | 386.909                  | 0                   | 386.909                       |
| 6            | 1.53624    | 774.534      | Structural Fill | 50                  | 36                            | 338.339            | 502.003              | 622.13                   | 0                   | 622.13                        |
| 7            | 1.53624    | 1417.42      | Structural Fill | 50                  | 36                            | 541.789            | 803.869              | 1037.61                  | 0                   | 1037.61                       |
| 8            | 1.53624    | 1869.07      | Structural Fill | 50                  | 36                            | 655.595            | 972.726              | 1270.02                  | 0                   | 1270.02                       |
| 9            | 1.53624    | 1755.73      | Structural Fill | 50                  | 36                            | 580.837            | 861.806              | 1117.36                  | 0                   | 1117.36                       |
| 10           | 1.53624    | 1608.49      | Structural Fill | 50                  | 36                            | 504.092            | 747.936              | 960.628                  | 0                   | 960.628                       |
| 11           | 1.53624    | 1532.18      | Structural Fill | 50                  | 36                            | 454.336            | 674.112              | 859.019                  | 0                   | 859.019                       |
| 12           | 1.53624    | 1449.56      | Structural Fill | 50                  | 36                            | 407.474            | 604.581              | 763.318                  | 0                   | 763.318                       |
| 13           | 1.53624    | 1442.97      | Structural Fill | 50                  | 36                            | 646.433            | 959.132              | 1251.31                  | 0                   | 1251.31                       |
| 14           | 1.53624    | 1915.15      | Structural Fill | 50                  | 36                            | 467.296            | 693.341              | 885.483                  | 0                   | 885.483                       |
| 15           | 1.53624    | 2449.95      | Structural Fill | 50                  | 36                            | 552.921            | 820.385              | 1060.35                  | 0                   | 1060.35                       |
|              |            |              | Structural      |                     |                               |                    |                      |                          |                     |                               |

|    |         |         | Fill               |    |    |         |         |         |   |         |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|
| 17 | 1.53624 | 2407.26 | Structural<br>Fill | 50 | 36 | 479.046 | 710.775 | 909.478 | 0 | 909.478 |
| 18 | 1.53624 | 2076.52 | Structural<br>Fill | 50 | 36 | 390.56  | 579.486 | 728.778 | 0 | 728.778 |
| 19 | 1.53624 | 1803.38 | Structural<br>Fill | 50 | 36 | 319.799 | 474.495 | 584.268 | 0 | 584.268 |
| 20 | 1.53624 | 1528.34 | Structural<br>Fill | 50 | 36 | 414.538 | 615.063 | 777.744 | 0 | 777.744 |
| 21 | 1.53624 | 1379.45 | Structural<br>Fill | 50 | 36 | 214.965 | 318.95  | 370.178 | 0 | 370.178 |
| 22 | 1.53624 | 1644.98 | Structural<br>Fill | 50 | 36 | 352.102 | 522.425 | 650.237 | 0 | 650.237 |
| 23 | 1.53624 | 1859.2  | Structural<br>Fill | 50 | 36 | 228.132 | 338.486 | 397.066 | 0 | 397.066 |
| 24 | 1.53624 | 1472.93 | Structural<br>Fill | 50 | 36 | 188.058 | 279.028 | 315.232 | 0 | 315.232 |
| 25 | 1.53624 | 525.724 | Structural<br>Fill | 50 | 36 | 71.7641 | 106.479 | 77.736  | 0 | 77.736  |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.48373

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 465.128           | 8657.97                    | 0                             | 0                            | 0                                |
| 2            | 466.664           | 8657.84                    | 186.134                       | 146.669                      | 38.2372                          |
| 3            | 468.2             | 8657.77                    | 481.858                       | 379.693                      | 38.2373                          |
| 4            | 469.737           | 8657.77                    | 797.037                       | 628.045                      | 38.2372                          |
| 5            | 471.273           | 8657.84                    | 1080.31                       | 851.259                      | 38.2373                          |
| 6            | 472.809           | 8657.97                    | 1327.69                       | 1046.19                      | 38.2373                          |
| 7            | 474.345           | 8658.17                    | 1643.58                       | 1295.1                       | 38.2372                          |
| 8            | 475.881           | 8658.44                    | 2051.94                       | 1616.88                      | 38.2373                          |
| 9            | 477.418           | 8658.78                    | 2437.29                       | 1920.52                      | 38.2372                          |
| 10           | 478.954           | 8659.19                    | 2690.27                       | 2119.87                      | 38.2373                          |
| 11           | 480.49            | 8659.68                    | 2832.8                        | 2232.18                      | 38.2373                          |
| 12           | 482.026           | 8660.24                    | 2888.81                       | 2276.31                      | 38.2372                          |
| 13           | 483.563           | 8660.89                    | 2872.37                       | 2263.36                      | 38.2373                          |
| 14           | 485.099           | 8661.63                    | 4088.57                       | 3221.69                      | 38.2372                          |
| 15           | 486.635           | 8662.46                    | 3876.78                       | 3054.81                      | 38.2373                          |
| 16           | 488.171           | 8663.39                    | 3489.18                       | 2749.39                      | 38.2373                          |
| 17           | 489.708           | 8664.44                    | 2949.46                       | 2324.1                       | 38.2372                          |
| 18           | 491.244           | 8665.61                    | 2378.72                       | 1874.37                      | 38.2372                          |
| 19           | 492.78            | 8666.92                    | 1814.01                       | 1429.39                      | 38.2371                          |
| 20           | 494.316           | 8668.39                    | 1262.14                       | 994.535                      | 38.2372                          |
| 21           | 495.853           | 8670.06                    | 1739                          | 1370.29                      | 38.2373                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 22 | 497.389 | 8671.97 | 1223.57 | 964.145 | 38.2373 |
| 23 | 498.925 | 8674.19 | 1446.55 | 1139.84 | 38.2371 |
| 24 | 500.461 | 8676.85 | 553.723 | 436.32  | 38.2372 |
| 25 | 501.998 | 8680.22 | 26.5325 | 20.907  | 38.2373 |
| 26 | 503.534 | 8685.12 | 0       | 0       | 0       |

## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 526.379 | 8685.61 |
| 510.378 | 8685.26 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 421.181 | 8639.59 |
| 393.295 | 8638    |

### External Boundary

| X       | Y       |
|---------|---------|
| 440.831 | 8645.59 |
| 421.181 | 8639.59 |
| 393.295 | 8638    |
| 380.649 | 8637.31 |
| 378.561 | 8637.19 |
| 374.318 | 8631.91 |
| 373.988 | 8631.83 |
| 373.068 | 8631.67 |
| 361.645 | 8630.22 |
| 359.063 | 8629.4  |
| 355.702 | 8629.09 |
| 346.687 | 8627.67 |
| 336.161 | 8625    |
| 332.942 | 8624.55 |
| 328.731 | 8623.66 |
| 320.329 | 8621.56 |
| 313.544 | 8619.77 |
| 308.424 | 8619    |
| 301.704 | 8618.47 |
| 293.567 | 8617.14 |
| 284.996 | 8615.9  |
| 275.351 | 8614.1  |
| 267.191 | 8613.02 |

|         |         |
|---------|---------|
| 267.191 | 8509.63 |
| 734.667 | 8509.63 |
| 734.667 | 8722.08 |
| 709.533 | 8718.07 |
| 655.938 | 8707.4  |
| 624.624 | 8700.84 |
| 598.226 | 8695.91 |
| 587.034 | 8693.6  |
| 557.261 | 8688.49 |
| 549.449 | 8686.73 |
| 541.984 | 8684.7  |
| 533.081 | 8682.27 |
| 526.379 | 8685.61 |
| 510.378 | 8685.26 |
| 503.19  | 8685.11 |
| 500.375 | 8685.05 |
| 496.374 | 8677.04 |
| 492.368 | 8676.54 |
| 488.372 | 8676.03 |
| 484.371 | 8668.03 |
| 479.585 | 8667.42 |
| 476.368 | 8667.02 |
| 472.836 | 8660.14 |
| 468.161 | 8659.51 |
| 458.639 | 8654.69 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 458.639 | 8654.69 |
| 471.723 | 8653.68 |
| 504.285 | 8667.49 |
| 535.195 | 8680.55 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 535.195 | 8680.55 |
| 541.984 | 8684.7  |

### Material Boundary

| X       | Y       |
|---------|---------|
| 472.836 | 8660.14 |
| 472.4   | 8659.27 |
| 476.399 | 8659.17 |

|         |         |
|---------|---------|
| 479.585 | 8667.42 |
|---------|---------|

### Material Boundary

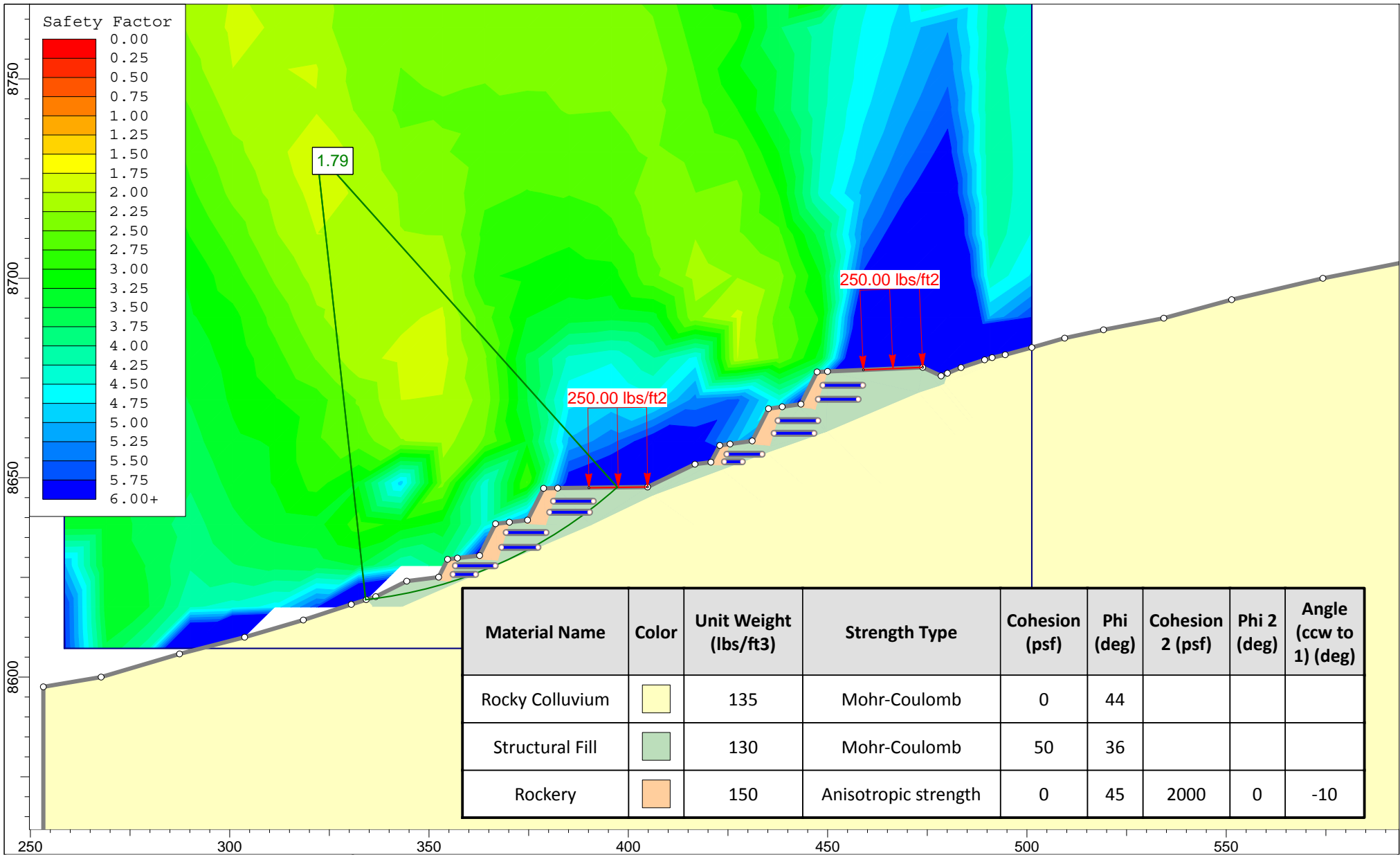
| X       | Y       |
|---------|---------|
| 484.371 | 8668.03 |
| 483.923 | 8667.13 |
| 488.916 | 8666.85 |
| 492.368 | 8676.54 |




### Material Boundary


| X       | Y       |
|---------|---------|
| 496.374 | 8677.04 |
| 495.927 | 8676.15 |
| 499.919 | 8675.91 |
| 503.19  | 8685.11 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.318 | 8631.91 |
| 373.743 | 8631.17 |
| 376.736 | 8630.96 |
| 380.649 | 8637.31 |



| Material Name   | Color  | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|--|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |  | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |  | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |  | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |

|  |  |                                 |                              |
|--|--|---------------------------------|------------------------------|
|  | <i>Project</i><br>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G                   |                                 |                              |
|  | <i>Analysis Description</i><br>GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 4-4' |                                 |                              |
|  | <i>Drawn By</i><br>SL  | <i>Scale</i><br>1:400           | <i>Company</i><br>IGES, INC. |
|  | <i>Date</i><br>9-25-2015   | <i>File Name</i><br>Static.slim |                              |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

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File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

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Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

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Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

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Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Support Properties


---

### Mirafi 3XT



Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

**Global Minimums**

---

**Method: spencer**

FS: 1.788680  
 Center: 321.818, 8731.753  
 Radius: 113.059  
 Left Slip Surface Endpoint: 334.104, 8619.364  
 Right Slip Surface Endpoint: 397.280, 8647.564  
 Resisting Moment=4.58962e+006 lb-ft  
 Driving Moment=2.56593e+006 lb-ft  
 Resisting Horizontal Force=36906.9 lb  
 Driving Horizontal Force=20633.6 lb  
 Total Slice Area=361.439 ft<sup>2</sup>

**Valid / Invalid Surfaces**

---

**Method: spencer**

Number of Valid Surfaces: 3922  
 Number of Invalid Surfaces: 1094

**Error Codes:**

Error Code -103 reported for 121 surfaces  
 Error Code -106 reported for 32 surfaces  
 Error Code -107 reported for 3 surfaces  
 Error Code -108 reported for 79 surfaces  
 Error Code -111 reported for 112 surfaces  
 Error Code -112 reported for 747 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.78868

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 0.169004   | 0.401064     | Rocky Colluvium | 0                   | 44                            | 1.4585             | 2.60879              | 2.70148                  | 0                   | 2.70148                       |
| 2            | 2.62528    | 100.856      | Structural Fill | 50                  | 36                            | 48.4655            | 86.6893              | 50.4985                  | 0                   | 50.4985                       |
| 3            | 2.62528    | 361.953      | Structural Fill | 50                  | 36                            | 90.3532            | 161.613              | 153.622                  | 0                   | 153.622                       |
| 4            | 2.62528    | 667.833      | Structural Fill | 50                  | 36                            | 137.662            | 246.234              | 270.092                  | 0                   | 270.092                       |
| 5            | 2.62528    | 948.968      | Structural Fill | 50                  | 36                            | 179.14             | 320.425              | 372.208                  | 0                   | 372.208                       |
| 6            | 2.62528    | 1001.1       | Structural Fill | 50                  | 36                            | 183.781            | 328.726              | 383.635                  | 0                   | 383.635                       |
| 7            | 2.62528    | 904.907      | Structural Fill | 50                  | 36                            | 165.897            | 296.737              | 339.605                  | 0                   | 339.605                       |
| 8            | 2.62528    | 799.27       | Structural Fill | 50                  | 36                            | 147.283            | 263.442              | 293.777                  | 0                   | 293.777                       |
| 9            | 2.62528    | 1779.35      | Structural Fill | 50                  | 36                            | 285.868            | 511.327              | 634.962                  | 0                   | 634.962                       |
| 10           | 2.62528    | 2022.2       | Structural Fill | 50                  | 36                            | 314.64             | 562.79               | 705.796                  | 0                   | 705.796                       |
| 11           | 2.62528    | 1703.45      | Structural Fill | 50                  | 36                            | 264.411            | 472.947              | 582.138                  | 0                   | 582.138                       |
| 12           | 2.62528    | 1523.4       | Structural Fill | 50                  | 36                            | 253.83             | 454.02               | 556.084                  | 0                   | 556.084                       |
| 13           | 2.62528    | 2599.52      | Structural Fill | 50                  | 36                            | 373.089            | 667.337              | 849.692                  | 0                   | 849.692                       |
| 14           | 2.62528    | 3835.31      | Structural Fill | 50                  | 36                            | 534.014            | 955.181              | 1245.87                  | 0                   | 1245.87                       |
| 15           | 2.62528    | 3317.79      | Structural Fill | 50                  | 36                            | 449.485            | 803.985              | 1037.77                  | 0                   | 1037.77                       |
| 16           | 2.62528    | 2890.74      | Structural Fill | 50                  | 36                            | 387.011            | 692.239              | 883.967                  | 0                   | 883.967                       |
| 17           | 2.62528    | 2903.35      | Structural Fill | 50                  | 36                            | 436.557            | 780.86               | 1005.94                  | 0                   | 1005.94                       |
| 18           | 2.62528    | 4316.83      | Structural Fill | 50                  | 36                            | 540.52             | 966.818              | 1261.89                  | 0                   | 1261.89                       |
| 19           | 2.62528    | 4557.98      | Structural Fill | 50                  | 36                            | 556.647            | 995.663              | 1301.59                  | 0                   | 1301.59                       |
| 20           | 2.62528    | 3703.26      | Structural Fill | 50                  | 36                            | 446.951            | 799.452              | 1031.53                  | 0                   | 1031.53                       |
| 21           | 2.62528    | 3104.07      | Structural Fill | 50                  | 36                            | 370.185            | 662.142              | 842.54                   | 0                   | 842.54                        |
| 22           | 2.62528    | 2485.55      | Structural Fill | 50                  | 36                            | 294.531            | 526.821              | 656.287                  | 0                   | 656.287                       |
| 23           | 2.62528    | 1827.84      | Structural Fill | 50                  | 36                            | 290.453            | 519.527              | 646.248                  | 0                   | 646.248                       |
| 24           | 2.62528    | 1128.3       | Structural Fill | 50                  | 36                            | 208.605            | 373.128              | 444.748                  | 0                   | 444.748                       |
| 25           | 2.62528    | 383.858      | Structural Fill | 50                  | 36                            | 129.686            | 231.967              | 250.456                  | 0                   | 250.456                       |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.78868

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 334.104           | 8619.36                    | 0                             | 0                            | 0                                |
| 2            | 334.273           | 8619.38                    | 0.196209                      | 0.084643                     | 23.335                           |
| 3            | 336.898           | 8619.7                     | 111.153                       | 47.9502                      | 23.3348                          |
| 4            | 339.524           | 8620.09                    | 289.225                       | 124.769                      | 23.3349                          |
| 5            | 342.149           | 8620.54                    | 529.581                       | 228.457                      | 23.335                           |
| 6            | 344.774           | 8621.05                    | 809.227                       | 349.093                      | 23.3349                          |
| 7            | 347.4             | 8621.63                    | 1070.29                       | 461.713                      | 23.3349                          |
| 8            | 350.025           | 8622.27                    | 1287.41                       | 555.376                      | 23.3349                          |
| 9            | 352.65            | 8622.98                    | 1465.4                        | 632.162                      | 23.335                           |
| 10           | 355.275           | 8623.76                    | 1721.43                       | 742.608                      | 23.3349                          |
| 11           | 357.901           | 8624.61                    | 1948.45                       | 840.542                      | 23.3349                          |
| 12           | 360.526           | 8625.53                    | 2106.85                       | 908.875                      | 23.3349                          |
| 13           | 363.151           | 8626.52                    | 2544.85                       | 1097.82                      | 23.3348                          |
| 14           | 365.777           | 8627.59                    | 2615.61                       | 1128.35                      | 23.3349                          |
| 15           | 368.402           | 8628.74                    | 2728.92                       | 1177.23                      | 23.3349                          |
| 16           | 371.027           | 8629.97                    | 2634.53                       | 1136.51                      | 23.3349                          |
| 17           | 373.652           | 8631.28                    | 2491.13                       | 1074.65                      | 23.3349                          |
| 18           | 376.278           | 8632.68                    | 3302.72                       | 1424.76                      | 23.3349                          |
| 19           | 378.903           | 8634.16                    | 2842.65                       | 1226.29                      | 23.3349                          |
| 20           | 381.528           | 8635.75                    | 2242.36                       | 967.336                      | 23.335                           |
| 21           | 384.153           | 8637.43                    | 1679.1                        | 724.349                      | 23.3349                          |
| 22           | 386.779           | 8639.22                    | 1143.97                       | 493.498                      | 23.3349                          |
| 23           | 389.404           | 8641.12                    | 670.333                       | 289.176                      | 23.335                           |
| 24           | 392.029           | 8643.14                    | 619.372                       | 267.192                      | 23.335                           |
| 25           | 394.655           | 8645.28                    | 220.981                       | 95.3293                      | 23.335                           |
| 26           | 397.28            | 8647.56                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 473.862 | 8677.66 |

|         |         |
|---------|---------|
| 458.966 | 8677.03 |
|---------|---------|

### External Boundary

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |
| 370.173 | 8638.84 |

|         |         |
|---------|---------|
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |
| 354.671 | 8629.53 |
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |
| 382.29  | 8647.38 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

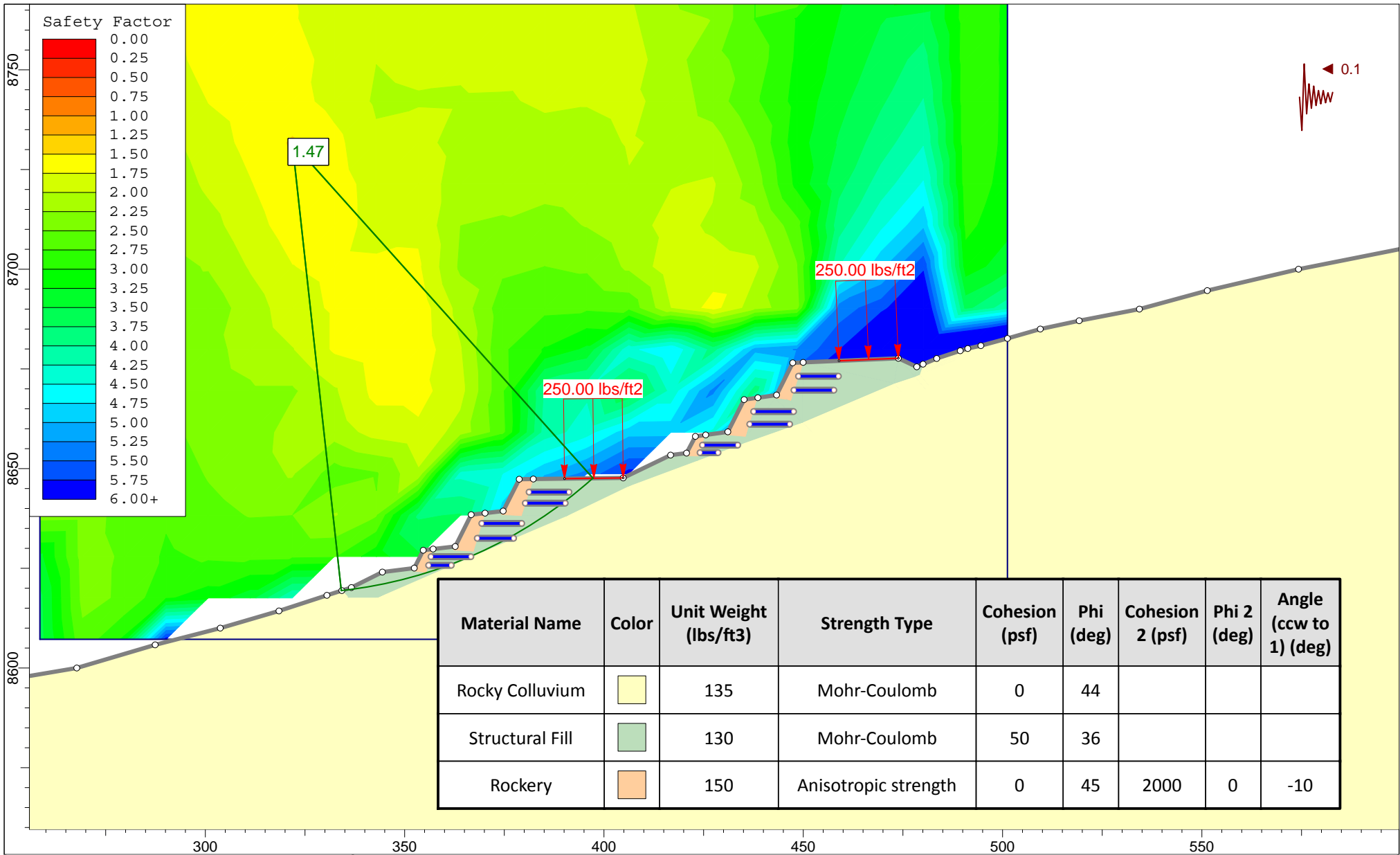
| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



|  |   |                                   |                              |
|--|---|-----------------------------------|------------------------------|
|  | <b>Project</b><br>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G                    |                                   |                              |
|  | <b>Analysis Description</b><br>GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 4-4' |                                   |                              |
|  | <b>Drawn By</b><br>SL   | <b>Scale</b><br>1:400             | <b>Company</b><br>IGES, INC. |
|  | <b>Date</b><br>9-25-2015  | <b>File Name</b><br>P-Static.slim |                              |

## ***Slide Analysis Information***

### ***SLIDE - An Interactive Slope Stability Program***

#### ***Project Summary***

---

File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

#### ***General Settings***

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

#### ***Analysis Options***

---

##### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

#### ***Groundwater Analysis***

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

#### ***Random Numbers***

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3



## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |


## Support Properties

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### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

### Global Minimums

---

**Method: spencer**

FS: 1.466280  
 Center: 321.818, 8731.753  
 Radius: 113.059  
 Left Slip Surface Endpoint: 334.104, 8619.364  
 Right Slip Surface Endpoint: 397.280, 8647.564  
 Resisting Moment=4.4523e+006 lb-ft  
 Driving Moment=3.03646e+006 lb-ft  
 Resisting Horizontal Force=35822.9 lb  
 Driving Horizontal Force=24431.1 lb  
 Total Slice Area=361.439 ft<sup>2</sup>

### Valid / Invalid Surfaces

---

**Method: spencer**

Number of Valid Surfaces: 3579  
 Number of Invalid Surfaces: 1437

**Error Codes:**

Error Code -103 reported for 121 surfaces  
 Error Code -106 reported for 32 surfaces  
 Error Code -107 reported for 1 surface  
 Error Code -108 reported for 162 surfaces  
 Error Code -111 reported for 279 surfaces  
 Error Code -112 reported for 842 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.46628

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 0.169004   | 0.401064     | Rocky Colluvium | 0                   | 44                            | 2.02971            | 2.97613              | 3.08187                  | 0                   | 3.08187                       |
| 2            | 2.62528    | 100.856      | Structural Fill | 50                  | 36                            | 67.3283            | 98.7222              | 67.0602                  | 0                   | 67.0602                       |
| 3            | 2.62528    | 361.953      | Structural Fill | 50                  | 36                            | 120.753            | 177.058              | 174.881                  | 0                   | 174.881                       |
| 4            | 2.62528    | 667.833      | Structural Fill | 50                  | 36                            | 179.899            | 263.782              | 294.246                  | 0                   | 294.246                       |
| 5            | 2.62528    | 948.968      | Structural Fill | 50                  | 36                            | 230.406            | 337.839              | 396.178                  | 0                   | 396.178                       |
| 6            | 2.62528    | 1001.1       | Structural Fill | 50                  | 36                            | 233.907            | 342.973              | 403.245                  | 0                   | 403.245                       |
| 7            | 2.62528    | 904.907      | Structural Fill | 50                  | 36                            | 209.561            | 307.275              | 354.108                  | 0                   | 354.108                       |
| 8            | 2.62528    | 799.27       | Structural Fill | 50                  | 36                            | 184.841            | 271.028              | 304.218                  | 0                   | 304.218                       |
| 9            | 2.62528    | 1779.35      | Structural Fill | 50                  | 36                            | 350.559            | 514.017              | 638.665                  | 0                   | 638.665                       |
| 10           | 2.62528    | 2022.2       | Structural Fill | 50                  | 36                            | 381.6              | 559.532              | 701.312                  | 0                   | 701.312                       |
| 11           | 2.62528    | 1703.45      | Structural Fill | 50                  | 36                            | 318.497            | 467.006              | 573.96                   | 0                   | 573.96                        |
| 12           | 2.62528    | 1523.4       | Structural Fill | 50                  | 36                            | 327.83             | 480.69               | 592.792                  | 0                   | 592.792                       |
| 13           | 2.62528    | 2599.52      | Structural Fill | 50                  | 36                            | 438.823            | 643.438              | 816.796                  | 0                   | 816.796                       |
| 14           | 2.62528    | 3835.31      | Structural Fill | 50                  | 36                            | 630.009            | 923.769              | 1202.64                  | 0                   | 1202.64                       |
| 15           | 2.62528    | 3317.79      | Structural Fill | 50                  | 36                            | 517.881            | 759.359              | 976.35                   | 0                   | 976.35                        |
| 16           | 2.62528    | 2890.74      | Structural Fill | 50                  | 36                            | 442.717            | 649.147              | 824.654                  | 0                   | 824.654                       |
| 17           | 2.62528    | 2903.35      | Structural Fill | 50                  | 36                            | 564.765            | 828.103              | 1070.97                  | 0                   | 1070.97                       |
| 18           | 2.62528    | 4316.83      | Structural Fill | 50                  | 36                            | 605.15             | 887.319              | 1152.47                  | 0                   | 1152.47                       |
| 19           | 2.62528    | 4557.98      | Structural Fill | 50                  | 36                            | 617.661            | 905.664              | 1177.72                  | 0                   | 1177.72                       |
| 20           | 2.62528    | 3703.26      | Structural Fill | 50                  | 36                            | 492.972            | 722.835              | 926.077                  | 0                   | 926.077                       |
| 21           | 2.62528    | 3104.07      | Structural Fill | 50                  | 36                            | 406.011            | 595.326              | 750.577                  | 0                   | 750.577                       |
| 22           | 2.62528    | 2485.55      | Structural Fill | 50                  | 36                            | 321.73             | 471.746              | 580.482                  | 0                   | 580.482                       |
| 23           | 2.62528    | 1827.84      | Structural Fill | 50                  | 36                            | 344.414            | 505.008              | 626.265                  | 0                   | 626.265                       |
| 24           | 2.62528    | 1128.3       | Structural Fill | 50                  | 36                            | 231.664            | 339.684              | 398.716                  | 0                   | 398.716                       |
| 25           | 2.62528    | 383.858      | Structural Fill | 50                  | 36                            | 147.179            | 215.806              | 228.212                  | 0                   | 228.212                       |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.46628

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 334.104           | 8619.36                    | 0                             | 0                            | 0                                |
| 2            | 334.273           | 8619.38                    | 0.246005                      | 0.171301                     | 34.8507                          |
| 3            | 336.898           | 8619.7                     | 145.529                       | 101.336                      | 34.8506                          |
| 4            | 339.524           | 8620.09                    | 359.444                       | 250.293                      | 34.8508                          |
| 5            | 342.149           | 8620.54                    | 633.687                       | 441.256                      | 34.8507                          |
| 6            | 344.774           | 8621.05                    | 941.528                       | 655.616                      | 34.8507                          |
| 7            | 347.4             | 8621.63                    | 1223.55                       | 851.998                      | 34.8508                          |
| 8            | 350.025           | 8622.27                    | 1456.19                       | 1013.99                      | 34.8507                          |
| 9            | 352.65            | 8622.98                    | 1646.07                       | 1146.21                      | 34.8507                          |
| 10           | 355.275           | 8623.76                    | 1892.3                        | 1317.67                      | 34.8507                          |
| 11           | 357.901           | 8624.61                    | 2097.99                       | 1460.9                       | 34.8508                          |
| 12           | 360.526           | 8625.53                    | 2236.64                       | 1557.45                      | 34.8508                          |
| 13           | 363.151           | 8626.52                    | 2752.51                       | 1916.66                      | 34.8507                          |
| 14           | 365.777           | 8627.59                    | 2772.56                       | 1930.62                      | 34.8507                          |
| 15           | 368.402           | 8628.74                    | 2837.09                       | 1975.55                      | 34.8506                          |
| 16           | 371.027           | 8629.97                    | 2667.66                       | 1857.58                      | 34.8508                          |
| 17           | 373.652           | 8631.28                    | 2460.73                       | 1713.48                      | 34.8507                          |
| 18           | 376.278           | 8632.68                    | 3465.32                       | 2413.01                      | 34.8507                          |
| 19           | 378.903           | 8634.16                    | 2908.24                       | 2025.1                       | 34.8507                          |
| 20           | 381.528           | 8635.75                    | 2210.63                       | 1539.34                      | 34.8509                          |
| 21           | 384.153           | 8637.43                    | 1577.07                       | 1098.17                      | 34.8509                          |
| 22           | 386.779           | 8639.22                    | 991.456                       | 690.383                      | 34.8507                          |
| 23           | 389.404           | 8641.12                    | 485.781                       | 338.265                      | 34.8507                          |
| 24           | 392.029           | 8643.14                    | 541.852                       | 377.309                      | 34.8507                          |
| 25           | 394.655           | 8645.28                    | 190.692                       | 132.785                      | 34.8507                          |
| 26           | 397.28            | 8647.56                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

### Distributed Load

| X | Y |
|---|---|
|---|---|

|         |         |
|---------|---------|
| 473.862 | 8677.66 |
| 458.966 | 8677.03 |

### External Boundary

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |

|         |         |
|---------|---------|
| 370.173 | 8638.84 |
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |
| 354.671 | 8629.53 |
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |

|        |         |
|--------|---------|
| 382.29 | 8647.38 |
|--------|---------|

### Material Boundary

| X       | Y       |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

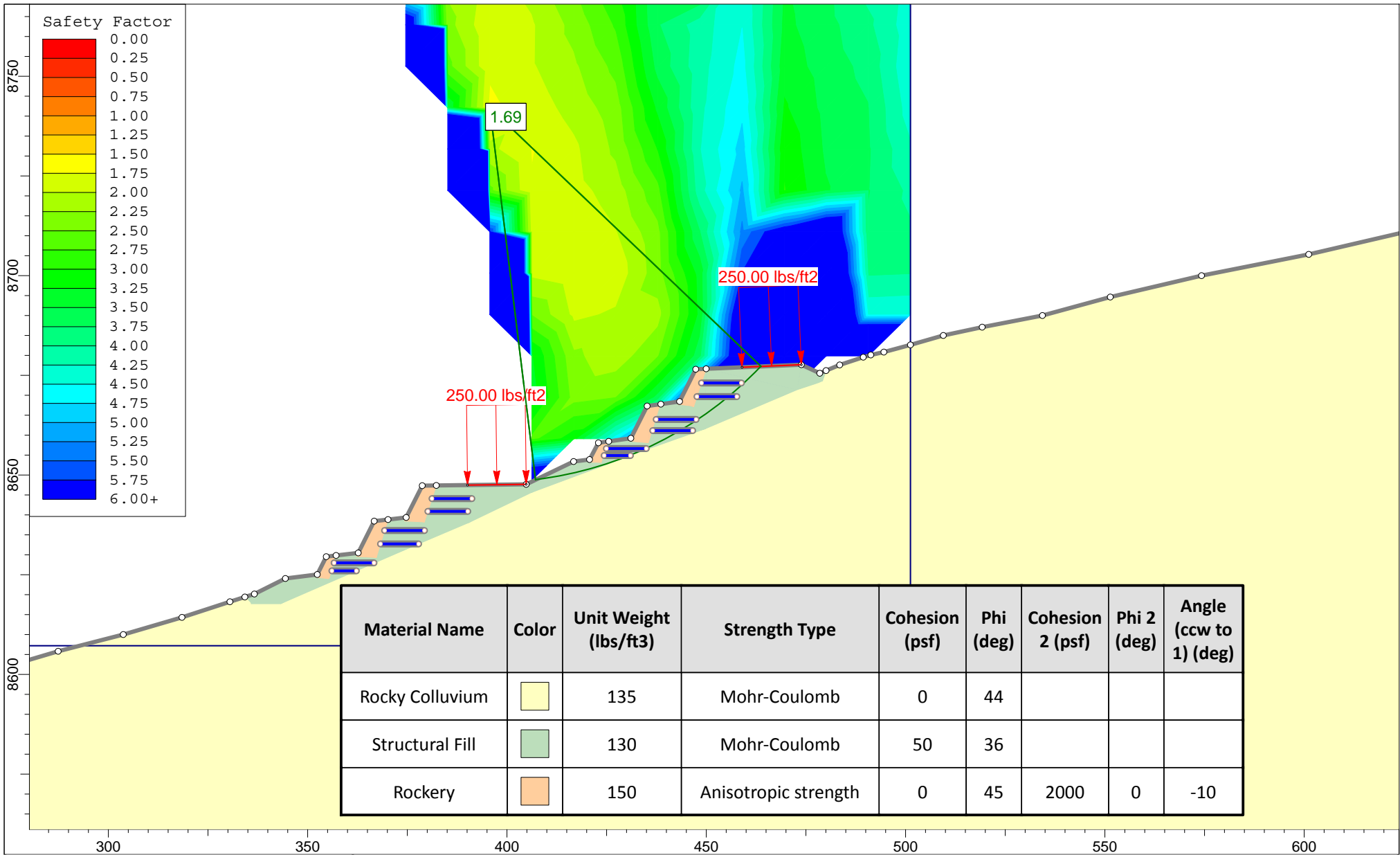
| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |




### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



| Material Name   | Color   | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|---|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |  | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |  | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |  | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |



SLIDEINTERPRET 6.029

|                             |           |              |       |   |                     |  |  |
|-----------------------------|-----------|--------------|-------|---|---------------------|--|--|
| <i>Project</i>              |           |              |       | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G      |                     |  |  |
| <i>Analysis Description</i> |           |              |       | GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 4-4' |                     |  |  |
| <i>Drawn By</i>             | SL        | <i>Scale</i> | 1:400 | <i>Company</i>  | IGES, INC.          |  |  |
| <i>Date</i>                 | 9-25-2015 |              |       | <i>File Name</i>  | Static - upper.slim |  |  |



# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

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File Name: Static - upper  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

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Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

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Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |


## Support Properties

---

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

**Global Minimums**

---

**Method: spencer**

FS: 1.691980  
 Center: 395.690, 8742.134  
 Radius: 94.059  
 Left Slip Surface Endpoint: 407.159, 8648.778  
 Right Slip Surface Endpoint: 463.767, 8677.231  
 Resisting Moment=3.56124e+006 lb-ft  
 Driving Moment=2.10477e+006 lb-ft  
 Resisting Horizontal Force=34081.4 lb  
 Driving Horizontal Force=20142.9 lb  
 Total Slice Area=337.324 ft<sup>2</sup>

**Valid / Invalid Surfaces**

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**Method: spencer**

Number of Valid Surfaces: 1570  
 Number of Invalid Surfaces: 3446

**Error Codes:**

- Error Code -103 reported for 11 surfaces
- Error Code -106 reported for 45 surfaces
- Error Code -107 reported for 6 surfaces
- Error Code -108 reported for 81 surfaces
- Error Code -111 reported for 38 surfaces
- Error Code -112 reported for 438 surfaces
- Error Code -113 reported for 275 surfaces
- Error Code -1000 reported for 2552 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 113 = Surface intersects outside slope limits.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.69198

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.26432    | 115.474      | Structural Fill | 50                  | 36                            | 59.5234            | 100.712              | 69.7997                  | 0                   | 69.7997                       |
| 2            | 2.26432    | 338.134      | Structural Fill | 50                  | 36                            | 104.146            | 176.213              | 173.717                  | 0                   | 173.717                       |
| 3            | 2.26432    | 544.122      | Structural Fill | 50                  | 36                            | 143.157            | 242.219              | 264.566                  | 0                   | 264.566                       |
| 4            | 2.26432    | 733.223      | Structural Fill | 50                  | 36                            | 176.873            | 299.266              | 343.085                  | 0                   | 343.085                       |
| 5            | 2.26432    | 834.07       | Structural Fill | 50                  | 36                            | 192.057            | 324.956              | 378.445                  | 0                   | 378.445                       |
| 6            | 2.26432    | 760.941      | Structural Fill | 50                  | 36                            | 174.135            | 294.633              | 336.709                  | 0                   | 336.709                       |
| 7            | 2.26432    | 1389.96      | Structural Fill | 50                  | 36                            | 283.978            | 480.485              | 592.513                  | 0                   | 592.513                       |
| 8            | 2.26432    | 1863.22      | Structural Fill | 50                  | 36                            | 360.797            | 610.462              | 771.411                  | 0                   | 771.411                       |
| 9            | 2.26432    | 1568.42      | Structural Fill | 50                  | 36                            | 301.547            | 510.212              | 633.426                  | 0                   | 633.426                       |
| 10           | 2.26432    | 1420.12      | Structural Fill | 50                  | 36                            | 269.576            | 456.118              | 558.975                  | 0                   | 558.975                       |
| 11           | 2.26432    | 1411.45      | Structural Fill | 50                  | 36                            | 268.209            | 453.805              | 555.789                  | 0                   | 555.789                       |
| 12           | 2.26432    | 2453.61      | Structural Fill | 50                  | 36                            | 421.684            | 713.481              | 913.202                  | 0                   | 913.202                       |
| 13           | 2.26432    | 3370.77      | Structural Fill | 50                  | 36                            | 564.573            | 955.247              | 1245.97                  | 0                   | 1245.97                       |
|              |            |              | Structural      |                     |                               |                    |                      |                          |                     |                               |

|    |         |         |                    |    |    |         |         |         |   |         |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|
|    |         |         | Fill               |    |    |         |         |         |   |         |
| 15 | 2.26432 | 2593.56 | Structural<br>Fill | 50 | 36 | 411.802 | 696.76  | 890.189 | 0 | 890.189 |
| 16 | 2.26432 | 2327.15 | Structural<br>Fill | 50 | 36 | 363.125 | 614.401 | 776.831 | 0 | 776.831 |
| 17 | 2.26432 | 2839.11 | Structural<br>Fill | 50 | 36 | 510.999 | 864.6   | 1121.2  | 0 | 1121.2  |
| 18 | 2.26432 | 3879.31 | Structural<br>Fill | 50 | 36 | 555.264 | 939.496 | 1224.29 | 0 | 1224.29 |
| 19 | 2.26432 | 3634.81 | Structural<br>Fill | 50 | 36 | 507.876 | 859.316 | 1113.93 | 0 | 1113.93 |
| 20 | 2.26432 | 3062.63 | Structural<br>Fill | 50 | 36 | 420.392 | 711.295 | 910.193 | 0 | 910.193 |
| 21 | 2.26432 | 2586.16 | Structural<br>Fill | 50 | 36 | 349.157 | 590.767 | 744.303 | 0 | 744.303 |
| 22 | 2.26432 | 2076.84 | Structural<br>Fill | 50 | 36 | 349.683 | 591.657 | 745.527 | 0 | 745.527 |
| 23 | 2.26432 | 1532.11 | Structural<br>Fill | 50 | 36 | 213.766 | 361.688 | 429.004 | 0 | 429.004 |
| 24 | 2.26432 | 948.923 | Structural<br>Fill | 50 | 36 | 198.845 | 336.442 | 394.254 | 0 | 394.254 |
| 25 | 2.26432 | 323.654 | Structural<br>Fill | 50 | 36 | 125.891 | 213.005 | 224.357 | 0 | 224.357 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.69198

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 407.159           | 8648.78                    | 0                             | 0                            | 0                                |
| 2            | 409.424           | 8649.08                    | 113.377                       | 61.9434                      | 28.6499                          |
| 3            | 411.688           | 8649.45                    | 286.172                       | 156.35                       | 28.65                            |
| 4            | 413.952           | 8649.87                    | 499.275                       | 272.778                      | 28.6499                          |
| 5            | 416.217           | 8650.34                    | 735.955                       | 402.088                      | 28.6499                          |
| 6            | 418.481           | 8650.88                    | 967.933                       | 528.829                      | 28.6499                          |
| 7            | 420.745           | 8651.47                    | 1161.6                        | 634.641                      | 28.65                            |
| 8            | 423.01            | 8652.13                    | 1415.51                       | 773.363                      | 28.65                            |
| 9            | 425.274           | 8652.85                    | 1677.88                       | 916.707                      | 28.6499                          |
| 10           | 427.538           | 8653.63                    | 1864.9                        | 1018.89                      | 28.65                            |
| 11           | 429.802           | 8654.48                    | 2001.22                       | 1093.37                      | 28.6501                          |
| 12           | 432.067           | 8655.39                    | 2171.29                       | 1186.28                      | 28.6499                          |
| 13           | 434.331           | 8656.38                    | 2226.58                       | 1216.49                      | 28.6499                          |
| 14           | 436.595           | 8657.44                    | 2315.25                       | 1264.93                      | 28.6499                          |
| 15           | 438.86            | 8658.57                    | 2215.11                       | 1210.23                      | 28.6501                          |
| 16           | 441.124           | 8659.78                    | 2070.95                       | 1131.46                      | 28.6499                          |
| 17           | 443.388           | 8661.07                    | 1890.54                       | 1032.9                       | 28.6501                          |
| 18           | 445.653           | 8662.44                    | 2638.59                       | 1441.59                      | 28.6499                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 19 | 447.917 | 8663.91 | 2101.65 | 1148.24 | 28.6501 |
| 20 | 450.181 | 8665.47 | 1513.53 | 826.913 | 28.6499 |
| 21 | 452.446 | 8667.13 | 953.506 | 520.947 | 28.6499 |
| 22 | 454.71  | 8668.9  | 427.666 | 233.655 | 28.65   |
| 23 | 456.974 | 8670.78 | 948.256 | 518.079 | 28.65   |
| 24 | 459.239 | 8672.79 | 573.176 | 313.154 | 28.6499 |
| 25 | 461.503 | 8674.94 | 201.529 | 110.105 | 28.6499 |
| 26 | 463.767 | 8677.23 | 0       | 0       | 0       |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 473.862 | 8677.66 |
| 458.966 | 8677.03 |

### External Boundary

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |

|         |         |
|---------|---------|
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |
| 370.173 | 8638.84 |
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |
| 354.671 | 8629.53 |
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

|  |  |
|--|--|
|  |  |
|--|--|

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |
| 382.29  | 8647.38 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |

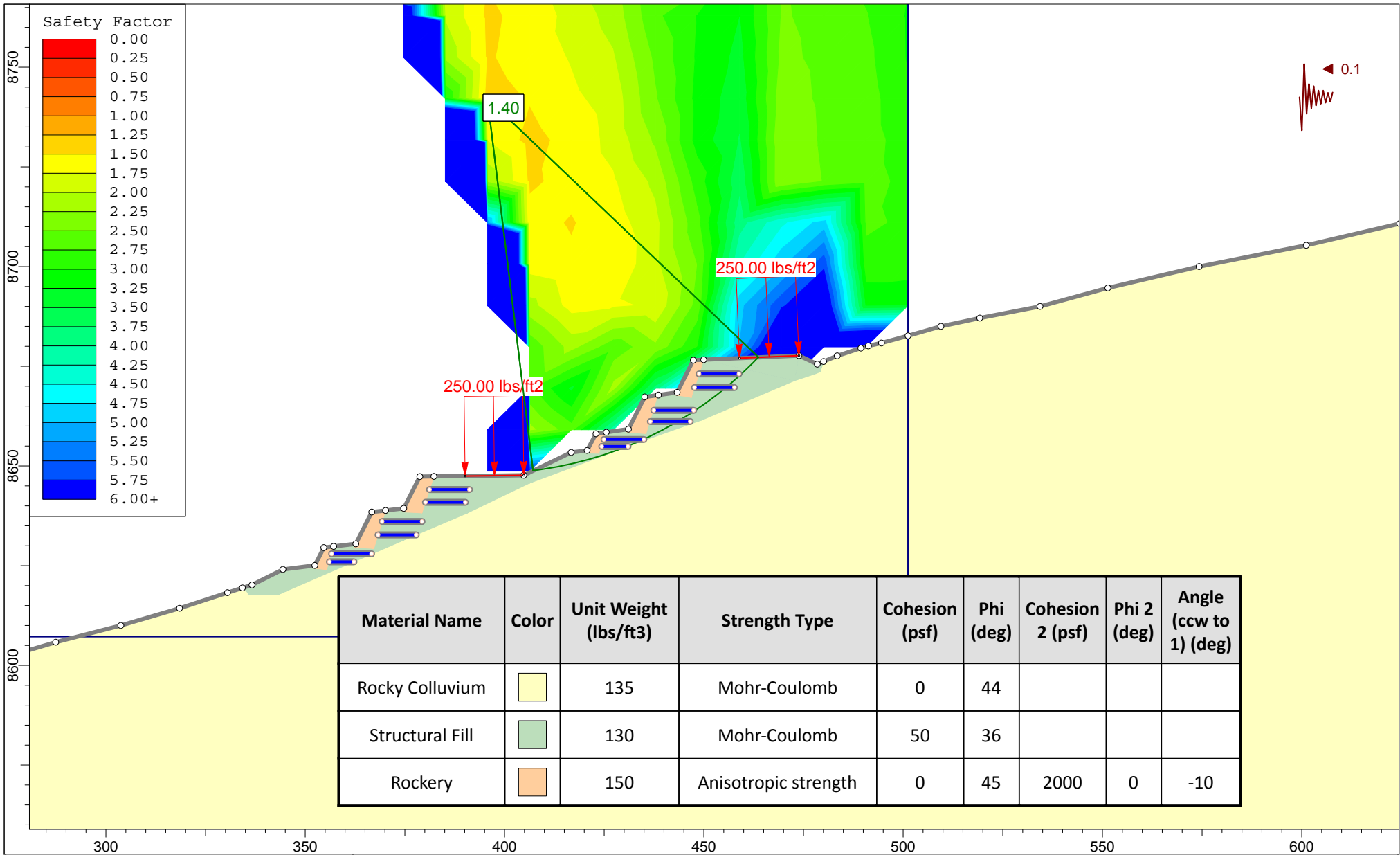
### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |



**Material Boundary**

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



|  |   |   |                              |
|--|---|---|------------------------------|
|  | <b>Project</b><br>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G                    |   |                              |
|  | <b>Analysis Description</b><br>GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 4-4' |   |                              |
|  | <b>Drawn By</b><br>SL   | <b>Scale</b><br>1:400                     | <b>Company</b><br>IGES, INC. |
|  | <b>Date</b><br>9-25-2015  | <b>File Name</b><br>P-Static - upper.slim |                              |

# ***Slide Analysis Information***

## ***SLIDE - An Interactive Slope Stability Program***

### ***Project Summary***

---

File Name: P-Static - upper  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### ***General Settings***

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### ***Analysis Options***

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### ***Groundwater Analysis***

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### ***Random Numbers***

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present




### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties


| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |

## Support Properties

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

### Global Minimums

---

**Method: spencer**

FS: 1.397710  
 Center: 395.690, 8742.134  
 Radius: 94.059  
 Left Slip Surface Endpoint: 407.159, 8648.778  
 Right Slip Surface Endpoint: 463.767, 8677.231  
 Resisting Moment=3.43634e+006 lb-ft  
 Driving Moment=2.45855e+006 lb-ft  
 Resisting Horizontal Force=33020.2 lb  
 Driving Horizontal Force=23624.5 lb  
 Total Slice Area=337.324 ft<sup>2</sup>

### Valid / Invalid Surfaces

---

**Method: spencer**

Number of Valid Surfaces: 1490  
 Number of Invalid Surfaces: 3526

**Error Codes:**

Error Code -103 reported for 11 surfaces  
 Error Code -106 reported for 45 surfaces  
 Error Code -107 reported for 4 surfaces  
 Error Code -108 reported for 101 surfaces  
 Error Code -111 reported for 85 surfaces  
 Error Code -112 reported for 453 surfaces  
 Error Code -113 reported for 275 surfaces  
 Error Code -1000 reported for 2552 surfaces

## Error Codes

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 113 = Surface intersects outside slope limits.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.39771

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.26432    | 115.474      | Structural Fill | 50                  | 36                            | 80.9219            | 113.105              | 86.8572                  | 0                   | 86.8572                       |
| 2            | 2.26432    | 338.134      | Structural Fill | 50                  | 36                            | 136.754            | 191.143              | 194.267                  | 0                   | 194.267                       |
| 3            | 2.26432    | 544.122      | Structural Fill | 50                  | 36                            | 184.363            | 257.686              | 285.855                  | 0                   | 285.855                       |
| 4            | 2.26432    | 733.223      | Structural Fill | 50                  | 36                            | 224.411            | 313.662              | 362.9                    | 0                   | 362.9                         |
| 5            | 2.26432    | 834.07       | Structural Fill | 50                  | 36                            | 240.898            | 336.706              | 394.616                  | 0                   | 394.616                       |
| 6            | 2.26432    | 760.941      | Structural Fill | 50                  | 36                            | 216.846            | 303.088              | 348.346                  | 0                   | 348.346                       |
| 7            | 2.26432    | 1389.96      | Structural Fill | 50                  | 36                            | 346.937            | 484.918              | 598.612                  | 0                   | 598.612                       |
| 8            | 2.26432    | 1863.22      | Structural Fill | 50                  | 36                            | 435.152            | 608.217              | 768.318                  | 0                   | 768.318                       |
| 9            | 2.26432    | 1568.42      | Structural Fill | 50                  | 36                            | 361.218            | 504.878              | 626.083                  | 0                   | 626.083                       |
| 10           | 2.26432    | 1420.12      | Structural Fill | 50                  | 36                            | 320.577            | 448.074              | 547.903                  | 0                   | 547.903                       |
| 11           | 2.26432    | 1411.45      | Structural Fill | 50                  | 36                            | 322.359            | 450.564              | 551.33                   | 0                   | 551.33                        |
| 12           | 2.26432    | 2453.61      | Structural Fill | 50                  | 36                            | 489.263            | 683.848              | 872.419                  | 0                   | 872.419                       |
|              |            |              | Structural      |                     |                               |                    |                      |                          |                     |                               |

|    |         |         |                    |    |    |         |         |         |   |         |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|
|    |         |         | Fill               |    |    |         |         |         |   |         |
| 14 | 2.26432 | 2972.27 | Structural<br>Fill | 50 | 36 | 546.012 | 763.167 | 981.591 | 0 | 981.591 |
| 15 | 2.26432 | 2593.56 | Structural<br>Fill | 50 | 36 | 465.6   | 650.774 | 826.896 | 0 | 826.896 |
| 16 | 2.26432 | 2327.15 | Structural<br>Fill | 50 | 36 | 407.854 | 570.061 | 715.8   | 0 | 715.8   |
| 17 | 2.26432 | 2839.11 | Structural<br>Fill | 50 | 36 | 647.502 | 905.02  | 1176.83 | 0 | 1176.83 |
| 18 | 2.26432 | 3879.31 | Structural<br>Fill | 50 | 36 | 610.337 | 853.074 | 1105.34 | 0 | 1105.34 |
| 19 | 2.26432 | 3634.81 | Structural<br>Fill | 50 | 36 | 554.404 | 774.896 | 997.732 | 0 | 997.732 |
| 20 | 2.26432 | 3062.63 | Structural<br>Fill | 50 | 36 | 456.497 | 638.051 | 809.382 | 0 | 809.382 |
| 21 | 2.26432 | 2586.16 | Structural<br>Fill | 50 | 36 | 377.432 | 527.54  | 657.278 | 0 | 657.278 |
| 22 | 2.26432 | 2076.84 | Structural<br>Fill | 50 | 36 | 439.5   | 614.294 | 776.685 | 0 | 776.685 |
| 23 | 2.26432 | 1532.11 | Structural<br>Fill | 50 | 36 | 231.084 | 322.988 | 375.735 | 0 | 375.735 |
| 24 | 2.26432 | 948.923 | Structural<br>Fill | 50 | 36 | 219.305 | 306.525 | 353.077 | 0 | 353.077 |
| 25 | 2.26432 | 323.654 | Structural<br>Fill | 50 | 36 | 142.117 | 198.639 | 204.584 | 0 | 204.584 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.39771

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 407.159           | 8648.78                    | 0                             | 0                            | 0                                |
| 2            | 409.424           | 8649.08                    | 145.348                       | 111.895                      | 37.5906                          |
| 3            | 411.688           | 8649.45                    | 351.206                       | 270.372                      | 37.5905                          |
| 4            | 413.952           | 8649.87                    | 594.93                        | 458.001                      | 37.5905                          |
| 5            | 416.217           | 8650.34                    | 857.279                       | 659.968                      | 37.5905                          |
| 6            | 418.481           | 8650.88                    | 1108.64                       | 853.477                      | 37.5906                          |
| 7            | 420.745           | 8651.47                    | 1316.78                       | 1013.71                      | 37.5905                          |
| 8            | 423.01            | 8652.13                    | 1571.49                       | 1209.8                       | 37.5906                          |
| 9            | 425.274           | 8652.85                    | 1819.7                        | 1400.87                      | 37.5904                          |
| 10           | 427.538           | 8653.63                    | 1992.04                       | 1533.55                      | 37.5905                          |
| 11           | 429.802           | 8654.48                    | 2112.38                       | 1626.19                      | 37.5904                          |
| 12           | 432.067           | 8655.39                    | 2284.23                       | 1758.49                      | 37.5905                          |
| 13           | 434.331           | 8656.38                    | 2289.12                       | 1762.26                      | 37.5906                          |
| 14           | 436.595           | 8657.44                    | 2333.06                       | 1796.09                      | 37.5906                          |
| 15           | 438.86            | 8658.57                    | 2163.32                       | 1665.41                      | 37.5905                          |
| 16           | 441.124           | 8659.78                    | 1959.84                       | 1508.77                      | 37.5906                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 17 | 443.388 | 8661.07 | 1728.24 | 1330.47 | 37.5906 |
| 18 | 445.653 | 8662.44 | 2665.92 | 2052.33 | 37.5905 |
| 19 | 447.917 | 8663.91 | 2042.28 | 1572.23 | 37.5905 |
| 20 | 450.181 | 8665.47 | 1379.33 | 1061.86 | 37.5904 |
| 21 | 452.446 | 8667.13 | 763.9   | 588.081 | 37.5905 |
| 22 | 454.71  | 8668.9  | 198.746 | 153.003 | 37.5906 |
| 23 | 456.974 | 8670.78 | 896.568 | 690.214 | 37.5905 |
| 24 | 459.239 | 8672.79 | 515.349 | 396.736 | 37.5905 |
| 25 | 461.503 | 8674.94 | 184.275 | 141.862 | 37.5905 |
| 26 | 463.767 | 8677.23 | 0       | 0       | 0       |

## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 473.862 | 8677.66 |
| 458.966 | 8677.03 |

### External Boundary

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |



|         |         |
|---------|---------|
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |
| 370.173 | 8638.84 |
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |
| 354.671 | 8629.53 |
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |
| 382.29  | 8647.38 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

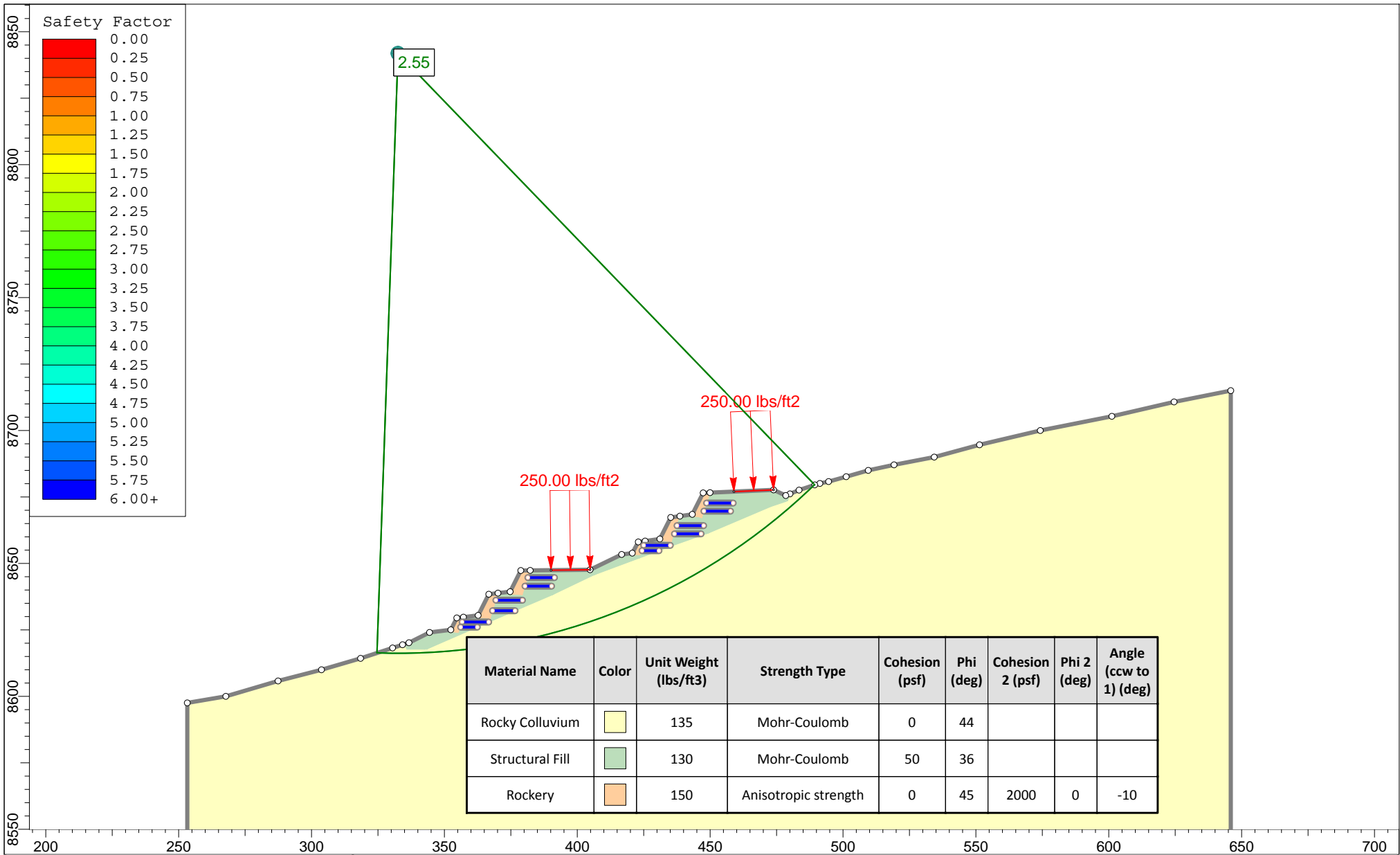
| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |


### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |

## Material Boundary

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



|  |                      |           |           |   |         |            |
|--|----------------------|-----------|-----------|---|---------|------------|
|  | Project              |           |           | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G      |         |            |
|  | Analysis Description |           |           | GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 4-4' |         |            |
|  | Drawn By             | SL        | Scale     | 1:600   | Company | IGES, INC. |
|  | Date                 | 9-25-2015 | File Name | Static - entire.slim  |         |            |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: Static - entire  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Support Properties

---

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material        | Adhesion (psf) | Friction Angle (deg) |
|-----------------|----------------|----------------------|
| Structural Fill | 50             | 36                   |

**Global Minimums**

**Method: spencer**

FS: 2.553450  
 Center: 332.561, 8841.888  
 Radius: 225.731  
 Left Slip Surface Endpoint: 324.610, 8616.297  
 Right Slip Surface Endpoint: 489.397, 8679.540  
 Resisting Moment=7.81297e+007 lb-ft  
 Driving Moment=3.05977e+007 lb-ft  
 Resisting Horizontal Force=318508 lb  
 Driving Horizontal Force=124736 lb  
 Total Slice Area=2751.56 ft<sup>2</sup>

**Valid / Invalid Surfaces**

**Method: spencer**

Number of Valid Surfaces: 1  
 Number of Invalid Surfaces: 0

**Slice Data**

**Global Minimum Query (spencer) - Safety Factor: 2.55345**

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 6.59151    | 1014.26      | Rocky Colluvium | 0                   | 44                            | 69.2424            | 176.807              | 183.089                  | 0                   | 183.089                       |
| 2            | 6.59151    | 2918.32      | Rocky Colluvium | 0                   | 44                            | 194.207            | 495.899              | 513.519                  | 0                   | 513.519                       |

|    |         |         |                 |   |    |         |         |         |   |         |
|----|---------|---------|-----------------|---|----|---------|---------|---------|---|---------|
| 3  | 6.59151 | 5234.42 | Rocky Colluvium | 0 | 44 | 339.726 | 867.474 | 898.296 | 0 | 898.296 |
| 4  | 6.59151 | 6766.53 | Rocky Colluvium | 0 | 44 | 428.491 | 1094.13 | 1133    | 0 | 1133    |
| 5  | 6.59151 | 9598.78 | Rocky Colluvium | 0 | 44 | 593.28  | 1514.91 | 1568.73 | 0 | 1568.73 |
| 6  | 6.59151 | 11108.4 | Rocky Colluvium | 0 | 44 | 670.332 | 1711.66 | 1772.48 | 0 | 1772.48 |
| 7  | 6.59151 | 17033.7 | Rocky Colluvium | 0 | 44 | 1003.79 | 2563.13 | 2654.2  | 0 | 2654.2  |
| 8  | 6.59151 | 17887.8 | Rocky Colluvium | 0 | 44 | 1029.58 | 2628.97 | 2722.38 | 0 | 2722.38 |
| 9  | 6.59151 | 23027   | Rocky Colluvium | 0 | 44 | 1294.64 | 3305.81 | 3423.27 | 0 | 3423.27 |
| 10 | 6.59151 | 21482.7 | Rocky Colluvium | 0 | 44 | 1185.51 | 3027.15 | 3134.71 | 0 | 3134.71 |
| 11 | 6.59151 | 20090.2 | Rocky Colluvium | 0 | 44 | 1166.66 | 2979.01 | 3084.85 | 0 | 3084.85 |
| 12 | 6.59151 | 18511.4 | Rocky Colluvium | 0 | 44 | 1056.81 | 2698.52 | 2794.39 | 0 | 2794.39 |
| 13 | 6.59151 | 17643.6 | Rocky Colluvium | 0 | 44 | 917.382 | 2342.49 | 2425.72 | 0 | 2425.72 |
| 14 | 6.59151 | 18255.3 | Rocky Colluvium | 0 | 44 | 912.217 | 2329.3  | 2412.06 | 0 | 2412.06 |
| 15 | 6.59151 | 18664.3 | Rocky Colluvium | 0 | 44 | 910.384 | 2324.62 | 2407.21 | 0 | 2407.21 |
| 16 | 6.59151 | 19367.5 | Rocky Colluvium | 0 | 44 | 921.78  | 2353.72 | 2437.35 | 0 | 2437.35 |
| 17 | 6.59151 | 21436.9 | Rocky Colluvium | 0 | 44 | 995.073 | 2540.87 | 2631.15 | 0 | 2631.15 |
| 18 | 6.59151 | 21689.6 | Rocky Colluvium | 0 | 44 | 981.382 | 2505.91 | 2594.95 | 0 | 2594.95 |
| 19 | 6.59151 | 24113.9 | Rocky Colluvium | 0 | 44 | 1062.82 | 2713.85 | 2810.27 | 0 | 2810.27 |
| 20 | 6.59151 | 22397.1 | Rocky Colluvium | 0 | 44 | 960.802 | 2453.36 | 2540.52 | 0 | 2540.52 |
| 21 | 6.59151 | 18874.5 | Rocky Colluvium | 0 | 44 | 830.402 | 2120.39 | 2195.73 | 0 | 2195.73 |
| 22 | 6.59151 | 15047.8 | Rocky Colluvium | 0 | 44 | 677.519 | 1730.01 | 1791.47 | 0 | 1791.47 |
| 23 | 6.59151 | 10708.5 | Rocky Colluvium | 0 | 44 | 463.154 | 1182.64 | 1224.65 | 0 | 1224.65 |
| 24 | 6.59151 | 5033.18 | Rocky Colluvium | 0 | 44 | 191.548 | 489.107 | 506.485 | 0 | 506.485 |
| 25 | 6.59151 | 1765.47 | Rocky Colluvium | 0 | 44 | 67.0293 | 171.156 | 177.237 | 0 | 177.237 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 2.55345



| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 324.61            | 8616.3                     | 0                             | 0                            | 0                                |
| 2            | 331.201           | 8616.16                    | 481.302                       | 186.464                      | 21.1772                          |
| 3            | 337.793           | 8616.22                    | 1732.36                       | 671.146                      | 21.1772                          |
| 4            | 344.384           | 8616.47                    | 3747.76                       | 1451.94                      | 21.1771                          |
| 5            | 350.976           | 8616.91                    | 6070.72                       | 2351.9                       | 21.1772                          |
| 6            | 357.567           | 8617.55                    | 8981.99                       | 3479.77                      | 21.1772                          |
| 7            | 364.159           | 8618.38                    | 11923.8                       | 4619.46                      | 21.1771                          |
| 8            | 370.75            | 8619.41                    | 15802.5                       | 6122.15                      | 21.1772                          |
| 9            | 377.342           | 8620.64                    | 19233.4                       | 7451.34                      | 21.1772                          |
| 10           | 383.933           | 8622.08                    | 22847.7                       | 8851.56                      | 21.1772                          |
| 11           | 390.525           | 8623.73                    | 25504.8                       | 9880.99                      | 21.1772                          |
| 12           | 397.116           | 8625.58                    | 27480.6                       | 10646.4                      | 21.1771                          |
| 13           | 403.708           | 8627.66                    | 28660.7                       | 11103.6                      | 21.1771                          |
| 14           | 410.299           | 8629.97                    | 29124.7                       | 11283.4                      | 21.1772                          |
| 15           | 416.891           | 8632.5                     | 29021.4                       | 11243.4                      | 21.1772                          |
| 16           | 423.482           | 8635.28                    | 28337.6                       | 10978.4                      | 21.1771                          |
| 17           | 430.074           | 8638.31                    | 27033.1                       | 10473                        | 21.1771                          |
| 18           | 436.665           | 8641.6                     | 24934.1                       | 9659.86                      | 21.1771                          |
| 19           | 443.257           | 8645.16                    | 22148.5                       | 8580.7                       | 21.1772                          |
| 20           | 449.848           | 8649.02                    | 18314.1                       | 7095.17                      | 21.1772                          |
| 21           | 456.44            | 8653.19                    | 14063                         | 5448.25                      | 21.1772                          |
| 22           | 463.031           | 8657.68                    | 9707.9                        | 3761                         | 21.1772                          |
| 23           | 469.623           | 8662.53                    | 5554.05                       | 2151.73                      | 21.1772                          |
| 24           | 476.214           | 8667.77                    | 2241.1                        | 868.24                       | 21.1772                          |
| 25           | 482.806           | 8673.42                    | 639.635                       | 247.805                      | 21.1772                          |
| 26           | 489.397           | 8679.54                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 473.862 | 8677.66 |
| 458.966 | 8677.03 |

### External Boundary

|  |
|--|
|  |
|--|

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |
| 370.173 | 8638.84 |
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |
| 354.671 | 8629.53 |

|         |         |
|---------|---------|
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |
| 382.29  | 8647.38 |

### Material Boundary

| X | Y |
|---|---|
|   |   |

|         |         |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

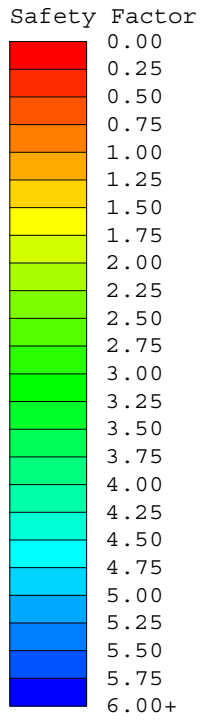
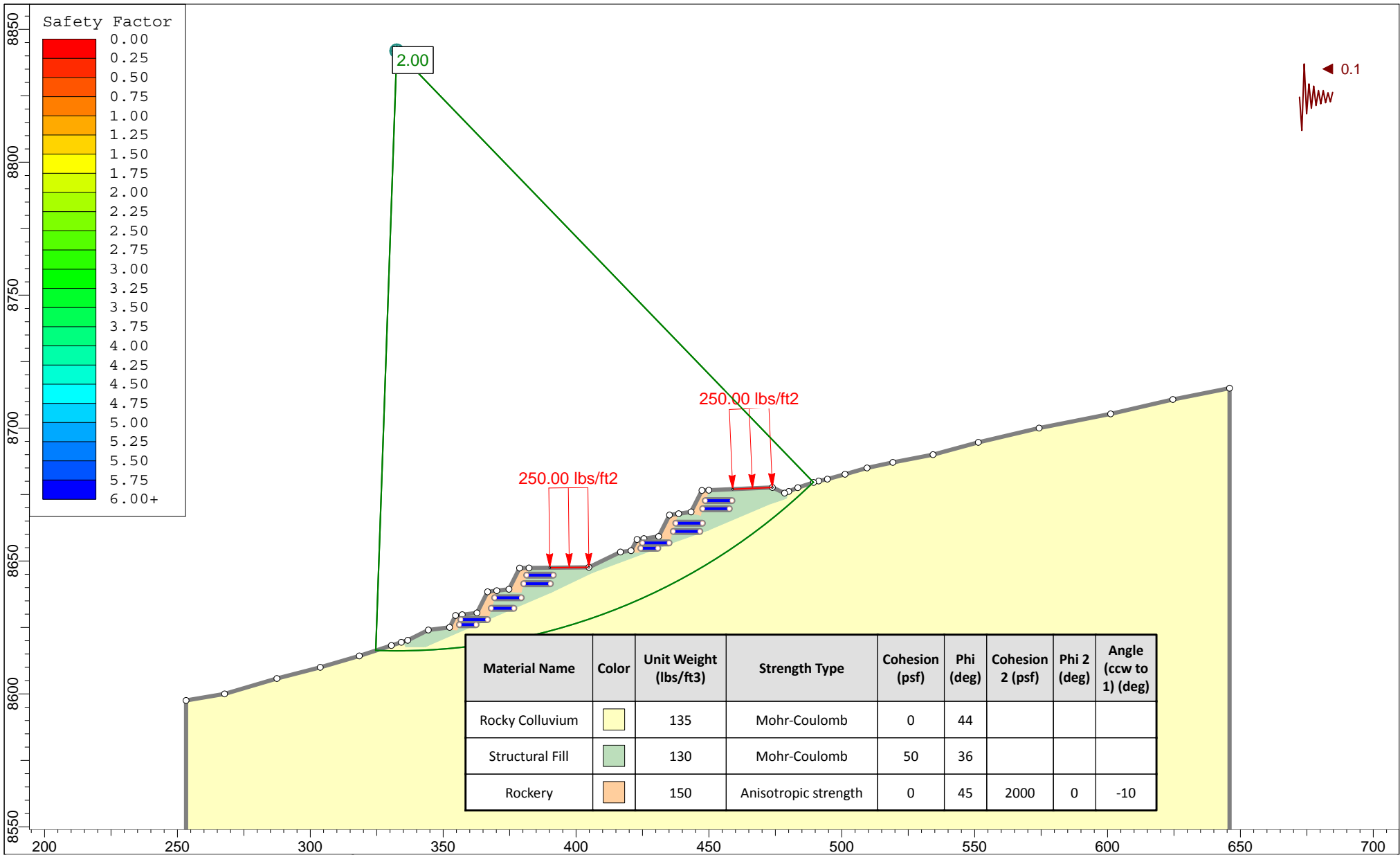
| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



| Material Name   | Color | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|-------|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |       | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |       | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |       | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |



SLIDEINTERPRET 6.029

|  |            |                  |                        |
|--|------------|------------------|------------------------|
| <i>Project</i>   |            |                  |                        |
| ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G       |            |                  |                        |
| <i>Analysis Description</i>                                  |            |                  |                        |
| GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 4-4' |            |                  |                        |
| <i>Drawn By</i>  | SL         | <i>Scale</i>     | 1:600                  |
| <i>Company</i>   | IGES, INC. |                  |                        |
| <i>Date</i>  | 9-25-2015  | <i>File Name</i> | P-Static - entire.slim |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: P-Static - entire  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |

## Support Properties

---

**Mirafi 3XT**

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

**Pullout Strength Dependency:**

| Material        | Adhesion (psf) | Friction Angle (deg) |
|-----------------|----------------|----------------------|
| Structural Fill | 50             | 36                   |

**Global Minimums**

**Method: spencer**

FS: 1.995270  
 Center: 332.561, 8841.888  
 Radius: 225.731  
 Left Slip Surface Endpoint: 324.610, 8616.297  
 Right Slip Surface Endpoint: 489.397, 8679.540  
 Resisting Moment=7.55532e+007 lb-ft  
 Driving Moment=3.78661e+007 lb-ft  
 Resisting Horizontal Force=308858 lb  
 Driving Horizontal Force=154795 lb  
 Total Slice Area=2751.56 ft<sup>2</sup>

**Valid / Invalid Surfaces**

**Method: spencer**

Number of Valid Surfaces: 1  
 Number of Invalid Surfaces: 0

**Slice Data**

**Global Minimum Query (spencer) - Safety Factor: 1.99527**

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 6.59151    | 1014.26      | Rocky Colluvium | 0                   | 44                            | 96.1765            | 191.898              | 198.716                  | 0                   | 198.716                       |



|    |         |         |                 |   |    |         |         |         |   |         |
|----|---------|---------|-----------------|---|----|---------|---------|---------|---|---------|
| 2  | 6.59151 | 2918.32 | Rocky Colluvium | 0 | 44 | 266.757 | 532.252 | 551.163 | 0 | 551.163 |
| 3  | 6.59151 | 5234.42 | Rocky Colluvium | 0 | 44 | 461.64  | 921.097 | 953.825 | 0 | 953.825 |
| 4  | 6.59151 | 6766.53 | Rocky Colluvium | 0 | 44 | 576.228 | 1149.73 | 1190.58 | 0 | 1190.58 |
| 5  | 6.59151 | 9598.78 | Rocky Colluvium | 0 | 44 | 789.828 | 1575.92 | 1631.92 | 0 | 1631.92 |
| 6  | 6.59151 | 11108.4 | Rocky Colluvium | 0 | 44 | 883.71  | 1763.24 | 1825.89 | 0 | 1825.89 |
| 7  | 6.59151 | 17033.7 | Rocky Colluvium | 0 | 44 | 1310.76 | 2615.32 | 2708.24 | 0 | 2708.24 |
| 8  | 6.59151 | 17887.8 | Rocky Colluvium | 0 | 44 | 1332    | 2657.69 | 2752.11 | 0 | 2752.11 |
| 9  | 6.59151 | 23027   | Rocky Colluvium | 0 | 44 | 1659.8  | 3311.74 | 3429.4  | 0 | 3429.4  |
| 10 | 6.59151 | 21482.7 | Rocky Colluvium | 0 | 44 | 1506.86 | 3006.6  | 3113.43 | 0 | 3113.43 |
| 11 | 6.59151 | 20090.2 | Rocky Colluvium | 0 | 44 | 1476.03 | 2945.08 | 3049.72 | 0 | 3049.72 |
| 12 | 6.59151 | 18511.4 | Rocky Colluvium | 0 | 44 | 1326.15 | 2646.02 | 2740.03 | 0 | 2740.03 |
| 13 | 6.59151 | 17643.6 | Rocky Colluvium | 0 | 44 | 1137.24 | 2269.11 | 2349.74 | 0 | 2349.74 |
| 14 | 6.59151 | 18255.3 | Rocky Colluvium | 0 | 44 | 1120.52 | 2235.74 | 2315.18 | 0 | 2315.18 |
| 15 | 6.59151 | 18664.3 | Rocky Colluvium | 0 | 44 | 1109.18 | 2213.11 | 2291.74 | 0 | 2291.74 |
| 16 | 6.59151 | 19367.5 | Rocky Colluvium | 0 | 44 | 1114.04 | 2222.82 | 2301.8  | 0 | 2301.8  |
| 17 | 6.59151 | 21436.9 | Rocky Colluvium | 0 | 44 | 1193.07 | 2380.5  | 2465.07 | 0 | 2465.07 |
| 18 | 6.59151 | 21689.6 | Rocky Colluvium | 0 | 44 | 1167.4  | 2329.27 | 2412.03 | 0 | 2412.03 |
| 19 | 6.59151 | 24113.9 | Rocky Colluvium | 0 | 44 | 1254.39 | 2502.85 | 2591.77 | 0 | 2591.77 |
| 20 | 6.59151 | 22397.1 | Rocky Colluvium | 0 | 44 | 1125.2  | 2245.07 | 2324.84 | 0 | 2324.84 |
| 21 | 6.59151 | 18874.5 | Rocky Colluvium | 0 | 44 | 968.074 | 1931.57 | 2000.21 | 0 | 2000.21 |
| 22 | 6.59151 | 15047.8 | Rocky Colluvium | 0 | 44 | 786.094 | 1568.47 | 1624.19 | 0 | 1624.19 |
| 23 | 6.59151 | 10708.5 | Rocky Colluvium | 0 | 44 | 532.975 | 1063.43 | 1101.21 | 0 | 1101.21 |
| 24 | 6.59151 | 5033.18 | Rocky Colluvium | 0 | 44 | 217.538 | 434.048 | 449.469 | 0 | 449.469 |
| 25 | 6.59151 | 1765.47 | Rocky Colluvium | 0 | 44 | 72.3446 | 144.347 | 149.476 | 0 | 149.476 |

## Interslice Data

**Global Minimum Query (spencer) - Safety Factor: 1.99527**

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 324.61            | 8616.3                     | 0                             | 0                            | 0                                |
| 2            | 331.201           | 8616.16                    | 560.842                       | 296.172                      | 27.8378                          |
| 3            | 337.793           | 8616.22                    | 1999.78                       | 1056.05                      | 27.8378                          |
| 4            | 344.384           | 8616.47                    | 4287.78                       | 2264.31                      | 27.8378                          |
| 5            | 350.976           | 8616.91                    | 6890.25                       | 3638.64                      | 27.8379                          |
| 6            | 357.567           | 8617.55                    | 10107.7                       | 5337.72                      | 27.8378                          |
| 7            | 364.159           | 8618.38                    | 13312.6                       | 7030.18                      | 27.8378                          |
| 8            | 370.75            | 8619.41                    | 17473.5                       | 9227.46                      | 27.8378                          |
| 9            | 377.342           | 8620.64                    | 21090.5                       | 11137.6                      | 27.8379                          |
| 10           | 383.933           | 8622.08                    | 24822.7                       | 13108.5                      | 27.8379                          |
| 11           | 390.525           | 8623.73                    | 27505.3                       | 14525.1                      | 27.8378                          |
| 12           | 397.116           | 8625.58                    | 29596.6                       | 15629.5                      | 27.8378                          |
| 13           | 403.708           | 8627.66                    | 30831.8                       | 16281.8                      | 27.8378                          |
| 14           | 410.299           | 8629.97                    | 31171.2                       | 16461                        | 27.8378                          |
| 15           | 416.891           | 8632.5                     | 30876.3                       | 16305.3                      | 27.8378                          |
| 16           | 423.482           | 8635.28                    | 29972.2                       | 15827.8                      | 27.8378                          |
| 17           | 430.074           | 8638.31                    | 28423.8                       | 15010.2                      | 27.8379                          |
| 18           | 436.665           | 8641.6                     | 26048.9                       | 13756                        | 27.8378                          |
| 19           | 443.257           | 8645.16                    | 22988.8                       | 12140                        | 27.8378                          |
| 20           | 449.848           | 8649.02                    | 18865.6                       | 9962.6                       | 27.8378                          |
| 21           | 456.44            | 8653.19                    | 14372.3                       | 7589.8                       | 27.8379                          |
| 22           | 463.031           | 8657.68                    | 9929.46                       | 5243.59                      | 27.8378                          |
| 23           | 469.623           | 8662.53                    | 5808.58                       | 3067.42                      | 27.8378                          |
| 24           | 476.214           | 8667.77                    | 2538.46                       | 1340.52                      | 27.8378                          |
| 25           | 482.806           | 8673.42                    | 930.359                       | 491.308                      | 27.8378                          |
| 26           | 489.397           | 8679.54                    | 0                             | 0                            | 0                                |

**List Of Coordinates**

**Distributed Load**

| X       | Y       |
|---------|---------|
| 404.829 | 8647.66 |
| 390.115 | 8647.48 |

**Distributed Load**

| X       | Y       |
|---------|---------|
| 473.862 | 8677.66 |
| 458.966 | 8677.03 |

**External Boundary**

| X       | Y       |
|---------|---------|
| 336.648 | 8620.18 |
| 334.248 | 8619.41 |
| 330.517 | 8618.22 |
| 318.467 | 8614.3  |
| 303.763 | 8610    |
| 287.416 | 8605.81 |
| 267.75  | 8600    |
| 253.242 | 8597.56 |
| 253.242 | 8472.79 |
| 645.903 | 8472.79 |
| 645.903 | 8715    |
| 624.575 | 8710.77 |
| 601.156 | 8705.33 |
| 574.249 | 8700    |
| 551.356 | 8694.63 |
| 534.337 | 8690    |
| 519.227 | 8687.08 |
| 509.483 | 8685    |
| 501.223 | 8682.65 |
| 494.567 | 8680.82 |
| 491.297 | 8680.1  |
| 489.397 | 8679.54 |
| 483.474 | 8677.61 |
| 480.052 | 8676.19 |
| 478.466 | 8675.53 |
| 473.862 | 8677.66 |
| 449.973 | 8676.65 |
| 447.379 | 8676.54 |
| 443.306 | 8668.45 |
| 438.615 | 8667.79 |
| 435.161 | 8667.3  |
| 431.088 | 8659.22 |
| 425.543 | 8658.44 |
| 422.943 | 8658.07 |
| 420.729 | 8653.89 |
| 416.729 | 8653.39 |
| 404.829 | 8647.66 |
| 382.29  | 8647.38 |
| 378.747 | 8647.34 |
| 374.734 | 8639.37 |
| 370.173 | 8638.84 |
| 366.709 | 8638.43 |
| 362.696 | 8630.46 |
| 357.151 | 8629.82 |

|         |         |
|---------|---------|
| 354.671 | 8629.53 |
| 352.422 | 8625.06 |
| 344.422 | 8624.06 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 334.248 | 8619.41 |
| 335.8   | 8617.72 |
| 343.202 | 8617.72 |
| 376.173 | 8632.02 |
| 390.511 | 8638.12 |
| 406.184 | 8645.63 |
| 423.426 | 8652.06 |
| 434.631 | 8656.28 |
| 449.753 | 8661.59 |
| 472.773 | 8671.38 |
| 478.006 | 8673.12 |
| 479.175 | 8673.61 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 352.422 | 8625.06 |
| 352.073 | 8624.37 |
| 355.55  | 8623.97 |
| 357.151 | 8629.82 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 362.696 | 8630.46 |
| 362.246 | 8629.57 |
| 367.238 | 8629.29 |
| 370.173 | 8638.84 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 374.734 | 8639.37 |
| 374.284 | 8638.48 |
| 379.278 | 8638.22 |
| 382.29  | 8647.38 |

### Material Boundary

|  |  |
|--|--|
|  |  |
|--|--|

| X       | Y       |
|---------|---------|
| 420.729 | 8653.89 |
| 420.291 | 8653.06 |
| 423.79  | 8652.97 |
| 425.543 | 8658.44 |

### Material Boundary

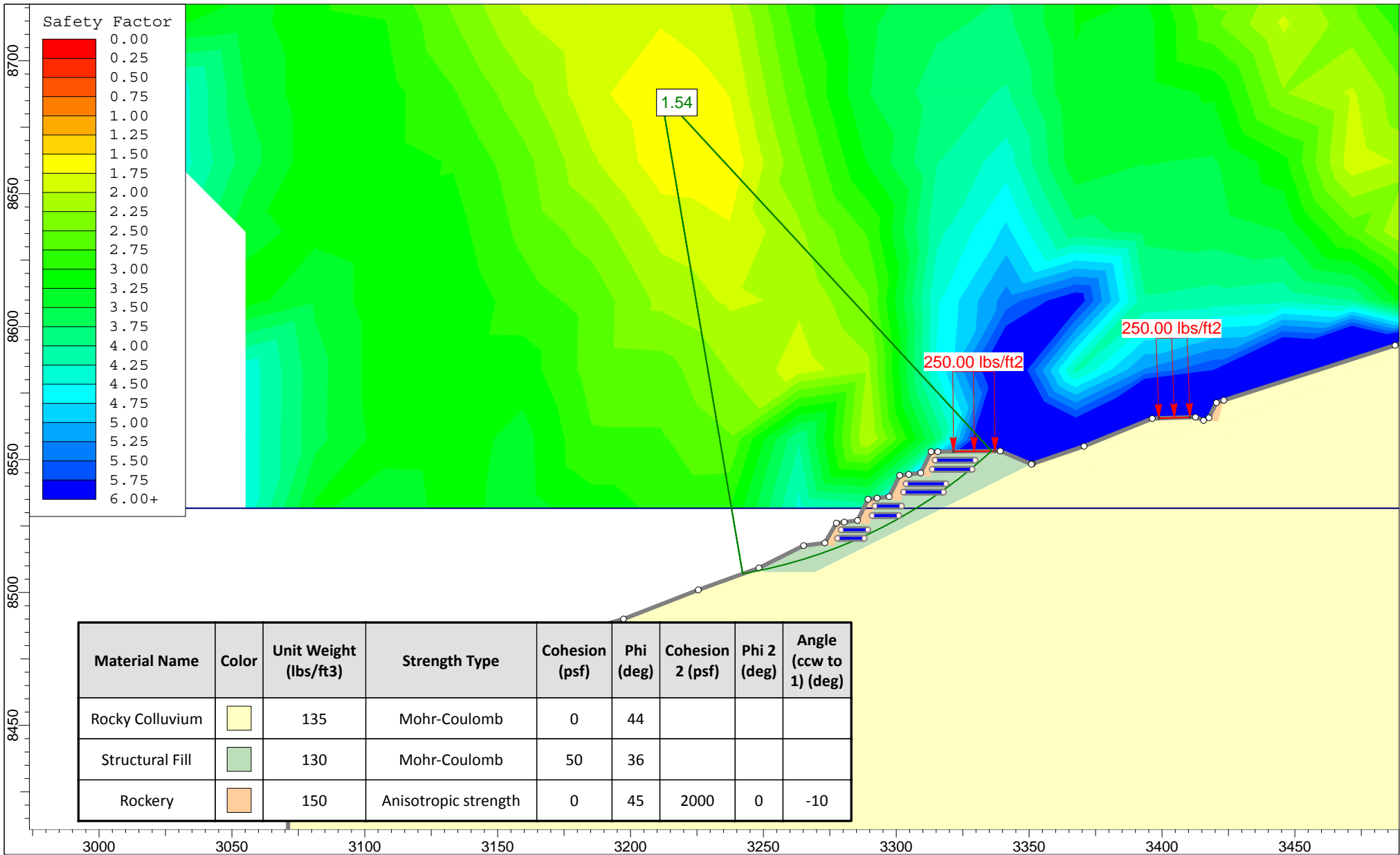
| X       | Y       |
|---------|---------|
| 431.088 | 8659.22 |
| 430.638 | 8658.33 |
| 435.618 | 8657.88 |
| 438.615 | 8667.79 |


### Material Boundary

| X       | Y       |
|---------|---------|
| 443.306 | 8668.45 |
| 442.856 | 8667.56 |
| 446.832 | 8667.12 |
| 449.973 | 8676.65 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 479.175 | 8673.61 |
| 480.052 | 8676.19 |



|  |   |                                 |                              |
|--|---|---------------------------------|------------------------------|
|  | <i>Project</i><br><b>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G</b>                   |                                 |                              |
|  | <i>Analysis Description</i><br><b>GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 5-5'</b> |                                 |                              |
|  | <i>Drawn By</i><br>SL   | <i>Scale</i><br>1:600           | <i>Company</i><br>IGES, INC. |
|  | <i>Date</i><br>9-25-2015  | <i>File Name</i><br>Static.slim |                              |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

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File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

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Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

3 Distributed Loads present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 3

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |




## Support Properties

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

#### Pullout Strength Dependency:

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

## Global Minimums

### Method: spencer

FS: 1.540910  
 Center: 3211.376, 8687.759  
 Radius: 183.369  
 Left Slip Surface Endpoint: 3242.235, 8507.005  
 Right Slip Surface Endpoint: 3335.925, 8553.179  
 Resisting Moment=1.42561e+007 lb-ft  
 Driving Moment=9.25172e+006 lb-ft  
 Resisting Horizontal Force=68865.5 lb  
 Driving Horizontal Force=44691.3 lb  
 Total Slice Area=756.574 ft<sup>2</sup>

## Valid / Invalid Surfaces

### Method: spencer

Number of Valid Surfaces: 4252  
 Number of Invalid Surfaces: 599

#### Error Codes:

Error Code -102 reported for 13 surfaces  
 Error Code -103 reported for 9 surfaces  
 Error Code -106 reported for 51 surfaces  
 Error Code -107 reported for 3 surfaces

Error Code -108 reported for 29 surfaces  
 Error Code -111 reported for 58 surfaces  
 Error Code -112 reported for 128 surfaces  
 Error Code -1000 reported for 308 surfaces

**Error Codes**

The following errors were encountered during the computation:

- 102 = Two surface / slope intersections, but resulting arc is actually outside soil region.
- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

**Slice Data**

Global Minimum Query (spencer) - Safety Factor: 1.54091

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 3.66338    | 162.915      | Rocky Colluvium | 0                   | 44                            | 32.1208            | 49.4953              | 51.2538                  | 0                   | 51.2538                       |
| 2            | 3.66338    | 479.046      | Rocky Colluvium | 0                   | 44                            | 91.9223            | 141.644              | 146.677                  | 0                   | 146.677                       |
| 3            | 3.75493    | 940.371      | Structural Fill | 50                  | 36                            | 160.209            | 246.867              | 270.963                  | 0                   | 270.963                       |
| 4            | 3.75493    | 1426.09      | Structural Fill | 50                  | 36                            | 218.681            | 336.967              | 394.976                  | 0                   | 394.976                       |
| 5            | 3.75493    | 1870.81      | Structural Fill | 50                  | 36                            | 269.313            | 414.987              | 502.362                  | 0                   | 502.362                       |
| 6            | 3.75493    | 2273.84      | Structural Fill | 50                  | 36                            | 312.474            | 481.494              | 593.902                  | 0                   | 593.902                       |
| 7            | 3.75493    | 2388.23      | Structural Fill | 50                  | 36                            | 319.312            | 492.031              | 608.402                  | 0                   | 608.402                       |
| 8            | 3.75493    | 2026.31      | Structural Fill | 50                  | 36                            | 270.496            | 416.81               | 504.872                  | 0                   | 504.872                       |
| 9            | 3.75493    | 2553.07      | Structural Fill | 50                  | 36                            | 324.349            | 499.793              | 619.086                  | 0                   | 619.086                       |
| 10           | 3.75493    | 4668.74      | Structural Fill | 50                  | 36                            | 551.322            | 849.537              | 1100.47                  | 0                   | 1100.47                       |
| 11           | 3.75493    | 4049.08      | Structural Fill | 50                  | 36                            | 472.07             | 727.418              | 932.384                  | 0                   | 932.384                       |
| 12           | 3.75493    | 3915.15      | Structural Fill | 50                  | 36                            | 522.81             | 805.603              | 1040                     | 0                   | 1040                          |
| 13           | 3.75493    | 6452.92      | Structural Fill | 50                  | 36                            | 699.003            | 1077.1               | 1413.68                  | 0                   | 1413.68                       |
| 14           | 3.75493    | 6001.29      | Structural Fill | 50                  | 36                            | 637.515            | 982.353              | 1283.28                  | 0                   | 1283.28                       |
| 15           | 3.75493    | 5343.56      | Structural Fill | 50                  | 36                            | 558.158            | 860.071              | 1114.97                  | 0                   | 1114.97                       |
| 16           | 3.75493    | 7530.97      | Structural Fill | 50                  | 36                            | 754.976            | 1163.35              | 1532.4                   | 0                   | 1532.4                        |

|    |         |         |                 |    |    |         |         |         |   |         |
|----|---------|---------|-----------------|----|----|---------|---------|---------|---|---------|
| 17 | 3.75493 | 7464.15 | Structural Fill | 50 | 36 | 730.782 | 1126.07 | 1481.09 | 0 | 1481.09 |
| 18 | 3.75493 | 6398.91 | Structural Fill | 50 | 36 | 615.951 | 949.125 | 1237.54 | 0 | 1237.54 |
| 19 | 3.75493 | 7968.76 | Structural Fill | 50 | 36 | 740.621 | 1141.23 | 1501.95 | 0 | 1501.95 |
| 20 | 3.75493 | 8121.2  | Structural Fill | 50 | 36 | 796.594 | 1227.48 | 1620.66 | 0 | 1620.66 |
| 21 | 3.75493 | 6680.62 | Structural Fill | 50 | 36 | 594.971 | 916.796 | 1193.04 | 0 | 1193.04 |
| 22 | 3.75493 | 5332.05 | Structural Fill | 50 | 36 | 532.832 | 821.046 | 1061.26 | 0 | 1061.26 |
| 23 | 3.75493 | 3908.45 | Structural Fill | 50 | 36 | 441.546 | 680.383 | 867.648 | 0 | 867.648 |
| 24 | 3.75493 | 2405.06 | Structural Fill | 50 | 36 | 289.865 | 446.656 | 545.951 | 0 | 545.951 |
| 25 | 3.75493 | 816.388 | Structural Fill | 50 | 36 | 163.952 | 252.636 | 278.905 | 0 | 278.905 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.54091

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 3242.23           | 8507.01                    | 0                             | 0                            | 0                                |
| 2            | 3245.9            | 8507.67                    | 83.6564                       | 48.0076                      | 29.8501                          |
| 3            | 3249.56           | 8508.41                    | 311.728                       | 178.891                      | 29.8502                          |
| 4            | 3253.32           | 8509.25                    | 685.52                        | 393.398                      | 29.8501                          |
| 5            | 3257.07           | 8510.17                    | 1141.7                        | 655.182                      | 29.85                            |
| 6            | 3260.83           | 8511.18                    | 1646.23                       | 944.72                       | 29.8502                          |
| 7            | 3264.58           | 8512.28                    | 2169.36                       | 1244.92                      | 29.85                            |
| 8            | 3268.34           | 8513.46                    | 2648.89                       | 1520.11                      | 29.8501                          |
| 9            | 3272.09           | 8514.73                    | 3022.34                       | 1734.42                      | 29.8501                          |
| 10           | 3275.85           | 8516.1                     | 3396.05                       | 1948.88                      | 29.8501                          |
| 11           | 3279.6            | 8517.55                    | 3862.43                       | 2216.52                      | 29.8501                          |
| 12           | 3283.36           | 8519.11                    | 4186.53                       | 2402.51                      | 29.8501                          |
| 13           | 3287.11           | 8520.76                    | 5675.87                       | 3257.2                       | 29.8501                          |
| 14           | 3290.87           | 8522.52                    | 5820.67                       | 3340.29                      | 29.8501                          |
| 15           | 3294.62           | 8524.37                    | 5828.49                       | 3344.78                      | 29.8501                          |
| 16           | 3298.38           | 8526.34                    | 5730.03                       | 3288.27                      | 29.8501                          |
| 17           | 3302.13           | 8528.42                    | 5376.29                       | 3085.28                      | 29.8501                          |
| 18           | 3305.89           | 8530.62                    | 4864.84                       | 2791.77                      | 29.8501                          |
| 19           | 3309.64           | 8532.94                    | 4306.25                       | 2471.22                      | 29.8501                          |
| 20           | 3313.4            | 8535.39                    | 3410.32                       | 1957.07                      | 29.8501                          |
| 21           | 3317.15           | 8537.97                    | 3461.34                       | 1986.35                      | 29.8501                          |
| 22           | 3320.91           | 8540.7                     | 2446.37                       | 1403.89                      | 29.8501                          |
| 23           | 3324.66           | 8543.57                    | 1405.99                       | 806.851                      | 29.8501                          |
| 24           | 3328.42           | 8546.6                     | 969.892                       | 556.589                      | 29.8501                          |
| 25           | 3332.17           | 8549.8                     | 320.434                       | 183.886                      | 29.85                            |
| 26           | 3335.92           | 8553.18                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 3337.17 | 8553.19 |
| 3321.56 | 8553.04 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 3557.63 | 8619.65 |
| 3538.26 | 8619.23 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 3410.51 | 8565.9  |
| 3398.86 | 8565.51 |

### External Boundary

| X       | Y       |
|---------|---------|
| 3248.35 | 8509.21 |
| 3225.52 | 8500.97 |
| 3197.41 | 8490    |
| 3176.59 | 8484.11 |
| 3126.28 | 8468.24 |
| 3114.23 | 8465.04 |
| 3108.16 | 8463.75 |
| 3103.82 | 8462.48 |
| 3094.3  | 8459.55 |
| 3071.13 | 8454.48 |
| 3071.13 | 8090.89 |
| 3771.89 | 8090.89 |
| 3771.89 | 8682.15 |
| 3734.92 | 8670.21 |
| 3693.28 | 8658.77 |
| 3670.74 | 8650    |
| 3654.61 | 8644.82 |
| 3616.95 | 8632.84 |
| 3595.91 | 8625.14 |
| 3584.79 | 8621.79 |
| 3566.98 | 8616.54 |
| 3560.21 | 8619.71 |
| 3525.76 | 8618.95 |
| 3522.45 | 8618.88 |
| 3518.44 | 8610.88 |
| 3513.83 | 8610.29 |

|         |         |
|---------|---------|
| 3510.42 | 8609.86 |
| 3506.41 | 8601.86 |
| 3501.48 | 8601.23 |
| 3498.39 | 8600.85 |
| 3495.61 | 8595.49 |
| 3487.73 | 8592.96 |
| 3423.33 | 8572.29 |
| 3420.47 | 8571.38 |
| 3417.68 | 8565.72 |
| 3415.64 | 8564.72 |
| 3412.59 | 8565.97 |
| 3396.37 | 8565.43 |
| 3370.67 | 8555    |
| 3351.24 | 8548.4  |
| 3350.88 | 8548.28 |
| 3339.16 | 8553.21 |
| 3315.66 | 8552.99 |
| 3313.16 | 8552.96 |
| 3309.21 | 8544.99 |
| 3304.72 | 8544.44 |
| 3301.3  | 8544.03 |
| 3297.34 | 8536.04 |
| 3292.82 | 8535.49 |
| 3289.41 | 8535.07 |
| 3285.44 | 8527.08 |
| 3280.48 | 8526.47 |
| 3277.49 | 8526.1  |
| 3273.16 | 8518.62 |
| 3265.16 | 8517.62 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3273.16 | 8518.62 |
| 3272.65 | 8517.76 |
| 3276.62 | 8517.24 |
| 3280.48 | 8526.47 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3285.44 | 8527.08 |
| 3284.99 | 8526.18 |
| 3289.96 | 8525.6  |
| 3292.82 | 8535.49 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3297.34 | 8536.04 |
| 3296.89 | 8535.15 |
| 3301.86 | 8534.57 |
| 3304.72 | 8544.44 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3309.21 | 8544.99 |
| 3308.75 | 8544.1  |
| 3312.73 | 8543.67 |
| 3315.66 | 8552.99 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3417.68 | 8565.72 |
| 3417.24 | 8564.83 |
| 3421.17 | 8564.12 |
| 3423.33 | 8572.29 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3495.61 | 8595.49 |
| 3495.16 | 8594.59 |
| 3499.14 | 8594.2  |
| 3501.48 | 8601.23 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3506.41 | 8601.86 |
| 3505.96 | 8600.96 |
| 3510.92 | 8600.32 |
| 3513.83 | 8610.29 |

### Material Boundary

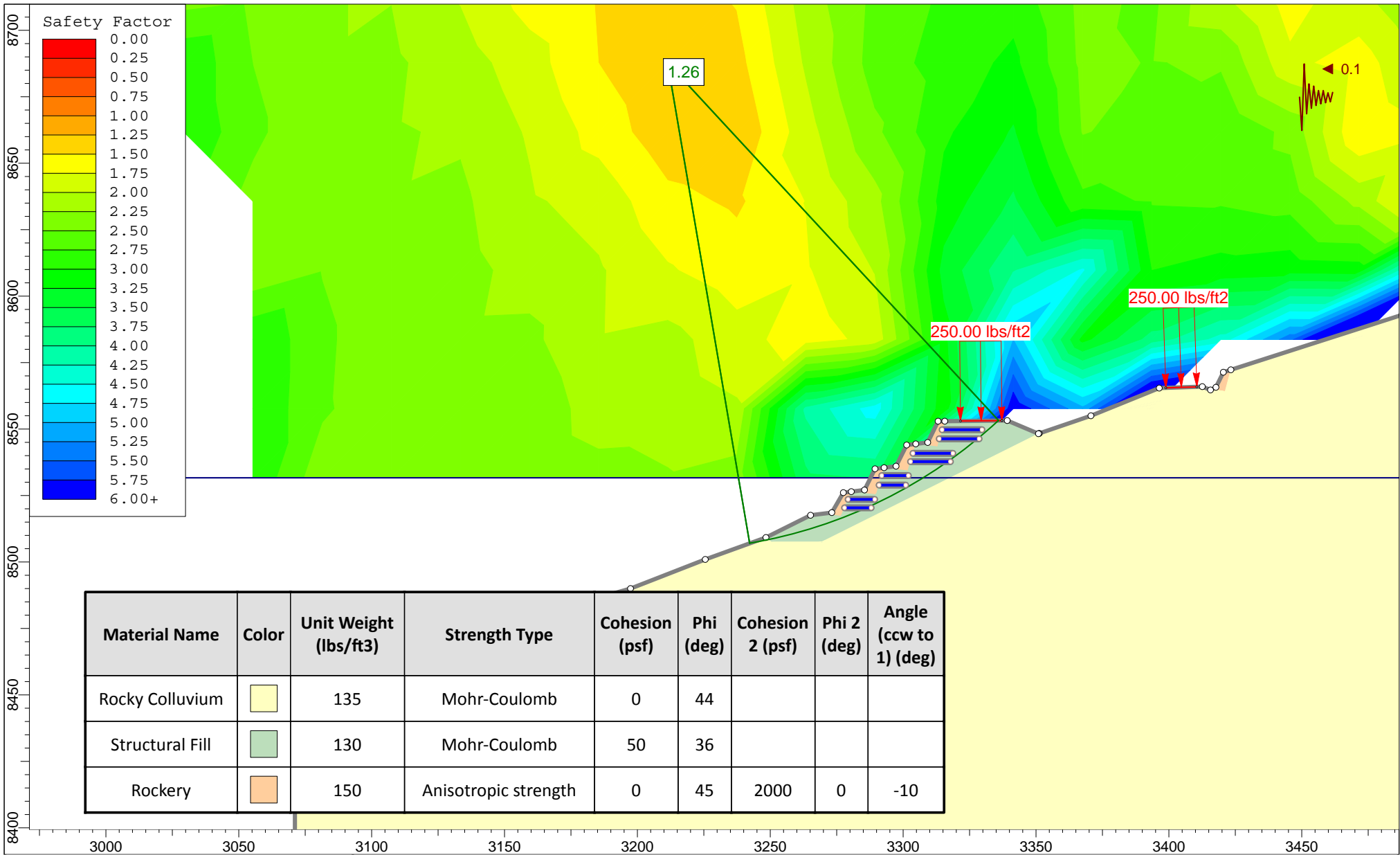
| X       | Y       |
|---------|---------|
| 3518.44 | 8610.88 |
| 3517.99 | 8609.98 |
| 3522.95 | 8609.34 |
| 3525.76 | 8618.95 |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 3248.35 | 8509.21 |
| 3250.85 | 8507.55 |
| 3269.41 | 8507.55 |
| 3351.24 | 8548.4  |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 3487.73 | 8592.96 |
| 3491.12 | 8589.59 |
| 3507.02 | 8589.59 |
| 3566.98 | 8616.54 |



|  |   |                                   |                              |
|--|---|-----------------------------------|------------------------------|
|  | <b>Project</b><br>ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G                    |                                   |                              |
|  | <b>Analysis Description</b><br>GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 5-5' |                                   |                              |
|  | <b>Drawn By</b><br>SL   | <b>Scale</b><br>1:600             | <b>Company</b><br>IGES, INC. |
|  | <b>Date</b><br>9-25-2015  | <b>File Name</b><br>P-Static.slim |                              |



## *Slide Analysis Information*

# *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 3 Distributed Loads present

### Distributed Load 1

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 3

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |

|          |   |   |   |
|----------|---|---|---|
| Ru Value | 0 | 0 | 0 |
|----------|---|---|---|


## Support Properties

---

### Mirafi 3XT

Support Type: GeoTextile  
 Force Application: Passive  
 Force Orientation: Parallel to Reinforcement  
 Anchorage: None  
 Shear Strength Model: Linear  
 Strip Coverage: 100 percent  
 Tensile Strength: 1918 lb/ft  
 Default Pullout Strength Adhesion: 5 psf  
 Default Pullout Strength Friction Angle: 40 degrees  
 and Material Dependent

#### Pullout Strength Dependency:

| Material   | Adhesion (psf) | Friction Angle (deg) |
|--|----------------|----------------------|
| <br>Structural Fill | 50             | 36                   |

## Global Minimums

---

### Method: spencer

FS: 1.261400  
 Center: 3211.376, 8687.759  
 Radius: 183.369  
 Left Slip Surface Endpoint: 3242.235, 8507.005  
 Right Slip Surface Endpoint: 3335.925, 8553.179  
 Resisting Moment=1.36359e+007 lb-ft  
 Driving Moment=1.08101e+007 lb-ft  
 Resisting Horizontal Force=66189.7 lb  
 Driving Horizontal Force=52473 lb  
 Total Slice Area=756.574 ft<sup>2</sup>

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 4113  
 Number of Invalid Surfaces: 738

#### Error Codes:

Error Code -102 reported for 13 surfaces  
 Error Code -103 reported for 9 surfaces  
 Error Code -106 reported for 51 surfaces

Error Code -107 reported for 1 surface  
 Error Code -108 reported for 49 surfaces  
 Error Code -111 reported for 142 surfaces  
 Error Code -112 reported for 165 surfaces  
 Error Code -1000 reported for 308 surfaces

### Error Codes

The following errors were encountered during the computation:

- 102 = Two surface / slope intersections, but resulting arc is actually outside soil region.
- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than  $0.0001 * (\text{maximum horizontal extent of soil region})$ . This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force  $< 0.1$ . This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

### Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.2614

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 3.66338    | 162.915      | Rocky Colluvium | 0                   | 44                            | 40.9819            | 51.6946              | 53.5312                  | 0                   | 53.5312                       |
| 2            | 3.66338    | 479.046      | Rocky Colluvium | 0                   | 44                            | 116.463            | 146.907              | 152.127                  | 0                   | 152.127                       |
| 3            | 3.75493    | 940.371      | Structural Fill | 50                  | 36                            | 199.875            | 252.122              | 278.196                  | 0                   | 278.196                       |
| 4            | 3.75493    | 1426.09      | Structural Fill | 50                  | 36                            | 269.947            | 340.511              | 399.855                  | 0                   | 399.855                       |
| 5            | 3.75493    | 1870.81      | Structural Fill | 50                  | 36                            | 329.784            | 415.989              | 503.74                   | 0                   | 503.74                        |
| 6            | 3.75493    | 2273.84      | Structural Fill | 50                  | 36                            | 380.002            | 479.334              | 590.928                  | 0                   | 590.928                       |
| 7            | 3.75493    | 2388.23      | Structural Fill | 50                  | 36                            | 386.226            | 487.186              | 601.734                  | 0                   | 601.734                       |
| 8            | 3.75493    | 2026.31      | Structural Fill | 50                  | 36                            | 326.13             | 411.38               | 497.396                  | 0                   | 497.396                       |
| 9            | 3.75493    | 2553.07      | Structural Fill | 50                  | 36                            | 388.3              | 489.801              | 605.333                  | 0                   | 605.333                       |
| 10           | 3.75493    | 4668.74      | Structural Fill | 50                  | 36                            | 653.908            | 824.84               | 1066.47                  | 0                   | 1066.47                       |
| 11           | 3.75493    | 4049.08      | Structural Fill | 50                  | 36                            | 557.73             | 703.52               | 899.493                  | 0                   | 899.493                       |
| 12           | 3.75493    | 3915.15      | Structural Fill | 50                  | 36                            | 658.831            | 831.05               | 1075.02                  | 0                   | 1075.02                       |
| 13           | 3.75493    | 6452.92      | Structural Fill | 50                  | 36                            | 815.868            | 1029.14              | 1347.67                  | 0                   | 1347.67                       |
| 14           | 3.75493    | 6001.29      | Structural Fill | 50                  | 36                            | 740.895            | 934.565              | 1217.5                   | 0                   | 1217.5                        |
| 15           | 3.75493    | 5343.56      | Structural Fill | 50                  | 36                            | 646.105            | 814.997              | 1052.93                  | 0                   | 1052.93                       |
| 16           | 3.75493    | 7530.97      | Structural Fill | 50                  | 36                            | 868.361            | 1095.35              | 1438.8                   | 0                   | 1438.8                        |

|    |         |         |                 |    |    |         |         |         |   |         |
|----|---------|---------|-----------------|----|----|---------|---------|---------|---|---------|
| 17 | 3.75493 | 7464.15 | Structural Fill | 50 | 36 | 836.737 | 1055.46 | 1383.9  | 0 | 1383.9  |
| 18 | 3.75493 | 6398.91 | Structural Fill | 50 | 36 | 702.643 | 886.314 | 1151.09 | 0 | 1151.09 |
| 19 | 3.75493 | 7968.76 | Structural Fill | 50 | 36 | 840.122 | 1059.73 | 1389.78 | 0 | 1389.78 |
| 20 | 3.75493 | 8121.2  | Structural Fill | 50 | 36 | 935.27  | 1179.75 | 1554.97 | 0 | 1554.97 |
| 21 | 3.75493 | 6680.62 | Structural Fill | 50 | 36 | 669.596 | 844.628 | 1093.71 | 0 | 1093.71 |
| 22 | 3.75493 | 5332.05 | Structural Fill | 50 | 36 | 602.492 | 759.983 | 977.208 | 0 | 977.208 |
| 23 | 3.75493 | 3908.45 | Structural Fill | 50 | 36 | 513.319 | 647.5   | 822.388 | 0 | 822.388 |
| 24 | 3.75493 | 2405.06 | Structural Fill | 50 | 36 | 329.719 | 415.907 | 503.628 | 0 | 503.628 |
| 25 | 3.75493 | 816.388 | Structural Fill | 50 | 36 | 187.76  | 236.84  | 257.164 | 0 | 257.164 |

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.2614

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 3242.23           | 8507.01                    | 0                             | 0                            | 0                                |
| 2            | 3245.9            | 8507.67                    | 98.5284                       | 65.3113                      | 33.5391                          |
| 3            | 3249.56           | 8508.41                    | 365.168                       | 242.058                      | 33.5391                          |
| 4            | 3253.32           | 8509.25                    | 788.852                       | 522.904                      | 33.5391                          |
| 5            | 3257.07           | 8510.17                    | 1291.85                       | 856.327                      | 33.5392                          |
| 6            | 3260.83           | 8511.18                    | 1836.74                       | 1217.52                      | 33.5392                          |
| 7            | 3264.58           | 8512.28                    | 2391.32                       | 1585.13                      | 33.5391                          |
| 8            | 3268.34           | 8513.46                    | 2893.24                       | 1917.83                      | 33.539                           |
| 9            | 3272.09           | 8514.73                    | 3284.21                       | 2176.99                      | 33.539                           |
| 10           | 3275.85           | 8516.1                     | 3663.56                       | 2428.45                      | 33.5391                          |
| 11           | 3279.6            | 8517.55                    | 4101.31                       | 2718.62                      | 33.5391                          |
| 12           | 3283.36           | 8519.11                    | 4396.21                       | 2914.1                       | 33.5391                          |
| 13           | 3287.11           | 8520.76                    | 6226.25                       | 4127.17                      | 33.539                           |
| 14           | 3290.87           | 8522.52                    | 6284.74                       | 4165.95                      | 33.5391                          |
| 15           | 3294.62           | 8524.37                    | 6206.86                       | 4114.32                      | 33.5391                          |
| 16           | 3298.38           | 8526.34                    | 6029.82                       | 3996.97                      | 33.5391                          |
| 17           | 3302.13           | 8528.42                    | 5548.13                       | 3677.67                      | 33.5391                          |
| 18           | 3305.89           | 8530.62                    | 4906.2                        | 3252.15                      | 33.539                           |
| 19           | 3309.64           | 8532.94                    | 4237.58                       | 2808.95                      | 33.5391                          |
| 20           | 3313.4            | 8535.39                    | 3197.49                       | 2119.51                      | 33.5391                          |
| 21           | 3317.15           | 8537.97                    | 3407.55                       | 2258.75                      | 33.5391                          |
| 22           | 3320.91           | 8540.7                     | 2278.81                       | 1510.55                      | 33.5391                          |
| 23           | 3324.66           | 8543.57                    | 1211.43                       | 803.016                      | 33.5391                          |
| 24           | 3328.42           | 8546.6                     | 910.605                       | 603.61                       | 33.5391                          |
| 25           | 3332.17           | 8549.8                     | 307.454                       | 203.801                      | 33.5391                          |
| 26           | 3335.92           | 8553.18                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 3337.17 | 8553.19 |
| 3321.56 | 8553.04 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 3557.63 | 8619.65 |
| 3538.26 | 8619.23 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 3410.51 | 8565.9  |
| 3398.86 | 8565.51 |

### External Boundary

| X       | Y       |
|---------|---------|
| 3248.35 | 8509.21 |
| 3225.52 | 8500.97 |
| 3197.41 | 8490    |
| 3176.59 | 8484.11 |
| 3126.28 | 8468.24 |
| 3114.23 | 8465.04 |
| 3108.16 | 8463.75 |
| 3103.82 | 8462.48 |
| 3094.3  | 8459.55 |
| 3071.13 | 8454.48 |
| 3071.13 | 8090.89 |
| 3771.89 | 8090.89 |
| 3771.89 | 8682.15 |
| 3734.92 | 8670.21 |
| 3693.28 | 8658.77 |
| 3670.74 | 8650    |
| 3654.61 | 8644.82 |
| 3616.95 | 8632.84 |
| 3595.91 | 8625.14 |
| 3584.79 | 8621.79 |
| 3566.98 | 8616.54 |
| 3560.21 | 8619.71 |
| 3525.76 | 8618.95 |
| 3522.45 | 8618.88 |
| 3518.44 | 8610.88 |
| 3513.83 | 8610.29 |

|         |         |
|---------|---------|
| 3510.42 | 8609.86 |
| 3506.41 | 8601.86 |
| 3501.48 | 8601.23 |
| 3498.39 | 8600.85 |
| 3495.61 | 8595.49 |
| 3487.73 | 8592.96 |
| 3423.33 | 8572.29 |
| 3420.47 | 8571.38 |
| 3417.68 | 8565.72 |
| 3415.64 | 8564.72 |
| 3412.59 | 8565.97 |
| 3396.37 | 8565.43 |
| 3370.67 | 8555    |
| 3351.24 | 8548.4  |
| 3350.88 | 8548.28 |
| 3339.16 | 8553.21 |
| 3315.66 | 8552.99 |
| 3313.16 | 8552.96 |
| 3309.21 | 8544.99 |
| 3304.72 | 8544.44 |
| 3301.3  | 8544.03 |
| 3297.34 | 8536.04 |
| 3292.82 | 8535.49 |
| 3289.41 | 8535.07 |
| 3285.44 | 8527.08 |
| 3280.48 | 8526.47 |
| 3277.49 | 8526.1  |
| 3273.16 | 8518.62 |
| 3265.16 | 8517.62 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3273.16 | 8518.62 |
| 3272.65 | 8517.76 |
| 3276.62 | 8517.24 |
| 3280.48 | 8526.47 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3285.44 | 8527.08 |
| 3284.99 | 8526.18 |
| 3289.96 | 8525.6  |
| 3292.82 | 8535.49 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3297.34 | 8536.04 |
| 3296.89 | 8535.15 |
| 3301.86 | 8534.57 |
| 3304.72 | 8544.44 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3309.21 | 8544.99 |
| 3308.75 | 8544.1  |
| 3312.73 | 8543.67 |
| 3315.66 | 8552.99 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3417.68 | 8565.72 |
| 3417.24 | 8564.83 |
| 3421.17 | 8564.12 |
| 3423.33 | 8572.29 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3495.61 | 8595.49 |
| 3495.16 | 8594.59 |
| 3499.14 | 8594.2  |
| 3501.48 | 8601.23 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3506.41 | 8601.86 |
| 3505.96 | 8600.96 |
| 3510.92 | 8600.32 |
| 3513.83 | 8610.29 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 3518.44 | 8610.88 |
| 3517.99 | 8609.98 |
| 3522.95 | 8609.34 |
| 3525.76 | 8618.95 |

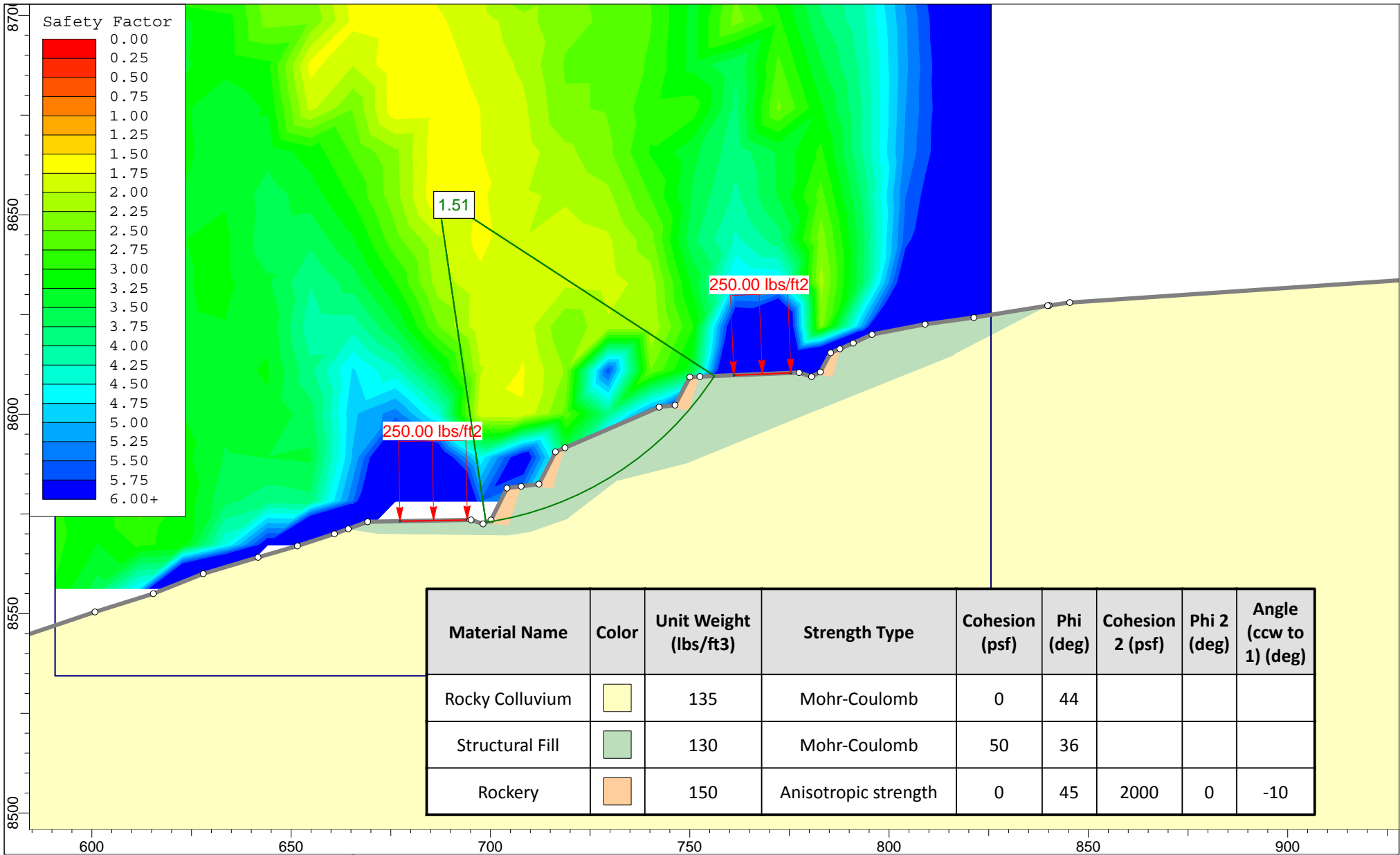





**Material Boundary**


| X       | Y       |
|---------|---------|
| 3248.35 | 8509.21 |
| 3250.85 | 8507.55 |
| 3269.41 | 8507.55 |
| 3351.24 | 8548.4  |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 3487.73 | 8592.96 |
| 3491.12 | 8589.59 |
| 3507.02 | 8589.59 |
| 3566.98 | 8616.54 |



| Material Name   | Color   | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|---|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |  | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |  | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |  | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |

|  |                      |           |       |   |             |            |
|--|----------------------|-----------|-------|---|-------------|------------|
|  | Project              |           |       | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G      |             |            |
|  | Analysis Description |           |       | GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 6-6' |             |            |
|  | Drawn By             | SL        | Scale | 1:400   | Company     | IGES, INC. |
|  | Date                 | 9-25-2015 |       | File Name   | Static.slim |            |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m\alpha < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Global Minimums

---

Method: spencer

FS: 1.507160  
 Center: 686.824, 8654.806  
 Radius: 82.828  
 Left Slip Surface Endpoint: 698.866, 8572.857  
 Right Slip Surface Endpoint: 756.228, 8609.599  
 Resisting Moment=4.07178e+006 lb-ft  
 Driving Moment=2.70162e+006 lb-ft  
 Resisting Horizontal Force=42382.2 lb  
 Driving Horizontal Force=28120.6 lb  
 Total Slice Area=502.741 ft<sup>2</sup>

## Valid / Invalid Surfaces

### Method: spencer

Number of Valid Surfaces: 3227  
 Number of Invalid Surfaces: 1580

#### Error Codes:

Error Code -103 reported for 771 surfaces  
 Error Code -106 reported for 6 surfaces  
 Error Code -107 reported for 3 surfaces  
 Error Code -108 reported for 34 surfaces  
 Error Code -111 reported for 128 surfaces  
 Error Code -112 reported for 638 surfaces

#### Error Codes

The following errors were encountered during the computation:

- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than  $0.0001 * (\text{maximum horizontal extent of soil region})$ . This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force  $< 0.1$ . This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.

## Slice Data

Global Minimum Query (spencer) - Safety Factor: 1.50716

| Slice Number | Width [ft] | Weight [lbs] | Base Material | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|---------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
|--------------|------------|--------------|---------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|

|    |          |         |                 |         |         |         |         |         |   |         |
|----|----------|---------|-----------------|---------|---------|---------|---------|---------|---|---------|
| 1  | 1.03808  | 24.0974 | Structural Fill | 50      | 36      | 53.0378 | 79.9364 | 41.204  | 0 | 41.204  |
| 2  | 2.69095  | 993.414 | Rockery         | 234.651 | 39.7204 | 421.274 | 634.927 | 481.787 | 0 | 481.787 |
| 3  | 2.69095  | 2762.58 | Rockery         | 278.905 | 38.7247 | 807.971 | 1217.74 | 1170.82 | 0 | 1170.82 |
| 4  | 2.46687  | 2559.6  | Structural Fill | 50      | 36      | 547.069 | 824.521 | 1066.04 | 0 | 1066.04 |
| 5  | 2.46687  | 2268.33 | Structural Fill | 50      | 36      | 473.402 | 713.492 | 913.217 | 0 | 913.217 |
| 6  | 2.46687  | 2185.43 | Structural Fill | 50      | 36      | 442.797 | 667.366 | 849.731 | 0 | 849.731 |
| 7  | 2.46687  | 3225.6  | Structural Fill | 50      | 36      | 615.254 | 927.286 | 1207.48 | 0 | 1207.48 |
| 8  | 2.46687  | 4400.54 | Structural Fill | 50      | 36      | 798.999 | 1204.22 | 1588.66 | 0 | 1588.66 |
| 9  | 2.46687  | 4278.91 | Structural Fill | 50      | 36      | 752.302 | 1133.84 | 1491.77 | 0 | 1491.77 |
| 10 | 2.46687  | 4238.4  | Structural Fill | 50      | 36      | 720.793 | 1086.35 | 1426.4  | 0 | 1426.4  |
| 11 | 2.46687  | 4201.06 | Structural Fill | 50      | 36      | 690.797 | 1041.14 | 1364.19 | 0 | 1364.19 |
| 12 | 2.46687  | 4130.8  | Structural Fill | 50      | 36      | 656.729 | 989.796 | 1293.52 | 0 | 1293.52 |
| 13 | 2.46687  | 4025.84 | Structural Fill | 50      | 36      | 618.77  | 932.586 | 1214.77 | 0 | 1214.77 |
| 14 | 2.46687  | 3884.09 | Structural Fill | 50      | 36      | 577.085 | 869.76  | 1128.3  | 0 | 1128.3  |
| 15 | 2.46687  | 3703.13 | Structural Fill | 50      | 36      | 531.827 | 801.548 | 1034.42 | 0 | 1034.42 |
| 16 | 2.46687  | 3480.06 | Structural Fill | 50      | 36      | 483.134 | 728.16  | 933.408 | 0 | 933.408 |
| 17 | 2.46687  | 3211.45 | Structural Fill | 50      | 36      | 431.138 | 649.794 | 825.544 | 0 | 825.544 |
| 18 | 2.46687  | 2893.12 | Structural Fill | 50      | 36      | 375.961 | 566.633 | 711.084 | 0 | 711.084 |
| 19 | 2.46687  | 2399.2  | Structural Fill | 50      | 36      | 303.906 | 458.035 | 561.613 | 0 | 561.613 |
| 20 | 2.46687  | 1861.37 | Structural Fill | 50      | 36      | 232.046 | 349.731 | 412.545 | 0 | 412.545 |
| 21 | 2.46687  | 2464.48 | Structural Fill | 50      | 36      | 284.197 | 428.33  | 520.726 | 0 | 520.726 |
| 22 | 0.166705 | 197.122 | Rockery         | 1483.69 | 11.6171 | 1016.07 | 1531.38 | 231.973 | 0 | 231.973 |
| 23 | 2.12406  | 2143.88 | Structural Fill | 50      | 36      | 272.724 | 411.039 | 496.926 | 0 | 496.926 |
| 24 | 2.12406  | 1220.95 | Structural Fill | 50      | 36      | 159.67  | 240.648 | 262.405 | 0 | 262.405 |
| 25 | 2.12406  | 416.709 | Structural Fill | 50      | 36      | 68.4197 | 103.12  | 73.1128 | 0 | 73.1128 |

## Interslice Data

**Global Minimum Query (spencer) - Safety Factor: 1.50716**

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 698.866           | 8572.86                    | 0                             | 0                            | 0                                |
| 2            | 699.904           | 8573.02                    | 48.4624                       | 27.6355                      | 29.6938                          |
| 3            | 702.595           | 8573.49                    | 952.093                       | 542.928                      | 29.6938                          |
| 4            | 705.286           | 8574.06                    | 2459.49                       | 1402.51                      | 29.6937                          |
| 5            | 707.753           | 8574.66                    | 3164.38                       | 1804.48                      | 29.6938                          |
| 6            | 710.219           | 8575.35                    | 3705.85                       | 2113.25                      | 29.6938                          |
| 7            | 712.686           | 8576.12                    | 4144.62                       | 2363.46                      | 29.6939                          |
| 8            | 715.153           | 8576.97                    | 4630.18                       | 2640.34                      | 29.6938                          |
| 9            | 717.62            | 8577.92                    | 5102.46                       | 2909.66                      | 29.6938                          |
| 10           | 720.087           | 8578.95                    | 5413.87                       | 3087.24                      | 29.6938                          |
| 11           | 722.554           | 8580.08                    | 5578.71                       | 3181.24                      | 29.6938                          |
| 12           | 725.021           | 8581.31                    | 5603.36                       | 3195.29                      | 29.6937                          |
| 13           | 727.487           | 8582.65                    | 5494.84                       | 3133.41                      | 29.6938                          |
| 14           | 729.954           | 8584.09                    | 5262.82                       | 3001.11                      | 29.6938                          |
| 15           | 732.421           | 8585.66                    | 4919.81                       | 2805.5                       | 29.6938                          |
| 16           | 734.888           | 8587.35                    | 4481.39                       | 2555.5                       | 29.6938                          |
| 17           | 737.355           | 8589.18                    | 3966.67                       | 2261.98                      | 29.6938                          |
| 18           | 739.822           | 8591.15                    | 3398.78                       | 1938.14                      | 29.6938                          |
| 19           | 742.289           | 8593.29                    | 2805.66                       | 1599.92                      | 29.6938                          |
| 20           | 744.756           | 8595.61                    | 2253.48                       | 1285.04                      | 29.6938                          |
| 21           | 747.222           | 8598.13                    | 1786.35                       | 1018.66                      | 29.6938                          |
| 22           | 749.689           | 8600.87                    | 1055.5                        | 601.896                      | 29.6938                          |
| 23           | 749.856           | 8601.07                    | 1179.57                       | 672.643                      | 29.6937                          |
| 24           | 751.98            | 8603.67                    | 468.371                       | 267.087                      | 29.6938                          |
| 25           | 754.104           | 8606.49                    | 65.0888                       | 37.1167                      | 29.6938                          |
| 26           | 756.228           | 8609.6                     | 0                             | 0                            | 0                                |

### List Of Coordinates

#### Distributed Load

| X       | Y       |
|---------|---------|
| 694.18  | 8573.48 |
| 677.313 | 8573.18 |

#### Distributed Load

| X       | Y       |
|---------|---------|
| 775.378 | 8610.38 |
| 761.042 | 8609.79 |

**External Boundary**

| X       | Y       |
|---------|---------|
| 712.158 | 8582.47 |
| 707.692 | 8581.92 |
| 704.147 | 8581.48 |
| 700.142 | 8573.49 |
| 698.139 | 8572.5  |
| 695.135 | 8573.5  |
| 669.186 | 8573.04 |
| 664.324 | 8571.26 |
| 660.858 | 8570    |
| 651.579 | 8566.97 |
| 641.697 | 8564.12 |
| 627.949 | 8560    |
| 615.417 | 8555    |
| 600.766 | 8550.43 |
| 576.666 | 8542.29 |
| 576.666 | 8484.11 |
| 933.571 | 8484.11 |
| 933.826 | 8633.99 |
| 845.33  | 8628.01 |
| 840.152 | 8627.29 |
| 839.773 | 8627.23 |
| 821.282 | 8624.26 |
| 809.037 | 8622.55 |
| 795.725 | 8620    |
| 791.035 | 8617.83 |
| 787.674 | 8616.39 |
| 785.358 | 8615.39 |
| 782.743 | 8610.58 |
| 780.553 | 8609.43 |
| 777.452 | 8610.46 |
| 752.516 | 8609.45 |
| 750.033 | 8609.35 |
| 746.292 | 8602.28 |
| 742.292 | 8601.78 |
| 718.697 | 8591.6  |
| 716.295 | 8590.56 |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 746.292 | 8602.28 |
| 745.825 | 8601.39 |
| 749.79  | 8600.86 |
| 752.516 | 8609.45 |



**Material Boundary**

| X       | Y       |
|---------|---------|
| 700.142 | 8573.49 |
| 699.694 | 8572.6  |
| 704.661 | 8572.02 |
| 707.692 | 8581.92 |

**Material Boundary**

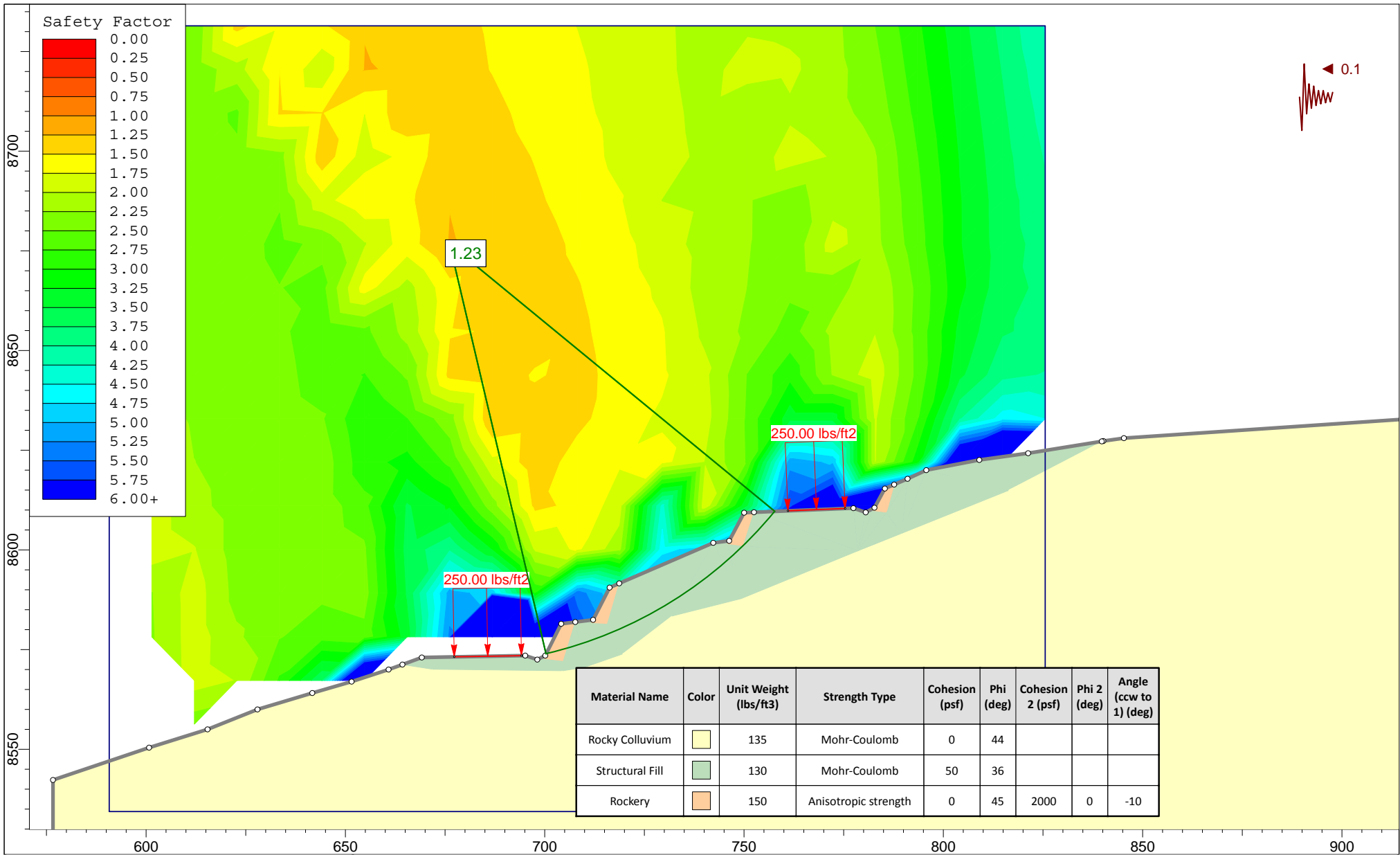
| X       | Y       |
|---------|---------|
| 712.158 | 8582.47 |
| 711.7   | 8581.58 |
| 715.694 | 8581.35 |
| 718.697 | 8591.6  |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 782.743 | 8610.58 |
| 782.247 | 8609.72 |
| 785.719 | 8609.28 |
| 787.674 | 8616.39 |

**Material Boundary**

| X       | Y       |
|---------|---------|
| 664.324 | 8571.26 |
| 671.862 | 8570.09 |
| 704.542 | 8569.71 |
| 709.945 | 8570.55 |
| 719.592 | 8573.92 |
| 731.958 | 8583.42 |
| 749.265 | 8587.78 |
| 778.566 | 8599.76 |
| 789.567 | 8604.18 |
| 816.212 | 8614.87 |
| 839.773 | 8627.23 |



| Material Name   | Color | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) |
|-----------------|-------|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|
| Rocky Colluvium |       | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        |
| Structural Fill |       | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        |
| Rockery         |       | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    |



SLIDEINTERPRET 6.029

|                             |  |           |              |  |                  |                |               |            |
|-----------------------------|--|-----------|--------------|--|------------------|----------------|---------------|------------|
| <i>Project</i>              |  |           |              | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G       |                  |                |               |            |
| <i>Analysis Description</i> |  |           |              | GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 6-6' |                  |                |               |            |
| <i>Drawn By</i>             |  | SL        | <i>Scale</i> |  | 1:400            | <i>Company</i> |               | IGES, INC. |
| <i>Date</i>                 |  | 9-25-2015 |              |  | <i>File Name</i> |                | P-Static.slim |            |

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

---

File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

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Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property                           | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------------------|---|---|---|
| Color                              |  |  |  |
| Strength Type                      | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft <sup>3</sup> ] | 135   | 130   | 150   |
| Cohesion [psf]                     | 0   | 50  |   |
| Friction Angle [deg]               | 44  | 36  |   |
| Cohesion 1 [psf]                   |   |   | 0   |
| Cohesion 2 [psf]                   |   |   | 2000  |
| Friction Angle 1 [deg]             |   |   | 45  |
| Friction Angle 2 [deg]             |   |   | 0   |
| Angle from 1 [deg]                 |   |   | -10   |
| Water Surface                      | None  | None  | None  |
| Ru Value                           | 0   | 0   | 0   |

## Global Minimums

---

## Method: spencer

FS: 1.233410  
Center: 676.152, 8676.697  
Radius: 105.599  
Left Slip Surface Endpoint: 700.350, 8573.908  
Right Slip Surface Endpoint: 757.744, 8609.661  
Resisting Moment=4.40715e+006 lb-ft  
Driving Moment=3.57313e+006 lb-ft  
Resisting Horizontal Force=36234 lb  
Driving Horizontal Force=29377 lb  
Total Slice Area=441.684 ft2

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 3049  
Number of Invalid Surfaces: 1758

#### Error Codes:

Error Code -102 reported for 12 surfaces  
Error Code -103 reported for 417 surfaces  
Error Code -106 reported for 20 surfaces  
Error Code -107 reported for 1 surface  
Error Code -108 reported for 100 surfaces  
Error Code -111 reported for 188 surfaces  
Error Code -112 reported for 707 surfaces  
Error Code -113 reported for 181 surfaces  
Error Code -1000 reported for 132 surfaces

#### Error Codes

The following errors were encountered during the computation:

- 102 = Two surface / slope intersections, but resulting arc is actually outside soil region.
- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than  $0.0001 * (\text{maximum horizontal extent of soil region})$ . This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force  $< 0.1$ . This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 113 = Surface intersects outside slope limits.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

## Slice Data

**Global Minimum Query (spencer) - Safety Factor: 1.23341**

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.65834    | 925.582      | Rockery         | 330.628             | 37.5609                       | 575.855            | 710.265              | 493.665                  | 0                   | 493.665                       |
| 2            | 2.65834    | 2437.59      | Rockery         | 370.2               | 36.6705                       | 930.012            | 1147.09              | 1043.39                  | 0                   | 1043.39                       |
| 3            | 2.31518    | 1981.7       | Structural Fill | 50                  | 36                            | 530.185            | 653.936              | 831.245                  | 0                   | 831.245                       |
| 4            | 2.31518    | 1718.3       | Structural Fill | 50                  | 36                            | 452.27             | 557.834              | 698.974                  | 0                   | 698.974                       |
| 5            | 2.31518    | 1607.23      | Structural Fill | 50                  | 36                            | 413.418            | 509.914              | 633.018                  | 0                   | 633.018                       |
| 6            | 2.31518    | 2477.34      | Structural Fill | 50                  | 36                            | 592.25             | 730.487              | 936.612                  | 0                   | 936.612                       |
| 7            | 2.31518    | 3594.96      | Structural Fill | 50                  | 36                            | 811.972            | 1001.5               | 1309.62                  | 0                   | 1309.62                       |
| 8            | 2.31518    | 3537.91      | Structural Fill | 50                  | 36                            | 775.101            | 956.017              | 1247.02                  | 0                   | 1247.02                       |
| 9            | 2.31518    | 3461.11      | Structural Fill | 50                  | 36                            | 735.765            | 907.5                | 1180.25                  | 0                   | 1180.25                       |
| 10           | 2.31518    | 3426.8       | Structural Fill | 50                  | 36                            | 706.275            | 871.127              | 1130.18                  | 0                   | 1130.18                       |
| 11           | 2.31518    | 3371.24      | Structural Fill | 50                  | 36                            | 673.842            | 831.123              | 1075.12                  | 0                   | 1075.12                       |
| 12           | 2.31518    | 3293.61      | Structural Fill | 50                  | 36                            | 638.642            | 787.707              | 1015.37                  | 0                   | 1015.37                       |
| 13           | 2.31518    | 3192.99      | Structural Fill | 50                  | 36                            | 600.841            | 741.083              | 951.192                  | 0                   | 951.192                       |
| 14           | 2.31518    | 3068.36      | Structural Fill | 50                  | 36                            | 560.592            | 691.44               | 882.865                  | 0                   | 882.865                       |
| 15           | 2.31518    | 2918.54      | Structural Fill | 50                  | 36                            | 518.041            | 638.957              | 810.63                   | 0                   | 810.63                        |
| 16           | 2.31518    | 2742.25      | Structural Fill | 50                  | 36                            | 473.323            | 583.801              | 734.712                  | 0                   | 734.712                       |
| 17           | 2.31518    | 2537.98      | Structural Fill | 50                  | 36                            | 426.564            | 526.128              | 655.335                  | 0                   | 655.335                       |
| 18           | 2.31518    | 2300.56      | Structural Fill | 50                  | 36                            | 377.374            | 465.457              | 571.827                  | 0                   | 571.827                       |
| 19           | 2.31518    | 1893.27      | Structural Fill | 50                  | 36                            | 306.827            | 378.443              | 452.065                  | 0                   | 452.065                       |
| 20           | 2.31518    | 1552.9       | Structural Fill | 50                  | 36                            | 249.814            | 308.123              | 355.278                  | 0                   | 355.278                       |
| 21           | 2.31518    | 2253.56      | Structural Fill | 50                  | 36                            | 333.105            | 410.855              | 496.676                  | 0                   | 496.676                       |
| 22           | 0.202432   | 238.294      | Rockery         | 1315.28             | 15.4062                       | 1151.5             | 1420.27              | 380.994                  | 0                   | 380.994                       |
| 23           | 2.62858    | 2604.1       | Structural Fill | 50                  | 36                            | 324                | 399.625              | 481.218                  | 0                   | 481.218                       |
| 24           | 2.62858    | 1484.28      | Structural Fill | 50                  | 36                            | 191.938            | 236.738              | 257.023                  | 0                   | 257.023                       |

|    |         |         |                    |    |    |         |         |         |   |         |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|
| 25 | 2.62858 | 507.514 | Structural<br>Fill | 50 | 36 | 85.5659 | 105.538 | 76.4412 | 0 | 76.4412 |
|----|---------|---------|--------------------|----|----|---------|---------|---------|---|---------|

## Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.23341

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 700.35            | 8573.91                    | 0                             | 0                            | 0                                |
| 2            | 703.009           | 8574.57                    | 1115.62                       | 797.996                      | 35.5759                          |
| 3            | 705.667           | 8575.31                    | 2582.86                       | 1847.5                       | 35.5759                          |
| 4            | 707.982           | 8576.01                    | 3031.42                       | 2168.35                      | 35.5758                          |
| 5            | 710.297           | 8576.77                    | 3377.44                       | 2415.86                      | 35.5759                          |
| 6            | 712.613           | 8577.59                    | 3656.66                       | 2615.58                      | 35.5758                          |
| 7            | 714.928           | 8578.48                    | 3957.19                       | 2830.55                      | 35.5759                          |
| 8            | 717.243           | 8579.42                    | 4244.21                       | 3035.85                      | 35.5758                          |
| 9            | 719.558           | 8580.43                    | 4429.53                       | 3168.41                      | 35.5759                          |
| 10           | 721.873           | 8581.51                    | 4519.6                        | 3232.84                      | 35.5759                          |
| 11           | 724.189           | 8582.66                    | 4520.24                       | 3233.3                       | 35.5759                          |
| 12           | 726.504           | 8583.88                    | 4437.01                       | 3173.76                      | 35.5759                          |
| 13           | 728.819           | 8585.17                    | 4276.74                       | 3059.12                      | 35.5759                          |
| 14           | 731.134           | 8586.54                    | 4047.61                       | 2895.23                      | 35.5759                          |
| 15           | 733.449           | 8587.99                    | 3759.18                       | 2688.92                      | 35.5759                          |
| 16           | 735.764           | 8589.53                    | 3422.47                       | 2448.07                      | 35.5759                          |
| 17           | 738.08            | 8591.16                    | 3050.05                       | 2181.68                      | 35.5759                          |
| 18           | 740.395           | 8592.89                    | 2656.2                        | 1899.96                      | 35.5759                          |
| 19           | 742.71            | 8594.71                    | 2257.83                       | 1615.01                      | 35.5759                          |
| 20           | 745.025           | 8596.65                    | 1906.07                       | 1363.4                       | 35.5759                          |
| 21           | 747.34            | 8598.7                     | 1601.84                       | 1145.78                      | 35.5758                          |
| 22           | 749.656           | 8600.88                    | 1068.15                       | 764.044                      | 35.576                           |
| 23           | 749.858           | 8601.08                    | 1203.11                       | 860.579                      | 35.576                           |
| 24           | 752.487           | 8603.73                    | 519.48                        | 371.581                      | 35.5759                          |
| 25           | 755.115           | 8606.58                    | 143.707                       | 102.792                      | 35.5757                          |
| 26           | 757.744           | 8609.66                    | 0                             | 0                            | 0                                |

## List Of Coordinates

### Distributed Load

| X       | Y       |
|---------|---------|
| 694.18  | 8573.48 |
| 677.313 | 8573.18 |

### Distributed Load

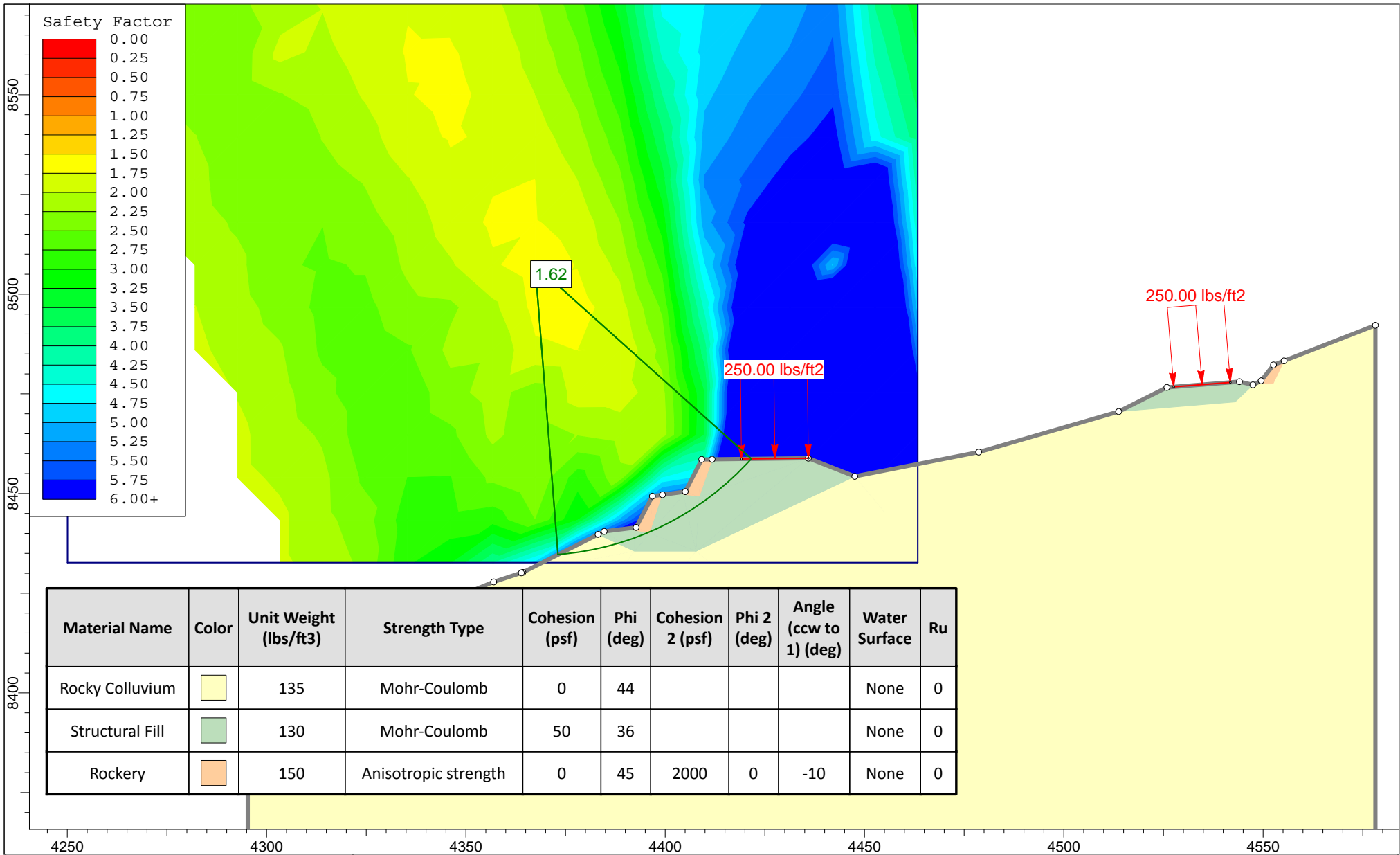
| X       | Y       |
|---------|---------|
| 775.378 | 8610.38 |
| 761.042 | 8609.79 |




### External Boundary


| X       | Y       |
|---------|---------|
| 712.158 | 8582.47 |
| 707.692 | 8581.92 |
| 704.147 | 8581.48 |
| 700.142 | 8573.49 |
| 698.139 | 8572.5  |
| 695.135 | 8573.5  |
| 669.186 | 8573.04 |
| 664.324 | 8571.26 |
| 660.858 | 8570    |
| 651.579 | 8566.97 |
| 641.697 | 8564.12 |
| 627.949 | 8560    |
| 615.417 | 8555    |
| 600.766 | 8550.43 |
| 576.666 | 8542.29 |
| 576.666 | 8484.11 |
| 933.571 | 8484.11 |
| 933.826 | 8633.99 |
| 845.33  | 8628.01 |
| 840.152 | 8627.29 |
| 839.773 | 8627.23 |
| 821.282 | 8624.26 |
| 809.037 | 8622.55 |
| 795.725 | 8620    |
| 791.035 | 8617.83 |
| 787.674 | 8616.39 |
| 785.358 | 8615.39 |
| 782.743 | 8610.58 |
| 780.553 | 8609.43 |
| 777.452 | 8610.46 |
| 752.516 | 8609.45 |
| 750.033 | 8609.35 |
| 746.292 | 8602.28 |
| 742.292 | 8601.78 |
| 718.697 | 8591.6  |
| 716.295 | 8590.56 |

### Material Boundary





| Material Name   | Color   | Unit Weight (lbs/ft3) | Strength Type        | Cohesion (psf) | Phi (deg) | Cohesion 2 (psf) | Phi 2 (deg) | Angle (ccw to 1) (deg) | Water Surface | Ru |
|-----------------|---|-----------------------|----------------------|----------------|-----------|------------------|-------------|------------------------|---------------|----|
| Rocky Colluvium |  | 135                   | Mohr-Coulomb         | 0              | 44        |                  |             |                        | None          | 0  |
| Structural Fill |  | 130                   | Mohr-Coulomb         | 50             | 36        |                  |             |                        | None          | 0  |
| Rockery         |  | 150                   | Anisotropic strength | 0              | 45        | 2000             | 0           | -10                    | None          | 0  |



*Project*  
**ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G**

*Analysis Description*  
**GLOBAL STABILITY ANALYSIS - STATIC CONDITION - SECTION 7-7'**

*Drawn By* SL      *Scale* 1:400      *Company* IGES, INC.

*Date* 9-25-2015      *File Name* Static.slim

# *Slide Analysis Information*

## *SLIDE - An Interactive Slope Stability Program*

### *Project Summary*

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File Name: Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

### *General Settings*

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

### *Analysis Options*

---

#### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m\alpha < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

### *Groundwater Analysis*

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

### *Random Numbers*

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |

## Global Minimums

---

Method: spencer

FS: 1.623560  
 Center: 4367.362, 8507.319  
 Radius: 72.876  
 Left Slip Surface Endpoint: 4373.120, 8434.671  
 Right Slip Surface Endpoint: 4421.639, 8458.689  
 Resisting Moment=1.8668e+006 lb-ft  
 Driving Moment=1.14982e+006 lb-ft  
 Resisting Horizontal Force=22391.7 lb  
 Driving Horizontal Force=13791.7 lb  
 Total Slice Area=241.237 ft2

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 4030  
 Number of Invalid Surfaces: 821

#### Error Codes:

Error Code -102 reported for 1 surface  
 Error Code -103 reported for 7 surfaces  
 Error Code -106 reported for 28 surfaces  
 Error Code -107 reported for 64 surfaces  
 Error Code -108 reported for 49 surfaces  
 Error Code -111 reported for 82 surfaces  
 Error Code -112 reported for 161 surfaces  
 Error Code -1000 reported for 429 surfaces

#### Error Codes

The following errors were encountered during the computation:

- 102 = Two surface / slope intersections, but resulting arc is actually outside soil region.
- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi))/F < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

## Slice Data

---

Global Minimum Query (spencer) - Safety Factor: 1.62356

|  |  |  |  |  | Base |  |  | Base | Effective |
|--|--|--|--|--|------|--|--|------|-----------|
|--|--|--|--|--|------|--|--|------|-----------|

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Cohesion [psf] | Friction Angle [degrees] | Stress [psf] | Strength [psf] | Normal Stress [psf] | Pressure [psf] | Normal Stress [psf] |
|--------------|------------|--------------|-----------------|----------------|--------------------------|--------------|----------------|---------------------|----------------|---------------------|
| 1            | 2.14165    | 126.877      | Rocky Colluvium | 0              | 44                       | 43.2804      | 70.2684        | 72.7648             | 0              | 72.7648             |
| 2            | 2.14165    | 371.367      | Rocky Colluvium | 0              | 44                       | 122.04       | 198.14         | 205.181             | 0              | 205.181             |
| 3            | 2.14165    | 597.227      | Rocky Colluvium | 0              | 44                       | 189.196      | 307.171        | 318.085             | 0              | 318.085             |
| 4            | 2.14165    | 804.226      | Rocky Colluvium | 0              | 44                       | 245.728      | 398.954        | 413.128             | 0              | 413.128             |
| 5            | 2.14165    | 991.029      | Rocky Colluvium | 0              | 44                       | 292.183      | 474.376        | 491.229             | 0              | 491.229             |
| 6            | 2.14165    | 1101.48      | Rocky Colluvium | 0              | 44                       | 313.459      | 508.919        | 527.004             | 0              | 527.004             |
| 7            | 2.14165    | 1019.65      | Rocky Colluvium | 0              | 44                       | 280.15       | 454.841        | 471.001             | 0              | 471.001             |
| 8            | 1.84809    | 791.135      | Structural Fill | 50             | 36                       | 212.028      | 344.24         | 404.986             | 0              | 404.986             |
| 9            | 1.84809    | 701.759      | Structural Fill | 50             | 36                       | 187.355      | 304.182        | 349.852             | 0              | 349.852             |
| 10           | 1.84809    | 753.051      | Structural Fill | 50             | 36                       | 193.987      | 314.95         | 364.672             | 0              | 364.672             |
| 11           | 1.84809    | 1480.93      | Structural Fill | 50             | 36                       | 341.603      | 554.613        | 694.538             | 0              | 694.538             |
| 12           | 0.835688   | 931.229      | Rockery         | 595.597        | 31.5991                  | 731.561      | 1187.73        | 962.539             | 0              | 962.539             |
| 13           | 1.94608    | 2360.36      | Structural Fill | 50             | 36                       | 482.118      | 782.748        | 1008.54             | 0              | 1008.54             |
| 14           | 1.94608    | 2022.57      | Structural Fill | 50             | 36                       | 406.472      | 659.932        | 839.5               | 0              | 839.5               |
| 15           | 1.94608    | 1809.46      | Structural Fill | 50             | 36                       | 357.028      | 579.656        | 729.009             | 0              | 729.009             |
| 16           | 1.94608    | 1609.17      | Structural Fill | 50             | 36                       | 312.152      | 506.797        | 628.727             | 0              | 628.727             |
| 17           | 1.94608    | 1561.81      | Structural Fill | 50             | 36                       | 295.433      | 479.653        | 591.367             | 0              | 591.367             |
| 18           | 1.94608    | 2269.69      | Structural Fill | 50             | 36                       | 403.906      | 655.765        | 833.763             | 0              | 833.763             |
| 19           | 1.94608    | 2901.69      | Structural Fill | 50             | 36                       | 493.076      | 800.539        | 1033.03             | 0              | 1033.03             |
| 20           | 1.94608    | 2534.43      | Structural Fill | 50             | 36                       | 421.034      | 683.574        | 872.039             | 0              | 872.039             |
| 21           | 1.94608    | 2065.74      | Structural Fill | 50             | 36                       | 337.482      | 547.922        | 685.331             | 0              | 685.331             |
| 22           | 1.94608    | 1663.16      | Structural Fill | 50             | 36                       | 268.203      | 435.443        | 530.516             | 0              | 530.516             |
| 23           | 1.94608    | 1230.37      | Structural Fill | 50             | 36                       | 198.75       | 322.683        | 375.316             | 0              | 375.316             |
| 24           | 1.94608    | 764.339      | Structural Fill | 50             | 36                       | 147.982      | 240.257        | 261.866             | 0              | 261.866             |
| 25           | 1.94608    | 261.295      | Structural Fill | 50             | 36                       | 125.878      | 204.37         | 212.472             | 0              | 212.472             |

### Interslice Data

Global Minimum Query (spencer) - Safety Factor: 1.62356

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 4373.12           | 8434.67                    | 0                             | 0                            | 0                                |
| 2            | 4375.26           | 8434.87                    | 78.1731                       | 39.2185                      | 26.6424                          |
| 3            | 4377.4            | 8435.14                    | 285.455                       | 143.209                      | 26.6423                          |
| 4            | 4379.55           | 8435.47                    | 586.19                        | 294.084                      | 26.6423                          |
| 5            | 4381.69           | 8435.86                    | 949.647                       | 476.426                      | 26.6423                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 6  | 4383.83 | 8436.33 | 1349.01 | 676.78  | 26.6423 |
| 7  | 4385.97 | 8436.86 | 1741.56 | 873.717 | 26.6423 |
| 8  | 4388.11 | 8437.46 | 2059.58 | 1033.27 | 26.6424 |
| 9  | 4389.96 | 8438.04 | 2218.9  | 1113.2  | 26.6425 |
| 10 | 4391.81 | 8438.67 | 2345.2  | 1176.56 | 26.6424 |
| 11 | 4393.66 | 8439.35 | 2453.99 | 1231.14 | 26.6424 |
| 12 | 4395.5  | 8440.1  | 2569.48 | 1289.08 | 26.6424 |
| 13 | 4396.34 | 8440.45 | 2839.18 | 1424.38 | 26.6423 |
| 14 | 4398.29 | 8441.33 | 2894.02 | 1451.89 | 26.6423 |
| 15 | 4400.23 | 8442.28 | 2890.94 | 1450.35 | 26.6424 |
| 16 | 4402.18 | 8443.3  | 2842.84 | 1426.22 | 26.6424 |
| 17 | 4404.12 | 8444.39 | 2761.41 | 1385.36 | 26.6423 |
| 18 | 4406.07 | 8445.57 | 2640.6  | 1324.76 | 26.6424 |
| 19 | 4408.02 | 8446.84 | 2374.39 | 1191.2  | 26.6423 |
| 20 | 4409.96 | 8448.19 | 1936.22 | 971.376 | 26.6423 |
| 21 | 4411.91 | 8449.64 | 1490.75 | 747.892 | 26.6424 |
| 22 | 4413.85 | 8451.2  | 1081.59 | 542.62  | 26.6423 |
| 23 | 4415.8  | 8452.87 | 717.96  | 360.192 | 26.6424 |
| 24 | 4417.75 | 8454.67 | 431.431 | 216.444 | 26.6424 |
| 25 | 4419.69 | 8456.6  | 215.118 | 107.922 | 26.6423 |
| 26 | 4421.64 | 8458.69 | 0       | 0       | 0       |

## List Of Coordinates

---

### Distributed Load

| X       | Y       |
|---------|---------|
| 4435.9  | 8458.85 |
| 4419.14 | 8458.66 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 4541.78 | 8477.86 |
| 4527.59 | 8476.73 |

### External Boundary

| X       | Y       |
|---------|---------|
| 4364.31 | 8430.23 |
| 4363.92 | 8430.1  |
| 4356.96 | 8427.82 |
| 4350.03 | 8425    |
| 4336.26 | 8420.12 |
| 4322.94 | 8414.14 |
| 4308.1  | 8406.75 |

|         |         |
|---------|---------|
| 4300    | 8404    |
| 4295.28 | 8404.05 |
| 4295.28 | 8297.19 |
| 4578.16 | 8297.19 |
| 4578.16 | 8492.19 |
| 4555.26 | 8483.29 |
| 4552.6  | 8482.25 |
| 4549.49 | 8478.28 |
| 4547.45 | 8477.25 |
| 4544.04 | 8478.04 |
| 4525.85 | 8476.6  |
| 4513.76 | 8470.55 |
| 4478.68 | 8460.38 |
| 4447.56 | 8454.3  |
| 4435.9  | 8458.85 |
| 4411.77 | 8458.57 |
| 4409.16 | 8458.54 |
| 4405.03 | 8450.47 |
| 4399.32 | 8449.68 |
| 4396.77 | 8449.33 |
| 4392.68 | 8441.5  |
| 4384.68 | 8440.5  |
| 4383.17 | 8439.74 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4392.68 | 8441.5  |
| 4392.24 | 8440.6  |
| 4396.19 | 8439.99 |
| 4399.32 | 8449.68 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4405.03 | 8450.47 |
| 4404.53 | 8449.6  |
| 4408.51 | 8449.15 |
| 4411.77 | 8458.57 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4549.49 | 8478.28 |
| 4548.87 | 8477.49 |
| 4552.37 | 8477.28 |

|         |         |
|---------|---------|
| 4555.26 | 8483.29 |
|---------|---------|

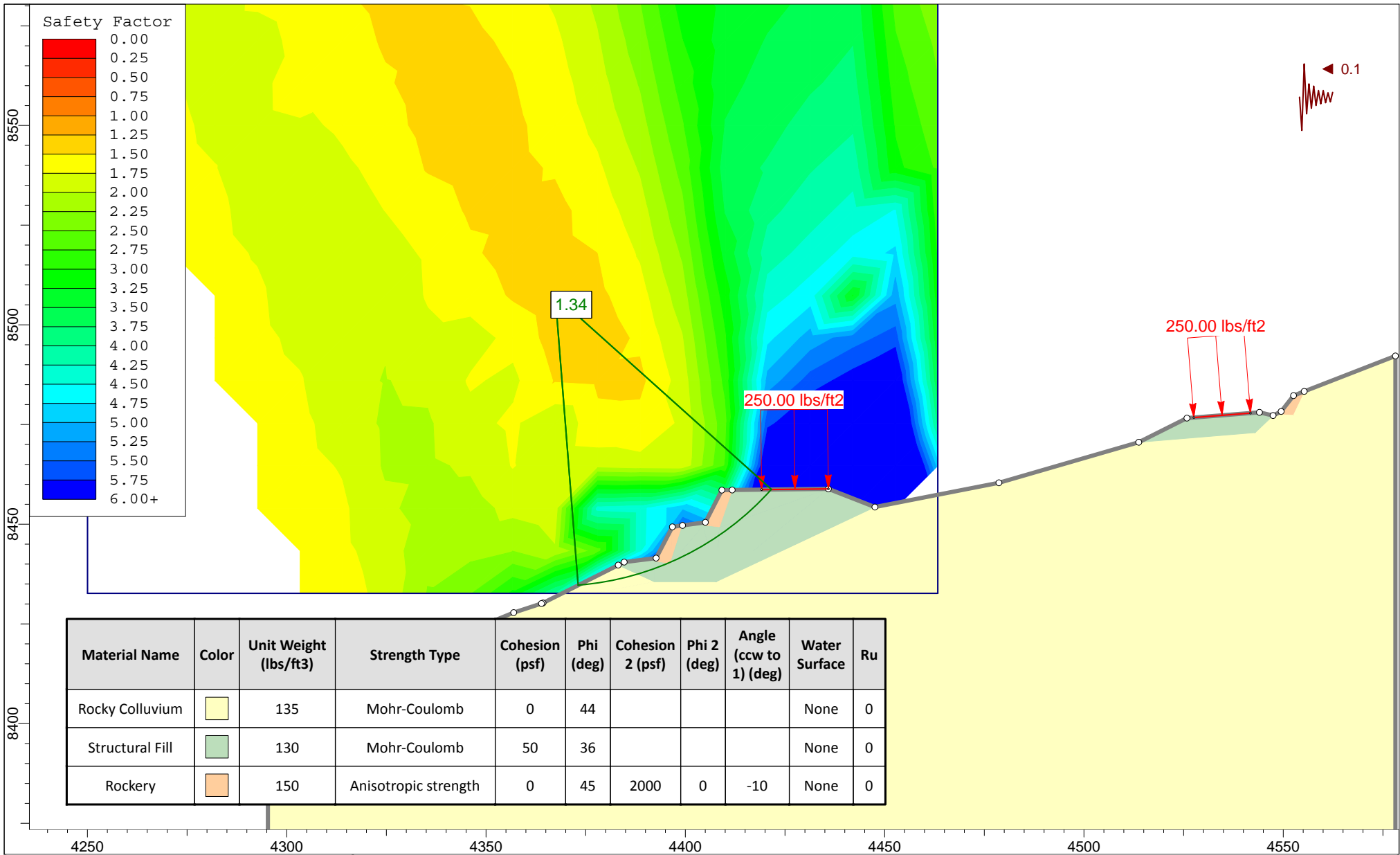
### Material Boundary


| X       | Y       |
|---------|---------|
| 4383.17 | 8439.74 |
| 4392.23 | 8435.56 |
| 4407.72 | 8435.56 |
| 4447.56 | 8454.3  |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4513.76 | 8470.55 |
| 4542.97 | 8472.96 |
| 4547.45 | 8477.25 |





|  |                      |           |       |  |               |            |
|--|----------------------|-----------|-------|--|---------------|------------|
|  | Project              |           |       | ROCKERY DESIGN - SUMMIT POWDER MOUNTAIN PHASE 1E/1F/1G       |               |            |
|  | Analysis Description |           |       | GLOBAL STABILITY ANALYSIS - SEISMIC CONDITION - SECTION 7-7' |               |            |
|  | Drawn By             | SL        | Scale | 1:400  | Company       | IGES, INC. |
|  | Date                 | 9-25-2015 |       | File Name  | P-Static.slim |            |

## ***Slide Analysis Information***

### ***SLIDE - An Interactive Slope Stability Program***

#### ***Project Summary***

---

File Name: P-Static  
Slide Modeler Version: 6.029  
Project Title: SLIDE - An Interactive Slope Stability Program  
Date Created: 8/13/2015, 2:54:03 PM

#### ***General Settings***

---

Units of Measurement: Imperial Units  
Time Units: days  
Permeability Units: feet/second  
Failure Direction: Right to Left  
Data Output: Standard  
Maximum Material Properties: 20  
Maximum Support Properties: 20

#### ***Analysis Options***

---

##### **Analysis Methods Used**

Spencer

Number of slices: 25  
Tolerance: 0.005  
Maximum number of iterations: 50  
Check  $m_{\alpha} < 0.2$ : Yes  
Initial trial value of FS: 1  
Steffensen Iteration: Yes

#### ***Groundwater Analysis***

---

Groundwater Method: Water Surfaces  
Pore Fluid Unit Weight: 62.4 lbs/ft<sup>3</sup>  
Advanced Groundwater Method: None

#### ***Random Numbers***

---

Pseudo-random Seed: 10116  
Random Number Generation Method: Park and Miller v.3

## Surface Options

---

Surface Type: Circular  
 Search Method: Grid Search  
 Radius Increment: 10  
 Composite Surfaces: Disabled  
 Reverse Curvature: Create Tension Crack  
 Minimum Elevation: Not Defined  
 Minimum Depth: Not Defined

## Loading

---

Seismic Load Coefficient (Horizontal): 0.1  
 2 Distributed Loads present

### Distributed Load 1




Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

### Distributed Load 2

Distribution: Constant  
 Magnitude [psf]: 250  
 Orientation: Normal to boundary

## Material Properties

---

| Property               | Rocky Colluvium   | Structural Fill   | Rockery   |
|------------------------|---|---|---|
| Color                  |  |  |  |
| Strength Type          | Mohr-Coulomb  | Mohr-Coulomb  | Anisotropic strength  |
| Unit Weight [lbs/ft3]  | 135   | 130   | 150   |
| Cohesion [psf]         | 0   | 50  |   |
| Friction Angle [deg]   | 44  | 36  |   |
| Cohesion 1 [psf]       |   |   | 0   |
| Cohesion 2 [psf]       |   |   | 2000  |
| Friction Angle 1 [deg] |   |   | 45  |
| Friction Angle 2 [deg] |   |   | 0   |
| Angle from 1 [deg]     |   |   | -10   |
| Water Surface          | None  | None  | None  |
| Ru Value               | 0   | 0   | 0   |

## Global Minimums

---

## Method: spencer

FS: 1.343240  
Center: 4367.362, 8507.319  
Radius: 72.876  
Left Slip Surface Endpoint: 4373.120, 8434.671  
Right Slip Surface Endpoint: 4421.639, 8458.689  
Resisting Moment=1.80756e+006 lb-ft  
Driving Moment=1.34567e+006 lb-ft  
Resisting Horizontal Force=21733.2 lb  
Driving Horizontal Force=16179.7 lb  
Total Slice Area=241.237 ft2

## Valid / Invalid Surfaces

---

### Method: spencer

Number of Valid Surfaces: 3895  
Number of Invalid Surfaces: 956

#### Error Codes:

Error Code -102 reported for 1 surface  
Error Code -103 reported for 7 surfaces  
Error Code -106 reported for 28 surfaces  
Error Code -107 reported for 28 surfaces  
Error Code -108 reported for 104 surfaces  
Error Code -111 reported for 158 surfaces  
Error Code -112 reported for 201 surfaces  
Error Code -1000 reported for 429 surfaces

#### Error Codes

The following errors were encountered during the computation:

- 102 = Two surface / slope intersections, but resulting arc is actually outside soil region.
- 103 = Two surface / slope intersections, but one or more surface / nonslope external polygon intersections lie between them. This usually occurs when the slip surface extends past the bottom of the soil region, but may also occur on a benched slope model with two sets of Slope Limits.
- 106 = Average slice width is less than 0.0001 \* (maximum horizontal extent of soil region). This limitation is imposed to avoid numerical errors which may result from too many slices, or too small a slip region.
- 107 = Total driving moment or total driving force is negative. This will occur if the wrong failure direction is specified, or if high external or anchor loads are applied against the failure direction.
- 108 = Total driving moment or total driving force < 0.1. This is to limit the calculation of extremely high safety factors if the driving force is very small (0.1 is an arbitrary number).
- 111 = safety factor equation did not converge
- 112 = The coefficient  $M\text{-Alpha} = \cos(\alpha)(1 + \tan(\alpha)\tan(\phi)/F) < 0.2$  for the final iteration of the safety factor calculation. This screens out some slip surfaces which may not be valid in the context of the analysis, in particular, deep seated slip surfaces with many high negative base angle slices in the passive zone.
- 1000 = No valid slip surfaces are generated at a grid center. Unable to draw a surface.

## Slice Data

---

**Global Minimum Query (spencer) - Safety Factor: 1.34324**

| Slice Number | Width [ft] | Weight [lbs] | Base Material   | Base Cohesion [psf] | Base Friction Angle [degrees] | Shear Stress [psf] | Shear Strength [psf] | Base Normal Stress [psf] | Pore Pressure [psf] | Effective Normal Stress [psf] |
|--------------|------------|--------------|-----------------|---------------------|-------------------------------|--------------------|----------------------|--------------------------|---------------------|-------------------------------|
| 1            | 2.14165    | 126.877      | Rocky Colluvium | 0                   | 44                            | 59.2548            | 79.5934              | 82.4212                  | 0                   | 82.4212                       |
| 2            | 2.14165    | 371.367      | Rocky Colluvium | 0                   | 44                            | 164.047            | 220.355              | 228.184                  | 0                   | 228.184                       |
| 3            | 2.14165    | 597.227      | Rocky Colluvium | 0                   | 44                            | 249.973            | 335.774              | 347.705                  | 0                   | 347.705                       |
| 4            | 2.14165    | 804.226      | Rocky Colluvium | 0                   | 44                            | 319.443            | 429.089              | 444.335                  | 0                   | 444.335                       |
| 5            | 2.14165    | 991.029      | Rocky Colluvium | 0                   | 44                            | 374.072            | 502.469              | 520.323                  | 0                   | 520.323                       |
| 6            | 2.14165    | 1101.48      | Rocky Colluvium | 0                   | 44                            | 395.56             | 531.332              | 550.212                  | 0                   | 550.212                       |
| 7            | 2.14165    | 1019.65      | Rocky Colluvium | 0                   | 44                            | 348.731            | 468.429              | 485.073                  | 0                   | 485.073                       |
| 8            | 1.84809    | 791.135      | Structural Fill | 50                  | 36                            | 256.341            | 344.327              | 405.106                  | 0                   | 405.106                       |
| 9            | 1.84809    | 701.759      | Structural Fill | 50                  | 36                            | 225.275            | 302.599              | 347.672                  | 0                   | 347.672                       |
| 10           | 1.84809    | 753.051      | Structural Fill | 50                  | 36                            | 231.358            | 310.769              | 358.918                  | 0                   | 358.918                       |
| 11           | 1.84809    | 1480.93      | Structural Fill | 50                  | 36                            | 401.045            | 538.7                | 672.639                  | 0                   | 672.639                       |
| 12           | 0.835688   | 931.229      | Rockery         | 595.597             | 31.5991                       | 888.362            | 1193.28              | 971.563                  | 0                   | 971.563                       |
| 13           | 1.94608    | 2360.36      | Structural Fill | 50                  | 36                            | 558.232            | 749.84               | 963.245                  | 0                   | 963.245                       |
| 14           | 1.94608    | 2022.57      | Structural Fill | 50                  | 36                            | 467.952            | 628.572              | 796.335                  | 0                   | 796.335                       |
| 15           | 1.94608    | 1809.46      | Structural Fill | 50                  | 36                            | 408.684            | 548.961              | 686.76                   | 0                   | 686.76                        |
| 16           | 1.94608    | 1609.17      | Structural Fill | 50                  | 36                            | 355.422            | 477.417              | 588.291                  | 0                   | 588.291                       |
| 17           | 1.94608    | 1561.81      | Structural Fill | 50                  | 36                            | 334.334            | 449.091              | 549.299                  | 0                   | 549.299                       |
| 18           | 1.94608    | 2269.69      | Structural Fill | 50                  | 36                            | 452.213            | 607.431              | 767.237                  | 0                   | 767.237                       |
| 19           | 1.94608    | 2901.69      | Structural Fill | 50                  | 36                            | 547.141            | 734.942              | 942.744                  | 0                   | 942.744                       |
| 20           | 1.94608    | 2534.43      | Structural Fill | 50                  | 36                            | 464.588            | 624.053              | 790.117                  | 0                   | 790.117                       |
| 21           | 1.94608    | 2065.74      | Structural Fill | 50                  | 36                            | 370.658            | 497.882              | 616.457                  | 0                   | 616.457                       |
| 22           | 1.94608    | 1663.16      | Structural Fill | 50                  | 36                            | 293.376            | 394.075              | 473.579                  | 0                   | 473.579                       |
| 23           | 1.94608    | 1230.37      | Structural Fill | 50                  | 36                            | 217.028            | 291.521              | 332.425                  | 0                   | 332.425                       |
| 24           | 1.94608    | 764.339      | Structural Fill | 50                  | 36                            | 163.037            | 218.998              | 232.606                  | 0                   | 232.606                       |
| 25           | 1.94608    | 261.295      | Structural Fill | 50                  | 36                            | 138.776            | 186.409              | 187.751                  | 0                   | 187.751                       |

### Interslice Data

**Global Minimum Query (spencer) - Safety Factor: 1.34324**

| Slice Number | X coordinate [ft] | Y coordinate - Bottom [ft] | Interslice Normal Force [lbs] | Interslice Shear Force [lbs] | Interslice Force Angle [degrees] |
|--------------|-------------------|----------------------------|-------------------------------|------------------------------|----------------------------------|
| 1            | 4373.12           | 8434.67                    | 0                             | 0                            | 0                                |
| 2            | 4375.26           | 8434.87                    | 97.8624                       | 63.406                       | 32.9396                          |
| 3            | 4377.4            | 8435.14                    | 352.163                       | 228.17                       | 32.9396                          |
| 4            | 4379.55           | 8435.47                    | 714.001                       | 462.608                      | 32.9396                          |

|    |         |         |         |         |         |
|----|---------|---------|---------|---------|---------|
| 5  | 4381.69 | 8435.86 | 1143.11 | 740.63  | 32.9395 |
| 6  | 4383.83 | 8436.33 | 1605.92 | 1040.49 | 32.9396 |
| 7  | 4385.97 | 8436.86 | 2052.49 | 1329.83 | 32.9396 |
| 8  | 4388.11 | 8437.46 | 2407.54 | 1559.87 | 32.9396 |
| 9  | 4389.96 | 8438.04 | 2569.92 | 1665.08 | 32.9397 |
| 10 | 4391.81 | 8438.67 | 2697.8  | 1747.93 | 32.9396 |
| 11 | 4393.66 | 8439.35 | 2804.6  | 1817.13 | 32.9396 |
| 12 | 4395.5  | 8440.1  | 2898.66 | 1878.07 | 32.9396 |
| 13 | 4396.34 | 8440.45 | 3203.6  | 2075.65 | 32.9397 |
| 14 | 4398.29 | 8441.33 | 3210.99 | 2080.43 | 32.9396 |
| 15 | 4400.23 | 8442.28 | 3166.79 | 2051.8  | 32.9397 |
| 16 | 4402.18 | 8443.3  | 3081.92 | 1996.81 | 32.9396 |
| 17 | 4404.12 | 8444.39 | 2968.59 | 1923.38 | 32.9396 |
| 18 | 4406.07 | 8445.57 | 2817.28 | 1825.34 | 32.9396 |
| 19 | 4408.02 | 8446.84 | 2502.71 | 1621.53 | 32.9396 |
| 20 | 4409.96 | 8448.19 | 2002.52 | 1297.46 | 32.9398 |
| 21 | 4411.91 | 8449.64 | 1507.87 | 976.961 | 32.9395 |
| 22 | 4413.85 | 8451.2  | 1064.35 | 689.602 | 32.9396 |
| 23 | 4415.8  | 8452.87 | 678.865 | 439.843 | 32.9396 |
| 24 | 4417.75 | 8454.67 | 382.132 | 247.587 | 32.9396 |
| 25 | 4419.69 | 8456.6  | 175.455 | 113.679 | 32.9396 |
| 26 | 4421.64 | 8458.69 | 0       | 0       | 0       |

## List Of Coordinates

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### Distributed Load

| X       | Y       |
|---------|---------|
| 4435.9  | 8458.85 |
| 4419.14 | 8458.66 |

### Distributed Load

| X       | Y       |
|---------|---------|
| 4541.78 | 8477.86 |
| 4527.59 | 8476.73 |

### External Boundary

| X       | Y       |
|---------|---------|
| 4364.31 | 8430.23 |
| 4363.92 | 8430.1  |
| 4356.96 | 8427.82 |
| 4350.03 | 8425    |
| 4336.26 | 8420.12 |

|         |         |
|---------|---------|
| 4322.94 | 8414.14 |
| 4308.1  | 8406.75 |
| 4300    | 8404    |
| 4295.28 | 8404.05 |
| 4295.28 | 8297.19 |
| 4578.16 | 8297.19 |
| 4578.16 | 8492.19 |
| 4555.26 | 8483.29 |
| 4552.6  | 8482.25 |
| 4549.49 | 8478.28 |
| 4547.45 | 8477.25 |
| 4544.04 | 8478.04 |
| 4525.85 | 8476.6  |
| 4513.76 | 8470.55 |
| 4478.68 | 8460.38 |
| 4447.56 | 8454.3  |
| 4435.9  | 8458.85 |
| 4411.77 | 8458.57 |
| 4409.16 | 8458.54 |
| 4405.03 | 8450.47 |
| 4399.32 | 8449.68 |
| 4396.77 | 8449.33 |
| 4392.68 | 8441.5  |
| 4384.68 | 8440.5  |
| 4383.17 | 8439.74 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4392.68 | 8441.5  |
| 4392.24 | 8440.6  |
| 4396.19 | 8439.99 |
| 4399.32 | 8449.68 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4405.03 | 8450.47 |
| 4404.53 | 8449.6  |
| 4408.51 | 8449.15 |
| 4411.77 | 8458.57 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4549.49 | 8478.28 |

|         |         |
|---------|---------|
| 4548.87 | 8477.49 |
| 4552.37 | 8477.28 |
| 4555.26 | 8483.29 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4383.17 | 8439.74 |
| 4392.23 | 8435.56 |
| 4407.72 | 8435.56 |
| 4447.56 | 8454.3  |

### Material Boundary

| X       | Y       |
|---------|---------|
| 4513.76 | 8470.55 |
| 4542.97 | 8472.96 |
| 4547.45 | 8477.25 |



| X       | Y       |
|---------|---------|
| 746.292 | 8602.28 |
| 745.825 | 8601.39 |
| 749.79  | 8600.86 |
| 752.516 | 8609.45 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 700.142 | 8573.49 |
| 699.694 | 8572.6  |
| 704.661 | 8572.02 |
| 707.692 | 8581.92 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 712.158 | 8582.47 |
| 711.7   | 8581.58 |
| 715.694 | 8581.35 |
| 718.697 | 8591.6  |

### Material Boundary

| X       | Y       |
|---------|---------|
| 782.743 | 8610.58 |
| 782.247 | 8609.72 |
| 785.719 | 8609.28 |
| 787.674 | 8616.39 |

### Material Boundary

| X       | Y       |
|---------|---------|
| 664.324 | 8571.26 |
| 671.862 | 8570.09 |
| 704.542 | 8569.71 |
| 709.945 | 8570.55 |
| 719.592 | 8573.92 |
| 731.958 | 8583.42 |
| 749.265 | 8587.78 |
| 778.566 | 8599.76 |
| 789.567 | 8604.18 |
| 816.212 | 8614.87 |
| 839.773 | 8627.23 |