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October 14, 2016

To: Carson Young
Solitude Builders
801-452-5020

Pg 1 of 1

Re: Door Installation in Existing Window Locations
Nordic Valley Ski Lodge
3567 Nordic Valley Way
Eden, Utah

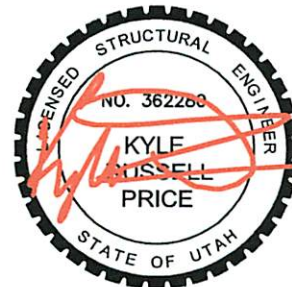
Carson,

On October 13th (yesterday) I visited the above ski lodge with you to observe conditions and recommend specifications to cut (2) door ways from existing windows into the foundation on the south side. I have attached (2) sketches, one with recommended cut and modifications per your request, and the other of the south lodge elevation showing the cut locations.

Also see calculations attached. I have included a 50 psf snow load and 100 psf floor live load in design. No other engineering for the lodge was provided other than the doors. Modifications follow the 2015 IBC chapter 34 and consequently the 2012 IEBC.

If you have any questions concerning this letter please feel free to contact me at anytime.
Sincerely,

Kyle Price, S.E.



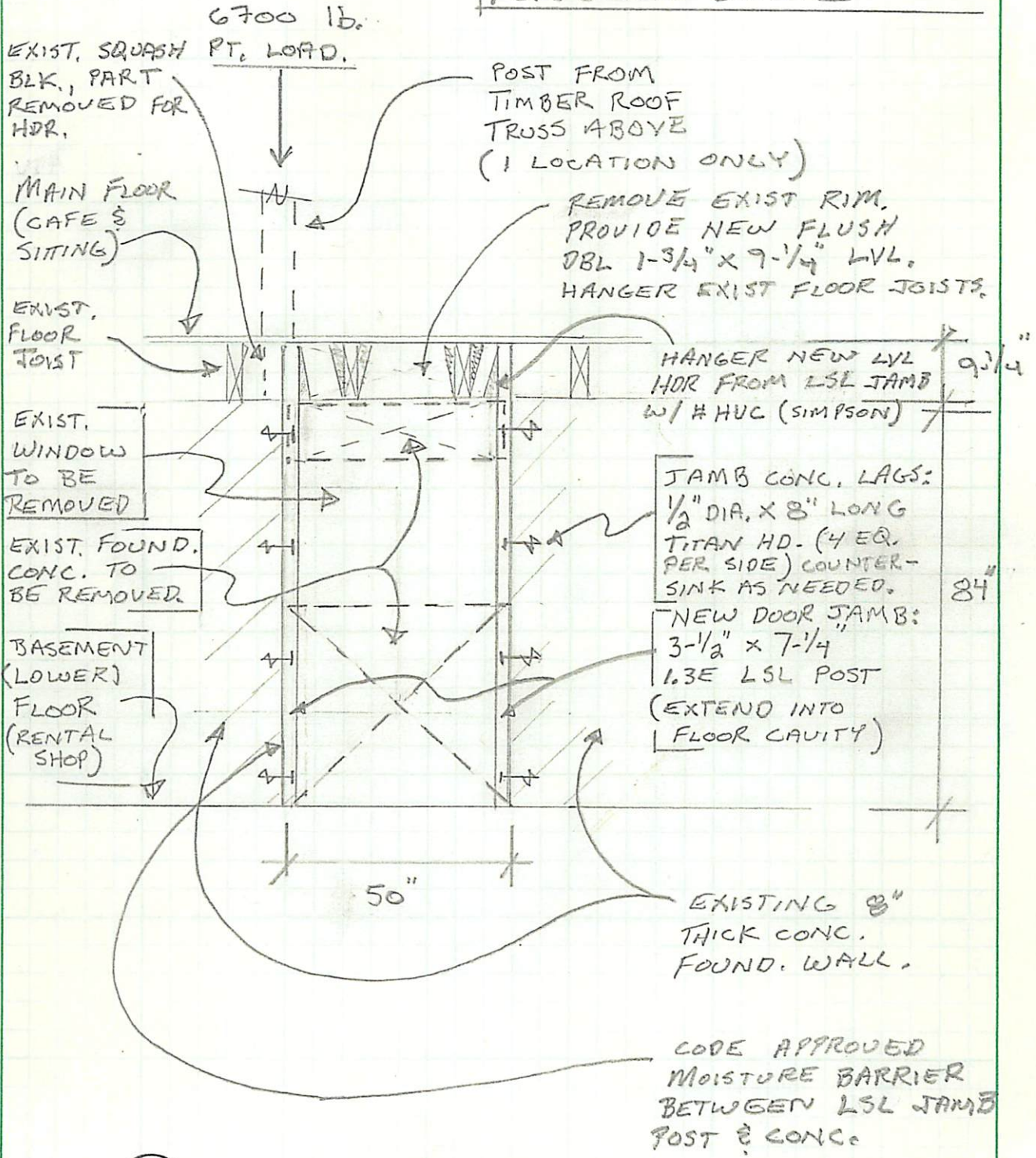
10/14/2016

10/13/16

NORDIC VALLEY
SKI LODGE

K. PRICE

FOUNDATION REMOVAL FOR DOOR DETAIL



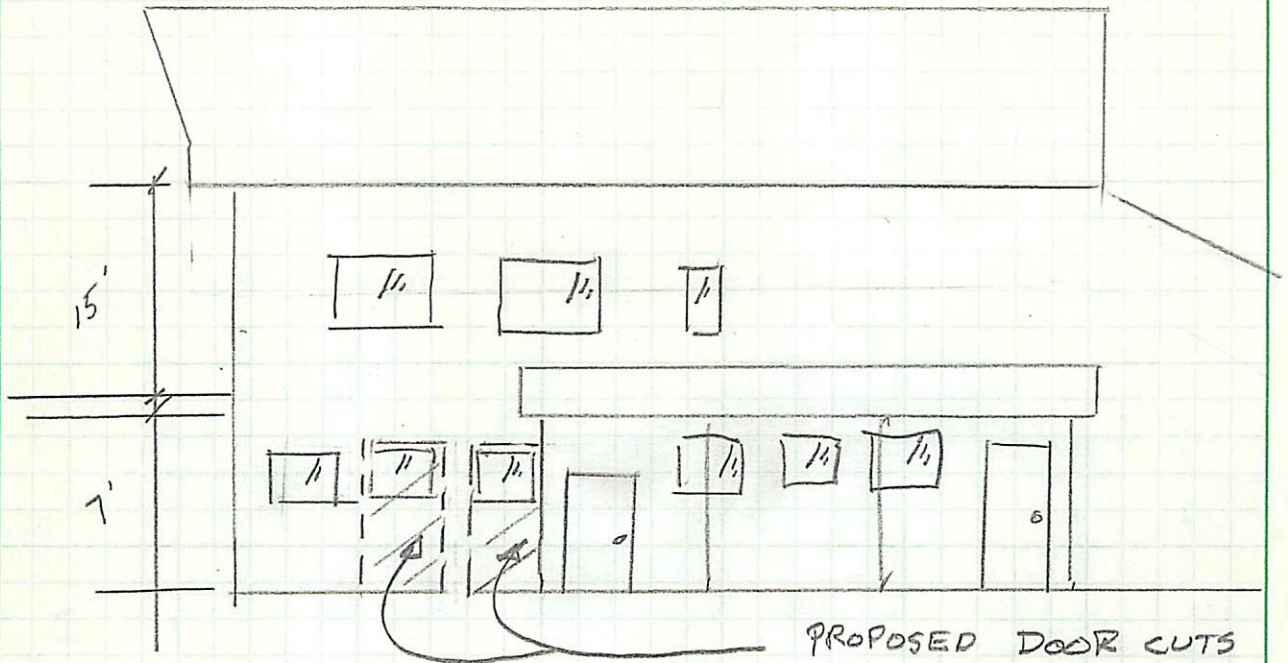
(A) INTERIOR ELEVATION
(2 DOORS TYP.)
NOT TO SCALE

10/14/16

SOLITUDE BLOBS

K. PRICE

NORDIC SKI LODGE



ⓑ ELEVATION SKETCH
SOUTH SIDE

Project: Solitude Nordic Lodge Door Mod
Design: K. Price
Date: 10/14/16

Project No.:

Sheet: of

DESIGN CRITERIA

Structure Type: Risk Category II, Light Wood Framed, Concrete Foundation

Design Codes: 2015 IBC, 2012 IEBC

Dead Loads:

20 psf for Roof Structure
10 psf for Walls (Siding, Stucco)
100 psf for Concrete Foundation

Live Loads:

20 psf for Roof Structure
100 psf for Floors

Snow Loads:

Pg: 70 Ce: 1 Ct: 1 I: 1
Cs: 1

$P_s \Rightarrow (P_g * C_s * C_e * C_t * I * 0.7)$

$P_s^* = 50$ psf

Seismic Loads: No Seismic Design provided other than out of plain loading for Jamb Posts.
No Engineering provided for any other portions of Lodge

Wind Loads: No Wind Design provided other than out of plain loading for Jamb Posts.

Exposure: C Risk Category: II
Wind Speed (3 sec. Gust): 120 mph

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Project No.:

Sheet: of

Deflection Criteria:

	(TL)		(LL)	
L/	240	L/	360	for: Roof Structure
L/	240	L/	480	for: Floor Structure
L/		L/	240	for: Exterior Walls
L/		L/		for:
L/		L/		for:

FOUNDATION CRITERIA

Soil Report: Not Available

By: Not Available

Date of Report: Not Available

Proj No. of Report: Not Available

Foundation Type: Concrete Spread Footing

Bearing Pressure: $Q_a = 1500$ psf
(Assumed)

Minium Depth: See Plans
Below: Exterior Finished Grade

Passive Pressure: $Y_p = 300$ pcf
(Assumed)

Coeff. of Friction: 0.4 alone 0.3 with passive

Active Pressure: $Y_a = 35$ pcf
(Assumed)

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Project No.:
Sheet: of

MATERIAL SPECIFICATIONS FOR REINFORCING STEEL, CONCRETE AND MASONRY

Reinforcing Steel: ASTM A615, Grade 60
ASTM A706, Grade 60 Weldable Rebar

Welded Wire Fabric: ASTM A185

Concrete Strengths: (Strength)

Footings:	3000	psi
Grade Beams:	3500	psi
Piles:	n/a	psi
Caissons:	n/a	psi
Slabs on Grade:	3500	psi
Structural Slabs:	3500	psi
Columns:	n/a	psi
Walls:	3500	psi

	(Strength)		(Density)	
Topping over Steel Deck:	3000	psi	150	psf
Topping over Plywood:				
Lightweight:	n/a	psi	n/a	psf
Cellular:	n/a	psi	n/a	psf

Concrete Masonry:

Units: ASTM C90 Medium Weight, Grade N-1

Mortar: Type "S" conforming to IBC Table 2103.7

Grout: Compress. Strength @ 28 days: 1800 psi

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Project No.:

Sheet: of

MATERIAL SPECIFICATIONS FOR WOOD FRAMING

Sawn Lumber: Douglas Fir Larch (North)

2 x 4 studs up to 8' 0" long:	Stud Grade
2 x 4 studs over 8' 0" long:	Stud Grade
Other Studs:	Stud Grade
Posts:	Grade #1
Joists:	Grade #2
Beams:	Grade #1
Headers:	Grade #2
Subpurlins:	Grade #1
Purlins:	Grade #1

Sheathing: APA Rated Sheathing

Roof:	Exposure:	I	Structural I	No
Floor:	Exposure:	I	Structural I	No
Shearwalls:	Exposure:	I	Structural I	No
	Exposure:		Structural	

Glued Laminated Beams (GLB): (All laminations Douglas Fir Larch unless noted otherwise)

Simple Spans:	24F-V4
Continuous:	24F-V8

Framing Hardware: Simpson Strong-Tie Connectors

Structural Nails: Common Wire Type or Galvanized Box

Bolts in Wood: ASTM A307 or better

Prefabricated Wood Joists: RE: Plan

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Project No.:

Sheet: of

Bending Capacities of Douglas Fir Larch (North):

2 X 10's					
Headers			Joists		
Snow Loads	1075	psi	Snow Loads	1237	psi
Normal Loads	935	psi	Normal Loads	1075	psi
2 X 12's					
Headers			Joists		
Snow Loads	978	psi	Snow Loads	1124	psi
Normal Loads	850	psi	Normal Loads	978	psi
Glu Laminated Members					
24F-V4, 24F-V8					
Snow Loads	2760	psi			
Normal Loads	2400	psi			

Project: Solitude Nordic Lodge Door Mod
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Date:

Project No.:

Sheet: of

Snow Load Calculations

Codes: 2015 IBC 1607, State Amendment, ASCE 7 10

Ground Snow Load, P_g

State Amendment R156-56-704

County: *Weber*

A : 5380 ft.

S : 63 psf/100 ft.

Po: 43 psf/100 ft.

Ao: 4.5 ft./1000

$$P_g = 1.0 \cdot S \cdot (A - A_o)^{0.5}$$

$$P_g = 70 \text{ psf}$$

Roof Snow Load, P_s (Sloped), P_f (Flat)

ASCE 7

Slope: 18 degrees

P_g : 70 psf

C_e : 1

C_t : 1

I : 1

C_s : 1

$$P_f = 0.7 \cdot C_e \cdot C_t \cdot I \cdot P_g$$

$$P_f = 49 \text{ psf}$$

$$P_s = C_e \cdot C_t \cdot I \cdot P_g \cdot C_s$$

$$P_s = 49 \text{ psf}$$

Design Roof Balanced Snow Load 50 psf

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SHEET: of

**Column Calculations W/ Bending
 2012 NDS**

COLUMN DOOR JAMB

Input	Results	COLUMN	DOOR JAMB
Axial			
$F_c = $ 1835.00 <i>psi</i>			
$C_d = $ 1.00			
$C_m = $ 1.00	$F'_c = 1835.00 \text{ psi}$		
$C_t = $ 1.00	$(C_d \cdot C_m \cdot C_t \cdot C_f \cdot C_i \cdot C_p)$		
$C_F = $ 1.00 <i>(built up col)</i>			
$C_i = $ 1.00	$C_p = 0.75$		
	$((1+(F_{ce}/F_c))/(2 \cdot C) - (((1+(F_{ce}/F_c))/(2 \cdot C))^2 - ((F_{ce}/F_c)/c))^{.5})$		
$load = $ 6,700 <i>lbs (max)</i>			
$Area = $ 21.75 <i>in²</i>	$F_{ce} = 2224 \text{ psi}$		
	$(K_{ce} \cdot E') / (L_e/d)^2$		
$K_{ce} = $ 0.30			
$E' = $ 1,300,000 <i>psi</i>	1382 <i>psi</i>	Design Vertical Load	
$L = $ 96.0 <i>in</i>	308 <i>psi</i>		
$K = $ 1.0 <i>in</i>		Roof	ASD Factor
$L_e = $ 96.0 <i>in</i>	<i>check</i> OK	Trib Width	5
$d = $ 7.25 <i>in</i>		Trib Length	20
$b = $ 3.00 <i>in</i>		Trib Area	100
$c = $ 0.80	$F'_b = 1700$	SL	50
	153	DL	20
		Total Roof	5750
		Floor	
		Trib Width	5
		Trib Length	2
		Trib Area	10
		LL	100
		DL	20
		Total Roof	950
		Total Factored PL	6700
Bending			
$F_b = $ 1700.00 <i>psi</i>	<i>tress Ratio</i> 0.15		
$C_D = $ 1.00	<i>check</i> OK		
$C_L = $ 1.00			
$C_v = $ 1.00			
$C_{fu} = $ 1.00			
$C_r = $ 1.00			
$C_i = $ 1.00			
1.00			
$load = $ 42 <i>plf</i>			
$S_x = $ 26.3 <i>in³</i>			

Provide **1 LSL 1.3E** 3-1/2" x 7-1/4"
 Maximum Height: 8.0 ft
 Weak Axis Braced at 2.0 ft

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Sheet of

BEAM #1, HDR / BEAM

INPUT		LOADING			LL	DL	LOAD DIST.	DEFLECTION LIMITS	
<i>BEAM PARAMETERS</i>									
BEAM TABLE NO.	8	W (PLF)	750		310	FROM LEFT		LL, L/	360
QUANTITY	2	W FROM LEFT (LBS)	0		0	WA, RIGHT WC,		TL, L/	240
SPAN (FT)	4.0	W FROM RIGHT (LBS)	0		0	TO START WB)			
		W @ MID (LBS)	0		0	(FT.)			
<i>ADJUSTMENT FACTORS</i>		PL 1 (LBS)	0		0	0.0			
CD	1.00	PL 2 (LBS)	0		0	5.0			
CM*CT*CI	1.00	PL 3 (LBS)	0		0	0.0			
CL	1.00								
CF*CV	1.00								
CFU*CR	1.00								

RESULTS

BEAM DESCRIPTION 2 | 1-3/4" x 7-1/4" 1.9E MICROROLLAM LVL

<i>BEAM PROPERTIES</i>		<i>REQ'D PROPERTIES</i>		<i>PROPERTIES ADEQUATE*2</i>	
SX (IN3)	30.66	SX (IN3)	9.78		YES
AREA (IN2)	25.38	AREA (IN2)	7.44		YES
IX (IN4)	III				
E' (PSI)	1900000	<i>CALC'D LOADS & STRESSES</i>			
F' B (PSI)	2600	MAX MOMENT (LB*FT)	2,120		
F' V (PSI)	285	REACTION L (LBS)	2,120		
		REACTION R (LBS)	2,120		
<i>MAX. DEFLECTION</i>		<i>CALC'D DEFLECTION</i>			
LL (IN.)	0.13	LL (IN.)	0.02		YES
TL (IN.)	0.20	TL (IN.)	0.03		YES