## GABION WALL DESIGN PACKAGE LOT 39 SUMMIT POWDER MOUNTAIN RESORT 8365 EAST SUMMIT PASS WEBER COUNTY, UTAH



NOTE: THIS PLAN SET HAS BEEN PREPARED WITH COLOR LINE-TYPES TO MAKE SOME DETAILS AND SPECIFICATIONS MORE CLEAR. ANY COPIES OF THESE PLANS SHOULD BE MADE IN COLOR. PHOTO TAKEN JUNE 18, 2017.

SCALE: 1" = 250' (11x17 ONLY)



12429 SOUTH 300 EAST, STE. 100 DRAPER, UTAH 84020 (801) 748-4044 FAX: (801) 748-4045

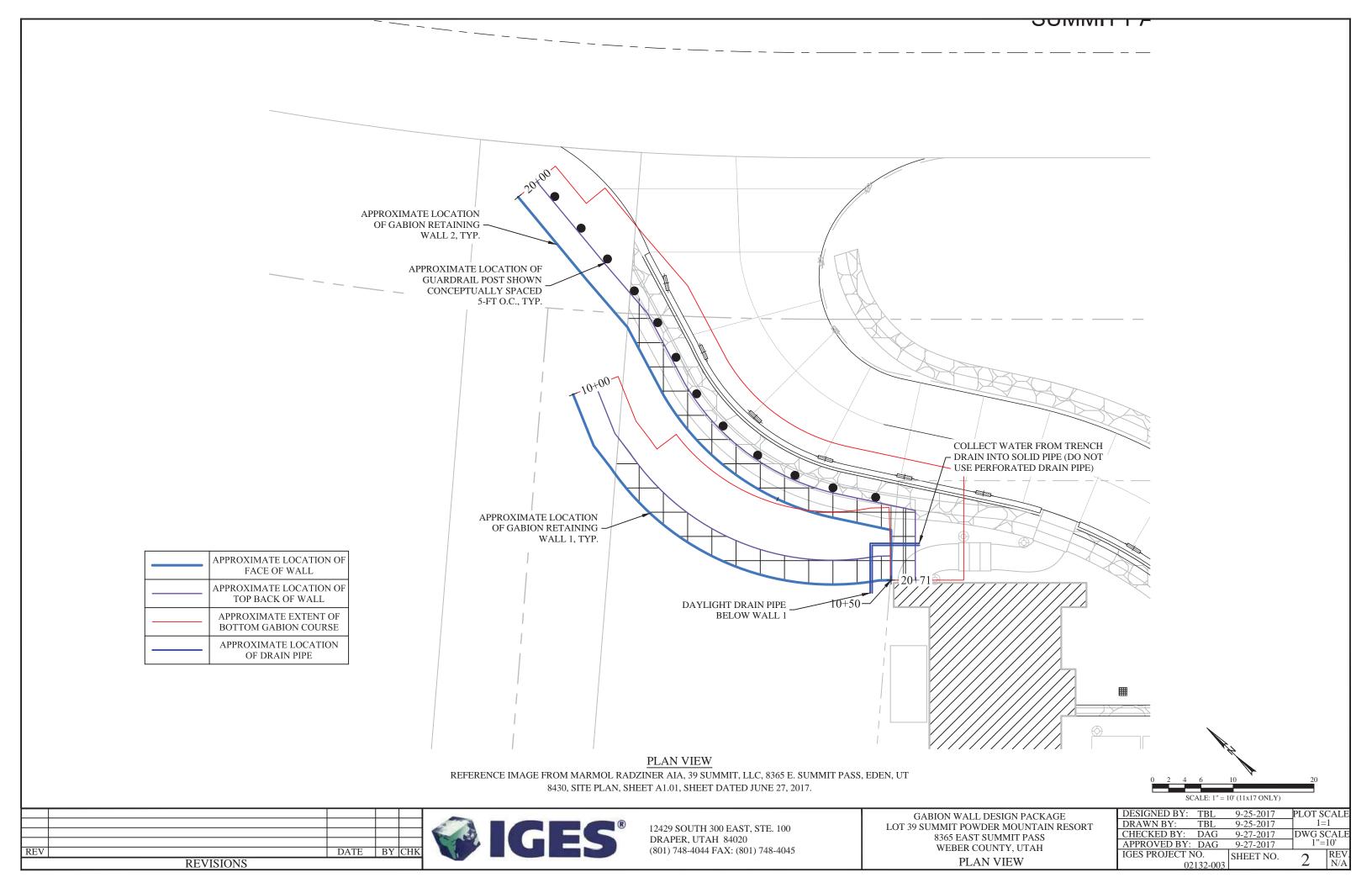
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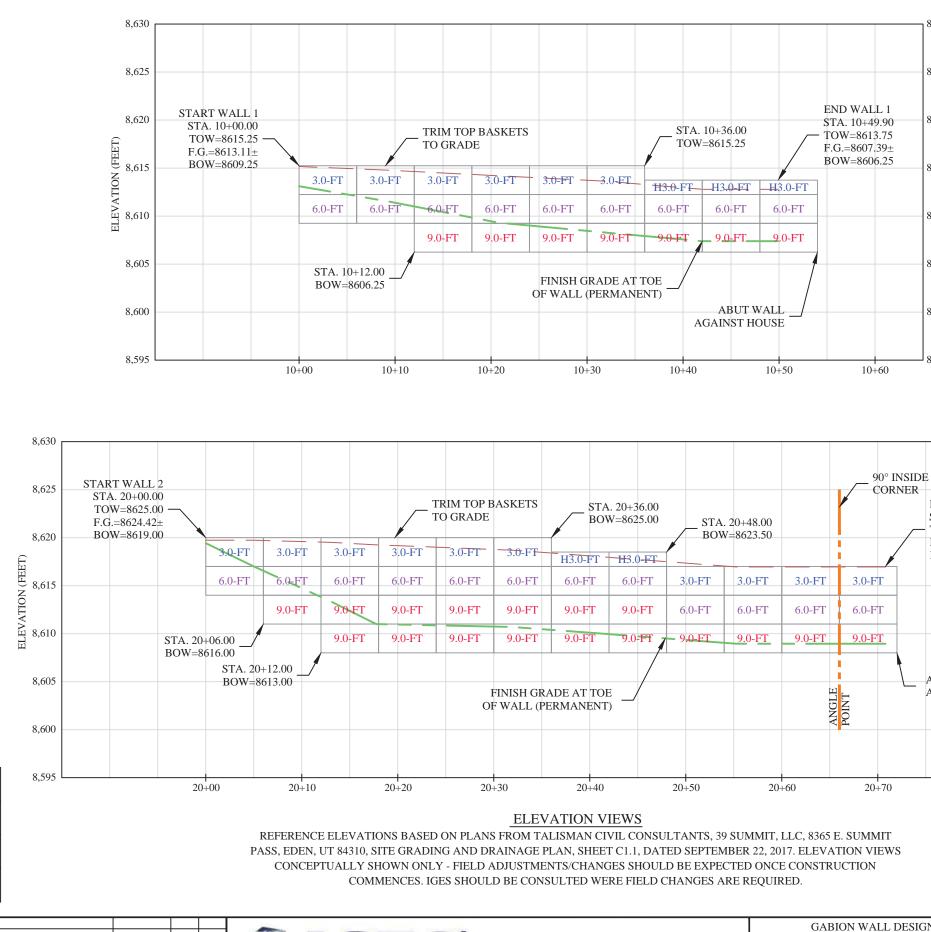
REVISIONS

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DESIGN PACKAGE CONTENTS			
	SHEET NO. DESCRIPTION		
	1	COVER SHEET	
	2	PLAN VIEW	
SHOP	3	ELEVATION VIEWS	
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	5	CONSTRUCTION SPECIFICATIONS & NOTES	
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DESIGN CALCULATION	SECTION 2	GABION STABILITY CALCULATIONS	
PACKAGE	SECTION 3	GLOBAL STABILITY CALCULATIONS	

PREPARED FOR:	39 SUMMIT LLC 314 LYTTON AVENUE, SUITE 200 PALO ALTO, CA 94301 ATTN: MEGAN MILLER & CASSANDRA BERESINI
PREPARED BY:	Tyler B. LOERTSCER, P.E.I.
REVIEWED BY:	DAVID A. GLASS, P.E.
N PACKAGE	DESIGNED BY: TBL 9-25-2017 PLOT SCALE
OUNTAIN RESORT	DRAWN BY: TBL 9-25-2017 1=1
IT PASS	CHECKED BY:         DAG         9-27-2017         DWG SCALE           APPROVED BY:         DAG         9-27-2017         1"=250'
, UTAH	
EET	IGES PROJECT NO. 02132-003 SHEET NO. 1 REV. N/A





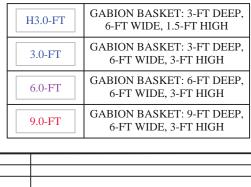
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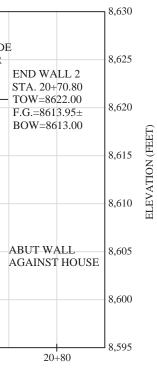
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REVISIONS

UABION WALL DESIG LOT 39 SUMMIT POWDER M 8365 EAST SUMM WEBER COUNTY ELEVATION

8,630		
8,625		
8,620	0	
8,615	ION (FEET	
8,610	ELEVATION	
8,605		
8,600		

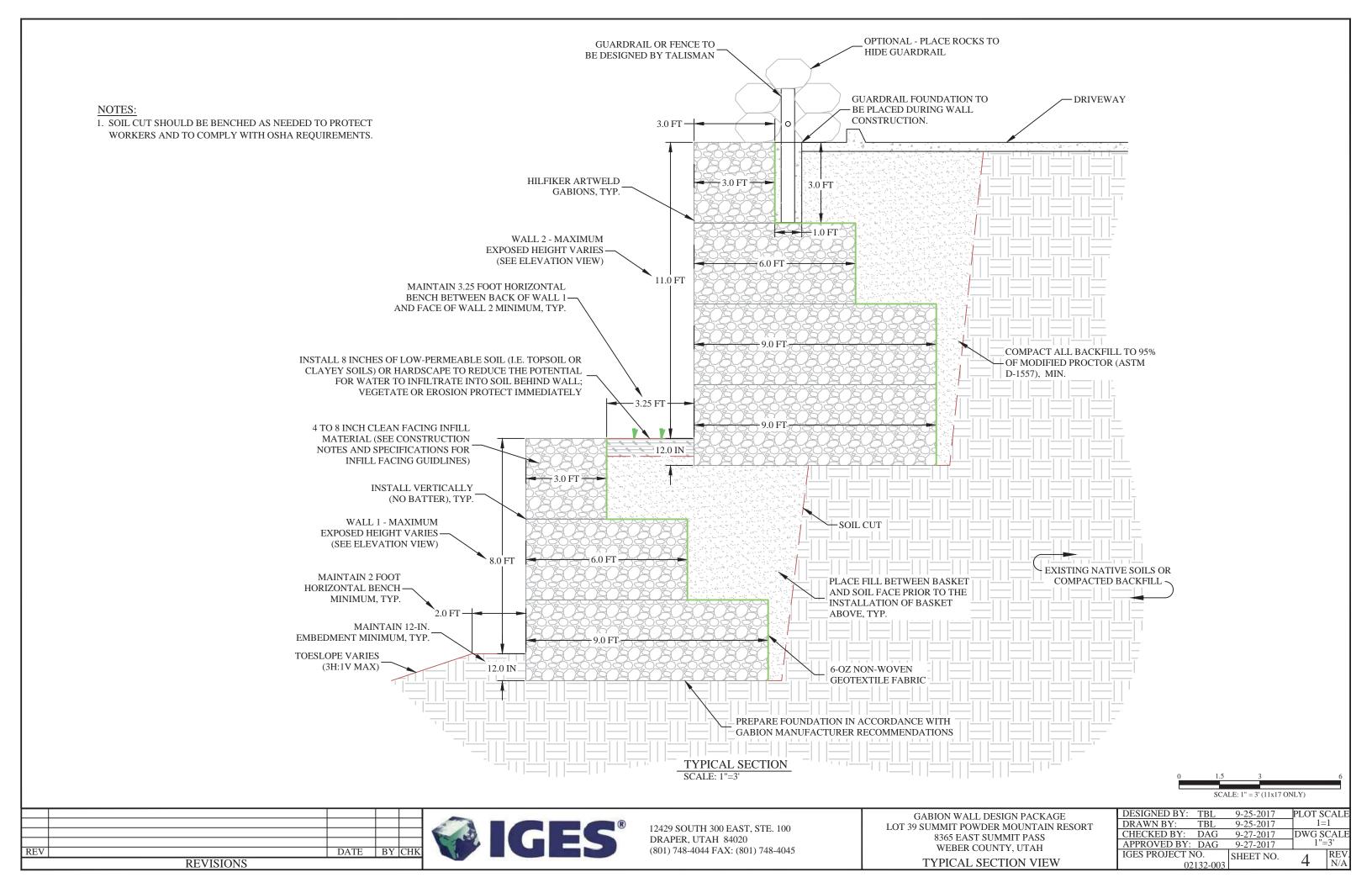
8,595



## LEGEND

## TOW = TOP OF RETAINING WALL BOW = BOTTOM OF RETAINING WALL FG = FINISHED GRADE AT BOTTOM OF WALL

	0 2 4 6 SCALE: 1	10 " = 10' (11x17 ONLY)	20
GN PACKAGE	DESIGNED BY: TBL	9-25-2017	PLOT SCALE
MOUNTAIN RESORT	DRAWN BY: TBL	9-25-2017	1=1
MIT PASS	CHECKED BY: DAG	9-27-2017	DWG SCALE
Y. UTAH	APPROVED BY: DAG	9-27-2017	1"=10'
VIEWS	IGES PROJECT NO. 02132-003	SHEET NO.	3 REV. N/A



### CONSTRUCTION SPECIFICATIONS

1. INTRODUCTION

- 1.1. FOLLOW THE GUIDANCE CONTAINED IN THE HILFIKER GABION CONSTRUCTION MANUAL FOR THE RETAINING WALL UNLESS SPECIFICALLY SUPERSEDED BY MORE STRINGENT SPECIFICATION OR MATERIAL PROPERTIES PROVIDED HEREIN OR ON THE DRAWINGS
- IN THE EVENT THERE IS ANY CONFLICT OR AMBIGUITY BETWEEN THE FOLLOWING SPECIFICATIONS AND THE REFERENCED 1.1.1 GUIDANCE, BRING ANY SUCH ISSUES IMMEDIATELY TO THE ATTENTION OF IGES, INC. FOR WRITTEN CLARIFICATION.
- DESIGN AND CONSTRUCTION INFORMATION IS BASED ON GEOTECHNICAL INFORMATION OBTAINED FROM SITE TOPOGRAPHY. 1.2 PROJECT PLANS, SITE GEOMETRY, SITE OBSERVATIONS, DISCUSSIONS WITH THE CLIENT AND THE ENGINEERING ANALYSIS PERFORMED AS PART OF THE SCOPE OF WORK FOR THIS PROJECT BY IGES, INC.
- LOCATE ALL EXISTING UTILITIES PRIOR TO RETAINING WALL CONSTRUCTION.
- 1.4. THE DESIGN HAS IMPLEMENTED THE FOLLOWING MEASURES TO REDUCE THE POTENTIAL FOR SATURATION OF THE SOIL BEHIND THE RETAINING WALLS:
- 1.4.1 ESTABLISH HARSCAPE, VEGETATION, OR EROSION CONTROL MEASURES ABOVE AND BELOW WALL IMMEDIATELY FOLLOWING CONSTRUCTION.
- 1.5. CONDITIONS SUCH AS LEAKY OR BROKEN IRRIGATION LINES AND/OR UNCONTROLLED RUNOFF FROM IMPROPER SITE GRADING (I.E. ALLOWING WATER TO POND ABOVE RETAINING WALL) CAN LEAD TO UNDERMINING OR HYDROSTATIC PRESSURES BUILDING UP BEHIND THE WALLS, WHICH CAN LEAD TO SLOPE OR WALL MOVEMENT.
- 1.5.1. HYDROSTATIC CONDITIONS WERE NOT CONSIDERED AND MUST BE PREVENTED.
- THE OWNER SHALL BE AWARE OF THE RISKS IF THESE OR OTHER CONDITIONS OCCUR THAT COULD SATURATE OR ERODE THE 1.5.2. SOIL BEHIND THE WALLS.
- 1.5.3. RETAINING WALLS ARE VULNERABLE TO EROSION AND HYDROSTATIC PRESSURES IMMEDIATELY AFTER INSTALLATION OF THE RETAINING WALL BASKETS, BUT PRIOR TO THE PLACEMENT OF THE LANDSCAPING OR FINISHING ELEMENTS AT THE SITE (I.E. 8-INCHES OF LOW PERMEABLE SOIL/HARDSCAPE, INSTALLATION OF CURB & GUTTER, VEGETATION OF SLOPES, ETC.). AS THESE ARE CRITICAL COMPONENTS TO THE OVERALL STABILITY OF THE RETAINING WALLS, THE RETAINING WALLS ARE NOT CONSIDERED COMPLETELY INSTALLED UNTIL THE LANDSCAPING/FINISHING ELEMENTS ARE COMPLETED. WE RECOMMEND THAT THESE ELEMENTS BE INSTALLED IMMEDIATELY FOLLOWING THE INSTALLATION OF THE BASKETS
- THE OWNER SHALL BE AWARE OF THE RISK TO THE RETAINING WALLS IF THE FINISHING/LANDSCAPING ELEMENTS ARE 1531 NOT INSTALLED IMMEDIATELY FOLLOWING THE INSTALLATION OF THE RETAINING WALL BASKETS.
- COMPLY WITH ALL ASPECTS OF OSHA 1926 SUBPART P APP B, SLOPING AND BENCHING FOR ALL EXCAVATED SLOPES. 1.6.

### 2. GABION RETAINING WALL MATERIALS

- 2.1. HILFIKER GABION BASKETS CONSISTING OF ARTWELD GABION PRODUCTS USING 3"x3" 9 GAUGE WELDED WIRE MESH THAT HAS BEEN ELECTROPLATE GALVANIZED - SEE PRODUCT STANDARD SPECIFICATIONS. ALTERNATIVE FINISHES MAY BE ACCEPTABLE, BUT MUST BE APPROVED IN WRITING BY IGES PRIOR TO USE.
- 2.2. BACKFILL SOILS
- IMPORTED, GRANULAR BORROW OR APPROVED NATIVE GRANULAR SOILS SCREENED FOR REMOVAL OF DEBRIS OR IMPORTED 2.2.1. MATERIALS COMPLYING WITH THE FOLLOWING CRITERIA:
- GRANULAR MATERIALS CONTAINING LESS THAN 25% FINES 2.2.1.1.
- MAXIMUM NOMINAL PARTICLE SIZE OF 4 INCHES 2.2.1.2.
- 2.2.1.3. PLOF 6 OR LESS
- 2.2.1.4. PH GREATER THAN 3 BUT LESS THAN 9
- 2.2.1.5. REASONABLY FREE FROM ORGANIC, OR OTHER DELETERIOUS MATERIALS
- 2.2.1.6. MINIMUM EFFECTIVE FRICTION ANGLE OF 34 DEGREES
- 2.3. BASKET FILL
- 2.3.1. 4- TO 8-INCH CLEAN AGGREGATE.
- 2.3.2. MINIMUM IN-PLACE UNIT WEIGHT OF 120 POUNDS PER CUBIC FOOT
- 233 MATERIAL CONTAINING LESS THEN 5% FINES.
- 3. GABION RETAINING WALL INSTALLATION
- 3.1 FIELD-VERIFY PROPOSED FINISHED GRADE AT BOTTOM OF WALL TO PROVIDE A MINIMUM WALL EMBEDMENT OF 12 INCHES AS SHOWN ON THE ELEVATION AND SECTION DRAWINGS.
- GRADE AND COMPACT FOUNDATION SUBGRADE SOILS FOR THE FULL LENGTH OF THE GABION RETAINING WALL PRIOR TO 3.2 PLACEMENT OF THE GABION BASKETS AND ANY BACKFILL
- REMOVE AND REPLACE ANY FOUNDATION SOILS FOUND TO BE UNSUITABLE OR UNSTABLE WITH APPROVED FILL MEETING THE 3.3 CRITERIA OUTLINED IN NOTE 2.2 ABOVE.
- INSTALL ALL GABION BASKETS IN ACCORDANCE WITH HILFIKER GABION GUIDELINES. 3.4
- SET GABION INFILL WITHIN 12 INCHES OF THE WALL FACE BY HAND TO PREVENT GABION DEFORMATION. 3.5.
- 3.6. OFFSET SUCCESSIVE ROWS OF GABIONS AS SHOWN ON THE TYPICAL SECTION VIEW - SHEET NO 3.
- 3.7. ROW WIDTHS SHOWN ARE MINIMUM REQUIRED. ROWS MAY BE LENGTHENED TO FACILITATE CONSTRUCTION AS NEEDED.
- 3.8. SET AND CHECK THE FIRST ROW OF GABION UNITS FOR LEVEL AND ALIGNMENT.



PLACE WALL BACKFILL MATERIAL IN 12-INCH MAXIMUM LOOSE LIFTS AND COMPACTED TO A MINIMUM OF 95 PERCENT OF THE 39 MAXIMUM DRY DENSITY (ASTM D-1557).

- 391 PERFORM DENSITY TESTING OF THE BACKFILL SOILS AT 50-FOOT INTERVALS MEASURED ALONG WALL FACE.
- 3.9.1.1. PERFORM 2 TESTS PER LIFT, MINIMUM.
- 3.9.2. GABIONS
- 3.9.3. MINIMUM OF 95 PERCENT OF ASTM D-1557.
- 4. CONSTRUCTION OBSERVATION
- 4.1. DESIGN ENGINEER, IGES, INC. MUST PERFORM PERIODIC CONSTRUCTION OBSERVATIONS.
- 4.1.1. ALL RESPONSIBILITY FOR THE RETAINING WALL
- 4.2. PROCEED WITH GABION WALL OBSERVATIONS AS FOLLOWS:
- 4.2.1. OBSERVE THE EXCAVATION OF THE FOUNDATION SOILS
- 4.2.1.1. ASSESS THE SUITABILITY OF THE FOUNDATIONS SOILS.
- 4.2.1.1.1.
- 4.2.2. OBSERVE THE INSTALLATION OF EACH COURSE OF RETAINING WALL GABION.
- 4.2.2.1. ASSESS MINIMUM EMBEDMENT REQUIREMENTS. 4.2.2.2. ASSESS DEPTH OF INFILL FACING ZONE.
- 4.2.2.3. ABOVE
- 4.2.3. OBSERVE THE INSTALLATION OF ANY RETAINED BACKFILL.
- 4.2.3.1.
- 4.2.3.2. OBSERVE FILL PLACEMENT AND COMPACTION.
- 4.2.3.2.1. ASSESS LOOSE LIFT THICKNESS.

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- 4.2.3.2.2. OBSERVE OPERATION OF COMPACTION EQUIPMENT. 423221
  - OF RETAINING WALL BASKETS.
- 4.2.3.3.
- OBSERVE THE COMPLETED RETAINING WALL SYSTEM. 4.2.4.
- 4241 ASSESS THE FINISHED RETAINING WALL HEIGHT AND BATTER.
- 4.2.4.2.
- 4.2.4.3. ASSESS SUITABILITY OF EROSION CONTROL MEASURES INSTALLED ABOVE THE RETAINING WALL

REVISIONS

IF APPLICABLE USE ONLY SMALL, WALK-BEHIND TYPE COMPACTION EQUIPMENT WITHIN 1 FOOT OF THE BACK OF THE

IF ANY LOCATIONS EXIST WHERE THE RETAINING WALLS WILL NOT BE PLACED UPON NATIVE SOILS, COMPACT THE FILL TO A

TO FULFILL ANY APPLICABLE CITY, COUNTY AND/OR STATE AGENCY REQUIREMENTS, AND TO PROTECT THE CONTRACTOR AND

IF IGES, INC. DOES NOT OBSERVE THE RETAINING WALL DURING CONSTRUCTION, A FINAL LETTER REGARDING COMPLIANCE OF THE WALL CONSTRUCTION WITH THE DESIGN CRITERIA AND RECOMMENDATIONS CANNOT BE PROVIDED. IF IGES, INC. DOES NOT PERFORM THE PERIODIC CONSTRUCTION OBSERVATIONS OUTLINED BELOW, THE WALL CONTRACTOR/OWNER ASSUMES

PROVIDE WRITTEN NOTICE OF ACCEPTANCE PRIOR TO PROCEEDING WITH RETAINING WALL CONSTRUCTION.

ASSESS GABION PLACEMENT AND POSITIONING FOR COMPLIANCE WITH THE REQUIREMENTS SET FORTH IN THE SECTIONS

EVALUATE THAT THE BACKFILL MATERIALS MEET THE REQUIREMENTS SET FORTH IN SECTION 2.2. ABOVE.

NOTE OUT-OF-TOLERANCE BEHAVIOR REGARDING MINIMUM ALLOWABLE OPERATING DISTANCE BEHIND BACK

ASSESS COMPACTED BACKFILL MATERIAL FOR COMPLIANCE WITH REQUIREMENTS SET FORTH IN SECTION 3.9. ABOVE.

EVALUATE THAT BACKSLOPE AND TOESLOPE GRADING CONDITIONS DO NOT EXCEED DESIGN GEOMETRY TOLERANCES.

GN PACKAGE	DESIGNED BY: TBL	9-25-2017	PLOT SC	CALE
MOUNTAIN RESORT	DRAWN BY: TBL	9-25-2017	1=1	
MIT PASS	CHECKED BY: DAG	9-27-2017	DWG SC	CALE
Y. UTAH	APPROVED BY: DAG	9-27-2017	NTS	S
CATIONS & NOTES	IGES PROJECT NO.	SHEET NO.	5	REV.
CATIONS & NOTES	02132-003	~	5	N/A

## GABION DESIGN PACKAGE LOT 39 SUMMIT POWDER MOUNTAIN RESORT 8365 EAST SUMMIT PASS WEBER COUNTY, UTAH

RETAINING WALL GEOMETRY AND LOADING CONDITIONS			
WALL	MAXIMUM HEIGHT (FT)	BACKSLOPE CONDITIONS	SURCHARGE LOADING
1	9	RELATIVELY FLAT	UPPER TIER
2	12	RELATIVELY FLAT	DRIVEWAY

RETAINING WALL ANALYSIS USED IN DESIGN		
ANALYSIS DESIGN REFERENCES/SOFTWARE		
EXTERNAL STABILITY	NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA) METHODOLOGY	
GLOBAL STABILITY	SLIDE: ROCSCIENCE, INC., 1998-2017, VERSION 7.027, BUILD DATE AUGUST 15, 2017	

MATERIAL ESTIMATED QUANTITIES				
GABION BASKETS GABION FILL QUANTITIES VOLUME				
H3.0-FT	GABION BASKET: 3-FT DEEP, 6-FT WIDE, 1.5-FT HIGH	5 UNITS (45 FT <sup>2</sup> )	2 YD <sup>3</sup>	
3.0-FT	GABION BASKET: 3-FT DEEP, 6-FT WIDE, 3-FT HIGH	16 UNITS (288 FT <sup>2</sup> )	11 YD <sup>3</sup>	
6.0-FT	GABION BASKET: 6-FT DEEP, 6-FT WIDE, 3-FT HIGH	21 UNITS (378 FT <sup>2</sup> )	28 YD <sup>3</sup>	
9.0-FT GABION BASKET: 9-FT DEEP, 6-FT WIDE, 3-FT HIGH		24 UNITS (432 FT <sup>2</sup> )	48 YD <sup>3</sup>	
	TOTAL         66 UNITS (1,188 FT <sup>2</sup> )         88 YD <sup>3</sup>			

NOTES:

1. MAY USE 3-FT WIDE BASKETS INSTEAD OF 6-FT WIDE BASKETS.

THESE DOCUMENTS ARE INSTRUMENTS OF SERVICE AND SHALL REMAIN THE INTELLECTUAL PROPERTY OF IGES, INC. NO USE OR RE-USE OF THESE DOCUMENTS SHALL BE PERMITTED IN PART OR IN TOTAL UNLESS EXPRESSLY AUTHORIZED IN WRITING BY IGES, INC.

ASSUMED SOIL CONDITIONS USED IN DESIGN				
EARTH MATERIALS	FRICTION ANGLE COHESION UNIT WEIGH			
RETAINED SOIL	34°	150 PSF	120 PCF	
FOUNDATION SOIL	34°	150 PSF	120 PCF	

SOURCES & NOTES:

GEOTECHNICAL INVESTIGATION REPORT, LOT 39R OF POWDER MOUNTAIN 1. RESORT, 8634 EAST SUMMIT PASS, WEBER COUNTY, UTAH, IGES PROJECT NO. 02052-001, DATED JUNE 3, 2015.

2. COHESION USED DURING GLOBAL STABILITY ANALYSES ONLY.

SEISMIC PARAMETERS USED IN RETAINING WALL DESIGN					
SEISMIC CRITERIA	GLOBAL STABILITY		EXTERNAL STABILITY		
	MCE PGA	kh	DESIGN PGA	kh	
2% IN 50 YEARS	0.33g	0.16g (GLOBAL)	0.22g	0.09g (EXTERNAL)	

SOURCES & NOTES:

- 1. GEOTECHNICAL INVESTIGATION REPORT, LOT 39R OF POWDER MOUNTAIN RESORT, 8634 EAST SUMMIT PASS, WEBER COUNTY, UTAH, IGES PROJECT NO. 02052-001, DATED JUNE 3, 2015.
- 2. A MAXIMUM ALLOWABLE SEISMIC DISPLACEMENT THRESHOLD OF 2.2 INCHES (10\*PGA) WAS USED TO REDUCE THE HORIZTONTAL SEISMIC ACCELERATION COEFFICIENT IN ACCORDANCE WITH NCMA 3RD EDITION METHODOLOGY.
- ONE-HALF OF THE MCE PGA WAS USED TO MODEL THE 3. HORIZONTAL SEISMIC ACCELERATION FOR GLOBAL STABILITY ANALYSES ( $k_h = 0.16g$ ).



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REVISIONS

REV

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MOUNTAIN RESORT	DRAWN BY: TBL	9-25-2017	1=1	
MIT PASS	CHECKED BY: DAG	9-27-2017	DWG SC	CALE
Y. UTAH	APPROVED BY: DAG	9-27-2017	NTS	5
-,	IGES PROJECT NO.	SHEET NO.	6	REV.
TERIA	02132-003	STILLET TOOL	0	N/A

# Section 2

PROJECT NO.: 02132-003 DATE: 9/25/2017

Gabion Geometry & Soil Data:

$H_{total} =$	9	ft	Total Height of Gabion Wall
$H_R =$	8	ft	Exposed Height of Gabion Wall
$\phi_s =$	34	deg	Soil Friction Angle - Effective
$c_s =$	0	psf	Cohesion Intercept of soil
$\gamma_s =$	120	pcf	Unit weight of the soil
$\gamma_u =$	140	pcf	Unit weight of the infill rock
$\varphi_r =$	35	deg	Infill Rock Friction Angle
δ =	22.7	deg	Interface Friction Angle
ψ=	0.0	deg	Back Cut Inclination
μ=	0.70		Frictional Component
K <sub>A</sub> =	0.272		Active Earth Pressure Coefficient

## Surcharge:

### Dead Load Uniform Surcharge: Live Load Uniform Surcharge: 185 $q_{sd} =$ psf (Dead Load Surcharge) $F_{sd} =$ 453.4 lbf/ft (Horizontal Surcharge Load) $y_{sd} =$ 4.5 ft (Surcharge load centroid)

## **Factor of Safety against Bearing Capacity:**

3

e <sub>w</sub> =	0.000	$q_{ac} =$	1,026	psf	$e_{c,s} = 1.234$	<b>FS</b> <sub>BC</sub>	19.8
$e_c =$	0.734	$q_{ult} =$	20,351	psf	$q_{ac,s} = 1,042$	FS <sub>BC,s</sub>	19.5

## # Gabions =

Gabion No.	$W_{u}(ft)$	$\Delta_{\rm u}$ (in)	H <sub>u</sub> (ft)	H <sub>wall</sub> (ft)	$\Sigma W_i$	$\Sigma W_i^* x_i$	P <sub>H</sub>	P <sub>H,s</sub>	R <sub>sc</sub>	R <sub>sc,s</sub>	M <sub>o</sub>	M <sub>o,s</sub>	M <sub>r</sub>	M <sub>r,s</sub>	FS <sub>SL</sub>	FSOT	FS <sub>SL,S</sub>	FS <sub>OT,S</sub>
1	9.0	0.0	3.0	9.0	7,560	26,460	1,640	2,480	3,893	3,922	5,547	9,327	32,623	33,179	2.5	5.9	1.7	3.6
2	6.0	0.0	3.0	6.0	3,780	9,450	822	1,234	2,802	2,821	1,922	3,158	11,509	11,674	3.4	6.0	2.3	3.7
3	3.0	0.0	3.0	3.0	1,260	1,890	275	407	923	928	345	543	2,235	2,255	3.4	6.5	2.3	4.2
4	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
5	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
6	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
7	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
8	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A

9.0 Total Estimated Height of Gabion Retaining Wall

(See Design Manual for Segmental Retaining Walls, National Concrete Masonry Association [NCMA] 3rd Edition for terms and equations of wall design)



Failure Mechanism	FS Required	FS Obtained	ОК
External Sliding	1.5	2.5	OK
External Overturning	2.0	5.9	OK
Individual Overturning	2.0	6.0	OK
Individual Sliding	1.5	3.4	OK
Bearing Capacity	2.0	19.8	OK
Seismic Overturning	1.5	3.6	OK
Seismic Sliding	1.1	1.7	OK
Seismic Bearing Capacity	1.5	19.5	OK

$q_{sl} =$	0	psf	(Dead Load Surcharge)
$F_{sl} =$	0.0	lbf/ft	(Horizontal Surcharge Load)
$y_{sl} =$	0	ft	(Surcharge load centroid)

0

5.23

0.338

- 1				
	$q_{sl} =$	0	psf	(Dead Load Surcharge)
	$F_{sl} =$	0.0	lbf/ft	(Horizontal Surcharge Load)
	<b>v</b> .=	0	ft	(Surcharge load centroid)

 $k_v =$ 

 $\theta =$ 

 $K_{AE} =$ 

SECTION: Wall 1 - 9 FT

SURCHARGE: Upper Tier

**Slope Geometry:** 

Backslope:

Soil Cut Angle:

A =0.220 Peak Ground acceleration (2% in 50 years) d = 2.2 in (Allowable Displacement) 0.092  $k_h =$ Use 1/2 of A? N

Seismic Earth Pressure Coefficient:

 $\beta_{con} =$ 

α=

6.0

0.0

(If "N" then use displacement-factored k<sub>h</sub>)

deg

deg

Eqv. Backslope Angle

Soil Cut Angle

PROJECT NO.: 02132-003 DATE: 9/25/2017

Gabion Geometry & Soil Data:

$H_{total} =$	6	ft	Total Height of Gabion Wall
$H_R =$	5	ft	Exposed Height of Gabion Wall
$\phi_s =$	34	deg	Soil Friction Angle - Effective
$c_s =$	0	psf	Cohesion Intercept of soil
$\gamma_s =$	120	pcf	Unit weight of the soil
$\gamma_{\rm u} =$	140	pcf	Unit weight of the infill rock
$\phi_r =$	35	deg	Infill Rock Friction Angle
δ =	22.7	deg	Interface Friction Angle
ψ=	0.0	deg	Back Cut Inclination
μ=	0.70		Frictional Component
K <sub>A</sub> =	0.272		Active Earth Pressure Coefficient

## Surcharge:

### Dead Load Uniform Surcharge: Live Load Uniform Surcharge: 277 $q_{sd} =$ psf (Dead Load Surcharge) $F_{sd} =$ 452.6 lbf/ft (Horizontal Surcharge Load) 3 $y_{sd} =$ ft (Surcharge load centroid)

## Factor of Safety against Bearing Capacity:

2

$e_w =$	0.000	$q_{ac} =$	794	psf	$e_{c,s} = 0.945$	<b>FS</b> <sub>BC</sub>	18.6
$e_c =$	0.619	$q_{ult} =$	14,745	psf	$q_{ac,s} = 805$	FS <sub>BC,s</sub>	18.3

SECTION: Wall 1 - 6 FT

**SURCHARGE:** Upper Tier

**Slope Geometry:** 

Backslope:

A =

d =

 $k_h =$ 

 $k_v =$ 

 $\theta =$ 

 $K_{AE} =$ 

Soil Cut Angle:

## # Gabions =

Gabion No.	$W_{u}(ft)$	$\Delta_{\rm u}$ (in)	H <sub>u</sub> (ft)	H <sub>wall</sub> (ft)	$\Sigma W_i$	$\Sigma W_i^* x_i$	$P_{\rm H}$	P <sub>H,s</sub>	R <sub>sc</sub>	R <sub>sc,s</sub>	M <sub>o</sub>	M <sub>o,s</sub>	M <sub>r</sub>	M <sub>r,s</sub>	FS <sub>SL</sub>	FSOT	FS <sub>SL,S</sub>	FS <sub>OT,S</sub>
1	6.0	0.0	3.0	6.0	3,780	9,450	960	1,372	1,974	1,987	2,339	3,574	11,857	12,021	2.3	5.1	1.6	3.4
2	3.0	0.0	3.0	3.0	1,260	1,890	345	476	919	924	449	647	2,322	2,342	2.7	5.2	1.9	3.6
3	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
4	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
5	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
6	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
7	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
8	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A

6.0 Total Estimated Height of Gabion Retaining Wall

(See Design Manual for Segmental Retaining Walls, National Concrete Masonry Association [NCMA] 3rd Edition for terms and equations of wall design)



Failure Mechanism	FS Required	FS Obtained	ОК
External Sliding	1.5	2.3	OK
External Overturning	2.0	5.1	OK
Individual Overturning	2.0	5.2	OK
Individual Sliding	1.5	2.7	OK
Bearing Capacity	2.0	18.6	OK
Seismic Overturning	1.5	3.4	OK
Seismic Sliding	1.1	1.6	OK
Seismic Bearing Capacity	1.5	18.3	OK

$q_{sl} =$	0	psf	(Dead Load Surcharge)
$F_{sl} =$	0.0	lbf/ft	(Horizontal Surcharge Load)
y <sub>sl</sub> =	0	ft	(Surcharge load centroid)

 $\beta_{con} =$ 

α=

Seismic Earth Pressure Coefficient:

2.2

0.092

5.23

0.338

0

6.0

0.0

0.220 Peak Ground acceleration (2% in 50 years)

in (Allowable Displacement)

Use 1/2 of A? N

(If "N" then use displacement-factored kh)

deg

deg

Eqv. Backslope Angle

Soil Cut Angle

$q_{sl} =$	0	psf	(Dead Load Surcharge)
$F_{sl} =$	0.0	lbf/ft	(Horizontal Surcharge Load)
V.1 =	0	ft	(Surcharge load centroid)

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## Gabion Geometry & Soil Data:

$H_{total} =$	12	ft	Total Height of Gabion Wall
$H_R =$	11	ft	Exposed Height of Gabion Wall
$\phi_s =$	34	deg	Soil Friction Angle - Effective
$c_s =$	0	psf	Cohesion Intercept of soil
$\gamma_s =$	120	pcf	Unit weight of the soil
$\gamma_{\rm u} =$	140	pcf	Unit weight of the infill rock
$\varphi_{\rm r} =$	35	deg	Infill Rock Friction Angle
δ =	22.7	deg	Interface Friction Angle
ψ=	0.0	deg	Back Cut Inclination
μ=	0.70		Frictional Component
K <sub>A</sub> =	0.254		Active Earth Pressure Coefficient

## Surcharge:

### Dead Load Uniform Surcharge: 200 $q_{sd} =$ psf (Dead Load Surcharge) $F_{sd} =$ 610.2 lbf/ft (Horizontal Surcharge Load) $y_{sd} =$ 6 ft (Surcharge load centroid)

## Factor of Safety against Bearing Capacity:

4

$e_w =$	0.000	$q_{ac} =$	1,747	psf	$e_{c,s} = 1.683$	FS <sub>BC</sub>	11.7
$e_c =$	1.162	$q_{ult} =$	20,351	psf	$q_{ac,s} = 1,774$	FS <sub>BC,s</sub>	11.5

## # Gabions =

Gabion No.	$W_{u}(ft)$	$\Delta_{\rm u}$ (in)	H <sub>u</sub> (ft)	H <sub>wall</sub> (ft)	$\Sigma W_i$	$\Sigma W_i^* x_i$	P <sub>H</sub>	P <sub>H,s</sub>	R <sub>sc</sub>	R <sub>sc,s</sub>	Mo	M <sub>o,s</sub>	M <sub>r</sub>	M <sub>r,s</sub>	FS <sub>SL</sub>	FSOT	FS <sub>SL,S</sub>	FS <sub>OT,S</sub>
1	9.0	0.0	3.0	12.0	11,340	43,470	2,872	3,856	5,865	5,910	13,176	19,082	53,206	54,061	2.1	4.0	1.6	2.8
2	9.0	0.0	3.0	9.0	7,560	26,460	1,774	2,383	5,621	5,659	6,271	9,012	32,333	32,814	3.2	5.2	2.4	3.6
3	6.0	0.0	3.0	6.0	3,780	7,560	929	1,191	2,797	2,813	2,281	3,067	9,535	9,678	3.0	4.2	2.4	3.2
4	3.0	0.0	3.0	3.0	1,260	1,890	338	397	921	925	443	532	2,225	2,243	2.7	5.0	2.3	4.2
5	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
6	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
7	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
8	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A

12.0 Total Estimated Height of Gabion Retaining Wall

(See Design Manual for Segmental Retaining Walls, National Concrete Masonry Association [NCMA] 3rd Edition for terms and equations of wall design)



Failure Mechanism	FS Required	FS Obtained	ОК
External Sliding	1.5	2.1	OK
External Overturning	2.0	4.0	OK
Individual Overturning	2.0	4.2	OK
Individual Sliding	1.5	2.7	OK
Bearing Capacity	2.0	11.7	OK
Seismic Overturning	1.5	2.8	OK
Seismic Sliding	1.1	1.6	OK
Seismic Bearing Capacity	1.5	11.5	OK

## Live Load Uniform Surcharge:

0.311

$q_{sl} =$	100	psf	(Dead Load Surcharge)
$F_{s1} =$	305.1	lbf/ft	(Horizontal Surcharge Load)
$y_{sl} =$	6	ft	(Surcharge load centroid)

 $\beta_{con} =$ 

α=

Seismic Earth Pressure Coefficient:

0.0

0.0

0.220 Peak Ground acceleration (2% in 50 years)

in (Allowable Displacement)

Use 1/2 of A? N

deg

deg

Eqv. Backslope Angle

Soil Cut Angle

q <sub>sl</sub> =	100	psf	(Dead Load Surcharge)
$F_{s1} =$	305.1	lbf/ft	(Horizontal Surcharge Load)
v. =	6	ft	(Surcharge load centroid)

2.2 0.092

A =

 $K_{AE} =$ 

 $k_h =$ 

## d =

 $k_v =$ 0 (If "N" then use displacement-factored k<sub>h</sub>)  $\theta =$ 5.23

SECTION: Wall 2 - 12 FT

SURCHARGE: Driveway

**Slope Geometry:** 

Backslope:

Soil Cut Angle:

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DATE: 9/25/2017

## Gabion Geometry & Soil Data:

$H_{total} =$	9	ft	Total Height of Gabion Wall
$H_R =$	8	ft	Exposed Height of Gabion Wall
$\varphi_s =$	34	deg	Soil Friction Angle - Effective
$c_s =$	0	psf	Cohesion Intercept of soil
$\gamma_s =$	120	pcf	Unit weight of the soil
$\gamma_u =$	140	pcf	Unit weight of the infill rock
$\varphi_r =$	35	deg	Infill Rock Friction Angle
δ =	22.7	deg	Interface Friction Angle
ψ=	0.0	deg	Back Cut Inclination
μ=	0.70		Frictional Component
K <sub>A</sub> =	0.254		Active Earth Pressure Coefficient

## Surcharge:

 $y_{sd} =$ 

# $\begin{array}{c|c} \underline{Dead\ Load\ Uniform\ Surcharge:}} & \underline{Live\ Load\ Uniform\ Surcharge:}\\ \hline q_{sd} = & \underline{200} & psf & (Dead\ Load\ Surcharge) & q_{sl} = & \underline{100} & psf & (Dead\ Load\ Surcharge) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load) & F_{sl} = & \underline{228.8} & lbf/ft & (Horizontal\ Surcharge\ Load\ Surcharge\ Surcharge\ Load\ Surcharge\ Load\ Surcharge\ Surcharge$

(Surcharge load centroid)

ft

$q_{sl} =$	100	psf	(Dead Load Surcharge)
$F_{s1} =$	228.8	lbf/ft	(Horizontal Surcharge Load)
$y_{sl} =$	4.5	ft	(Surcharge load centroid)

 $\beta_{con} =$ 

α=

Seismic Earth Pressure Coefficient:

2.2

0.092

5.23

0.311

0

0.0

0.0

0.220 Peak Ground acceleration (2% in 50 years)

in (Allowable Displacement)

Use 1/2 of A? N

(If "N" then use displacement-factored k<sub>h</sub>)

deg

deg

Eqv. Backslope Angle

Soil Cut Angle

### Factor of Safety against Bearing Capacity:

4.5

3

$e_w =$	0.000	$q_{ac} =$	1,059	psf	$e_{c,s} = 1.192$	<b>FS</b> <sub>BC</sub>	19.2
$e_c =$	0.830	$q_{ult} =$	20,351	psf	$q_{ac,s} = 1,072$	FS <sub>BC,s</sub>	19.0

SECTION: Wall 2 - 9 FT

SURCHARGE: Driveway

**Slope Geometry:** 

Backslope:

A =

d =

 $k_h =$ 

 $k_v =$ 

 $\theta =$ 

 $K_{AE} =$ 

Soil Cut Angle:

## # Gabions =

Gabion No.	$W_{u}(ft)$	$\Delta_{\rm u}$ (in)	H <sub>u</sub> (ft)	H <sub>wall</sub> (ft)	$\Sigma W_i$	$\Sigma W_i^* x_i$	P <sub>H</sub>	P <sub>H,s</sub>	R <sub>sc</sub>	R <sub>sc,s</sub>	M <sub>o</sub>	M <sub>o,s</sub>	M <sub>r</sub>	M <sub>r,s</sub>	FS <sub>SL</sub>	FSOT	FS <sub>SL,S</sub>	FS <sub>OT,S</sub>
1	9.0	0.0	3.0	9.0	7,560	26,460	1,774	2,383	3,878	3,903	6,271	9,012	32,333	32,814	2.3	5.2	1.7	3.6
2	6.0	0.0	3.0	6.0	3,780	9,450	929	1,191	2,791	2,808	2,281	3,067	11,425	11,568	3.0	5.0	2.4	3.8
3	3.0	0.0	3.0	3.0	1,260	1,890	338	397	920	924	443	532	2,225	2,243	2.7	5.0	2.3	4.2
4	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
5	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
6	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
7	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
8	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A

9.0 Total Estimated Height of Gabion Retaining Wall

(See Design Manual for Segmental Retaining Walls, National Concrete Masonry Association [NCMA] 3rd Edition for terms and equations of wall design)



Failure Mechanism	FS Required	FS Obtained	ОК
External Sliding	1.5	2.3	OK
External Overturning	2.0	5.2	OK
Individual Overturning	2.0	5.0	OK
Individual Sliding	1.5	2.7	OK
Bearing Capacity	2.0	19.2	OK
Seismic Overturning	1.5	3.6	OK
Seismic Sliding	1.1	1.7	OK
Seismic Bearing Capacity	1.5	19.0	OK

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DATE: 9/25/2017 . . . . . ~

Gabion	Geometry	&	Soil	Data:

$H_{total} =$	6	ft	Total Height of Gabion Wall
$H_R =$	5	ft	Exposed Height of Gabion Wall
$\varphi_s =$	34	deg	Soil Friction Angle - Effective
$c_s =$	0	psf	Cohesion Intercept of soil
$\gamma_s =$	120	pcf	Unit weight of the soil
$\gamma_u =$	140	pcf	Unit weight of the infill rock
$\varphi_{\rm r} =$	35	deg	Infill Rock Friction Angle
δ =	22.7	deg	Interface Friction Angle
ψ=	0.0	deg	Back Cut Inclination
μ=	0.70		Frictional Component
K <sub>A</sub> =	0.254		Active Earth Pressure Coefficient

## Surcharge:

 $F_{sd} =$ 

 $y_{sd} =$ 

## Dead Load Uniform Surcharge: $q_{sd} =$

1 Uniform Surch	narge:		Live Load	Uniform	n Surcha	rge:
200	psf	(Dead Load Surcharge)	$q_{sl} =$	100	psf	(Dead Load Surcharge)
305.1	lbf/ft	(Horizontal Surcharge Load)	$F_{sl} =$	152.6	lbf/ft	(Horizontal Surcharge Load)
3	ft	(Surcharge load centroid)	$\mathbf{y}_{\mathrm{sl}} =$	3	ft	(Surcharge load centroid)

SECTION: Wall 2 - 6 FT

 $\beta_{con} =$ 

α=

Seismic Earth Pressure Coefficient:

2.2

0.092

5.23

0.311

0.0

0.0

0.220 Peak Ground acceleration (2% in 50 years)

0 (If "N" then use displacement-factored  $k_h$ )

in (Allowable Displacement)

Use 1/2 of A? N

deg

deg

Eqv. Backslope Angle

Soil Cut Angle

**SURCHARGE:** Driveway

**Slope Geometry:** 

Backslope:

A =

d =

 $k_h =$ 

 $k_v =$ 

 $\theta =$ 

 $K_{AE} =$ 

Soil Cut Angle:

## **Factor of Safety against Bearing Capacity:**

2

$e_w =$	0.000	$q_{ac} =$	787	psf	$e_{c,s} = 0.811$	<b>FS</b> <sub>BC</sub>	18.7
$e_c =$	0.603	$q_{ m ult} =$	14,745	psf	$q_{ac,s} = 796$	FS <sub>BC,s</sub>	18.5

## # Gabions =

Gabion No.	$W_{u}(ft)$	$\Delta_{\rm u}$ (in)	H <sub>u</sub> (ft)	H <sub>wall</sub> (ft)	$\Sigma W_i$	$\Sigma W_i^* x_i$	P <sub>H</sub>	P <sub>H,s</sub>	R <sub>sc</sub>	R <sub>sc,s</sub>	M <sub>o</sub>	M <sub>o,s</sub>	M <sub>r</sub>	M <sub>r,s</sub>	FS <sub>SL</sub>	FSOT	FS <sub>SL,S</sub>	FS <sub>OT,S</sub>
1	6.0	0.0	3.0	6.0	3,780	9,450	929	1,191	1,940	1,951	2,281	3,067	11,425	11,568	2.3	5.0	1.8	3.8
2	3.0	0.0	3.0	3.0	1,260	1,890	338	397	917	922	443	532	2,225	2,243	2.7	5.0	2.3	4.2
3	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
4	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
5	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
6	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
7	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A
8	0.0	0.0	0.0	N/A	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A

6.0 Total Estimated Height of Gabion Retaining Wall

(See Design Manual for Segmental Retaining Walls, National Concrete Masonry Association [NCMA] 3rd Edition for terms and equations of wall design)



Failure Mechanism	FS Required	FS Obtained	ОК
External Sliding	1.5	2.3	OK
External Overturning	2.0	5.0	OK
Individual Overturning	2.0	5.0	OK
Individual Sliding	1.5	2.7	OK
Bearing Capacity	2.0	18.7	OK
Seismic Overturning	1.5	3.8	OK
Seismic Sliding	1.1	1.8	OK
Seismic Bearing Capacity	1.5	18.5	OK

# Section 3

