



# Staff Report for Administrative Approval Hillside Review – Notice of Conditional Approval

Weber County Planning Division

## Synopsis

### Application Information

**Application Request:** Consideration and action on a request to approve a Hillside Review for the Geary residence located on Lot 37R in the Summit Eden Phase 1C.

**Applicant:** Michael David Geary

**Authorized Representative:** Kirt Bovero

**File Number:** HSR 2016-15

### Property Information

**Approximate Address:** 8343 East Summit Pass

**Project Area:** 2.01 acres

**Zoning:** DRR-1

**Existing Land Use:** Vacant

**Proposed Land Use:** Single Family Residence

**Parcel ID:** 23-130-0002

**Township, Range, Section:** 7N 2E Sec NW8 SW5

### Adjacent Land Use

<b>North:</b> Resort	<b>South:</b> Resort
<b>East:</b> Resort	<b>West:</b> Resort

### Staff Information

**Report Presenter:** Ronda Kippen  
[rkippen@co.weber.ut.us](mailto:rkippen@co.weber.ut.us)  
801-399-8768

**Report Reviewer:** RG

## Applicable Ordinances

- Weber County Land Use Code Title 108 (Standards) Chapter 14 (Hillside Development Review)
- Weber County Land Use Code Title 104 (Zones) Chapter 27 (Natural Hazards Overlay District)

## Background

The subject lot is described as *All of Lot 37R, Summit Eden Phase 1C* and was recorded as Entry# 7672945 in the Office of the Weber County Recorder. The subdivision is part of a PRUD (CUP 2013-03) that was approved by the Weber County Commission on January 21, 2014. The road providing access to the subject lot is dedicated as Summit Pass and was recorded as Entry# 2672934 in the Office of the Weber County Recorder.

IGES has performed the required geologic and geotechnical investigation to determine if there is a geologic hazard located on the site and to assess the subsurface soils in order to better design the home for slope stability and safety purposes. Information related to the construction of the dwelling including a site plan, landscape plan, grading plan, and the geologic/geotechnical report, have been distributed to the Hillside Review Board for comment. The plans have been reviewed and approved and/or conditionally approved by all applicable review agencies.

## Planning Division Review

The Planning Division Staff has determined that the requirements and standards provided by the Hillside Review Chapter have been met for the excavation and construction of the dwelling. The following submittals were required:

1. Proposed Building Plans including site plan, grading plan and landscape plan (see Exhibit A)
2. Geotechnical and Geologic Investigation Report (see Exhibit B)
3. Utah Pollution Discharge Elimination system (UPDES) Permit with Storm water Pollution Prevention Plan (See Building Permit Application Packet for UPDES and SWPPP)

## Weber County Hillside Review Board comments

The Weber County Hillside Review Board, on this particular application, made comments related to the following:

Weber County Engineering Division: The Engineering Division granted approval on August 16, 2016. The approval is subject to the applicant following all recommendations found in the applicable Geotechnical and Geological Investigation Reports. Subsequent recommendations may be necessary if additional geologic hazards are exposed during the excavation and construction phase of the dwelling. A substitute slope easement must be submitted prior to receiving Certificate of Occupancy if the property is subject to the temporary slope easement along Summit Pass.

Weber Fire District: The Fire district has granted an approval on August 24, 2016 subject to construction of the home complying with the Wildland Urban Interface Code.

Weber County Building Inspection Department: The Building Inspection Office granted approval on August 26, 2016 based on the condition that the geologist and geotechnical engineer will need to approve the footing soil prior to placement of footings.

Weber-Morgan Health Department: The Health Department has verified that that they will not impose any requirements or conditions for this application due to the proposed residence connecting to the Powder Mountain Water and Sewer District for culinary and wastewater services.

Weber County Planning Division: The Planning Division has granted approval subject to the applicant complying with all Board requirements and conditions. This approval is also subject to the applicant strictly adhering to the recommendations outlined in the geologic and geotechnical investigation report dated July 8, 2016 provided by IGES (IGES Project No. 02332-001) including the following recommendations:

- All excavation should be observed by an IGES representative during proof rolling or otherwise prior to placement of engineered fill to evaluate whether soft, loose, or otherwise deleterious earth materials have been removed and that recommendations presented in the Geotechnical and Geological Report have been compiled with.
- A foundation drain must be installed around below-ground foundations (e.g., basement walls) to minimize the potential for flooding from shallow ground water, which may be present at various times during the year, particularly spring run-off.
- IGES recommends a perimeter foundation drain be constructed for the proposed residential structure in accordance with the IRC.
- IGES will be on site to verify compliance with these recommendations.
- Landscaping at the site should be planned to utilize drought resistant plants that require minimal watering. Roof runoff devices should be installed to direct all runoff a minimum of 10 feet away from the structure. Landscape plans must conform to Weber County development codes.

## Planning Division Recommendations

Based on site inspections and review agency comments, the Planning Division Staff has determined that it is necessary to impose additional requirements and conditions as part of approving HSR #2016-15. The recommendation for approval is subject to adherence to all review agencies conditions and based on the following conditions:

1. The cover sheet must be revised to included "Geologic and Geotechnical Investigation Report" for IGES Project# 02332-001.
2. All excavation should be observed by an IGES representative during proof rolling or otherwise prior to placement of engineered fill to evaluate whether soft, loose, or otherwise deleterious earth materials have been removed and that recommendations presented in the Geotechnical and Geological Report have been compiled with.
3. A foundation drains must be installed around below-ground foundations (e.g., basement walls) to minimize the potential for flooding from shallow ground water, which may be present at various times during the year, particularly spring run-off.
4. IGES recommends a perimeter foundation drain be constructed for the proposed residential structure in accordance with the IRC.
5. IGES will be on site to verify compliance with these recommendations.
6. Landscaping at the site should be planned to utilize drought resistant plants that require minimal watering. Roof runoff devices should be installed to direct all runoff a minimum of 10 feet away from the structure.



7. A substitute slope easement must be submitted prior to receiving Certificate of Occupancy if the property is subject to the temporary slope easement along Summit Pass.

The recommendation is based on the following findings:

1. The application was submitted and with the required conditions, has been deemed complete.
2. The requirements and standards found in the Hillside Development Review Procedures and Standards Chapter have been met or will be met during the excavation and construction phase of the dwelling.
3. The Hillside Review Board members reviewed the application individually and have provided their comments.
4. The applicant has met or will meet, as part of the building permit process and/or during the excavation and construction phase of the dwelling, the requirements and conditions set forth by the Hillside Review Board. As a condition it is understood, by the applicant and the geo-technical engineer and engineering geologist, that if any geologic hazards are revealed during the excavation and construction phase of the dwelling, work on Lot 37R in the Summit Eden Phase 1C will cease pending the development of appropriate mitigation measures and subsequent approval by the County.
5. The Planning Division Staff has determined that the proposed improvements have been sited within the required setbacks for the DRR-1 zone with the exception of the driveway and retaining wall(s).

### Administrative Approval

Administrative approval of Lot 37R in the Summit Eden Phase 1C Hillside Review (HR#2016-15), is hereby granted based upon its compliance with the Weber County Land Use Code. This approval is subject to the requirements of applicable review agencies and is based on the recommendations, conditions and findings listed in this staff report.

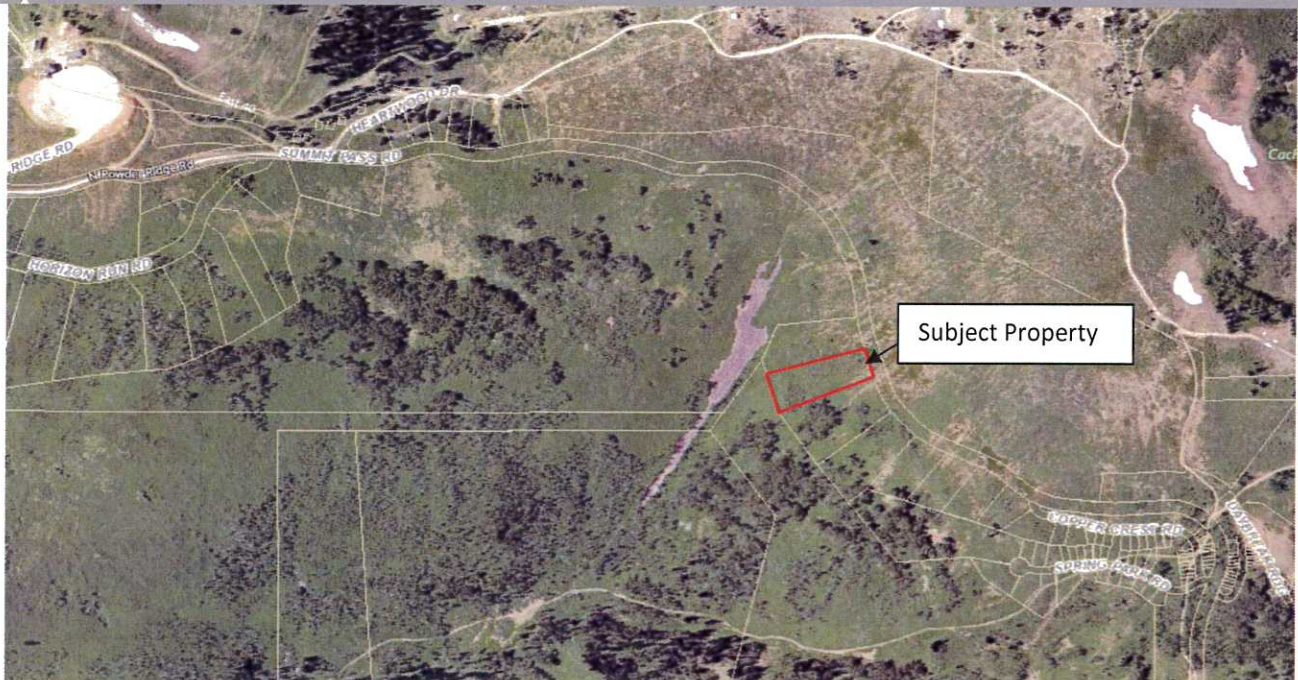
Date of Administrative Approval: September 6, 2016

  
Rick Grover  
Weber County Planning Director

### Exhibits

- A. Proposed Building Plans
- B. Geotechnical and Geologic Investigation Report

### Map 1











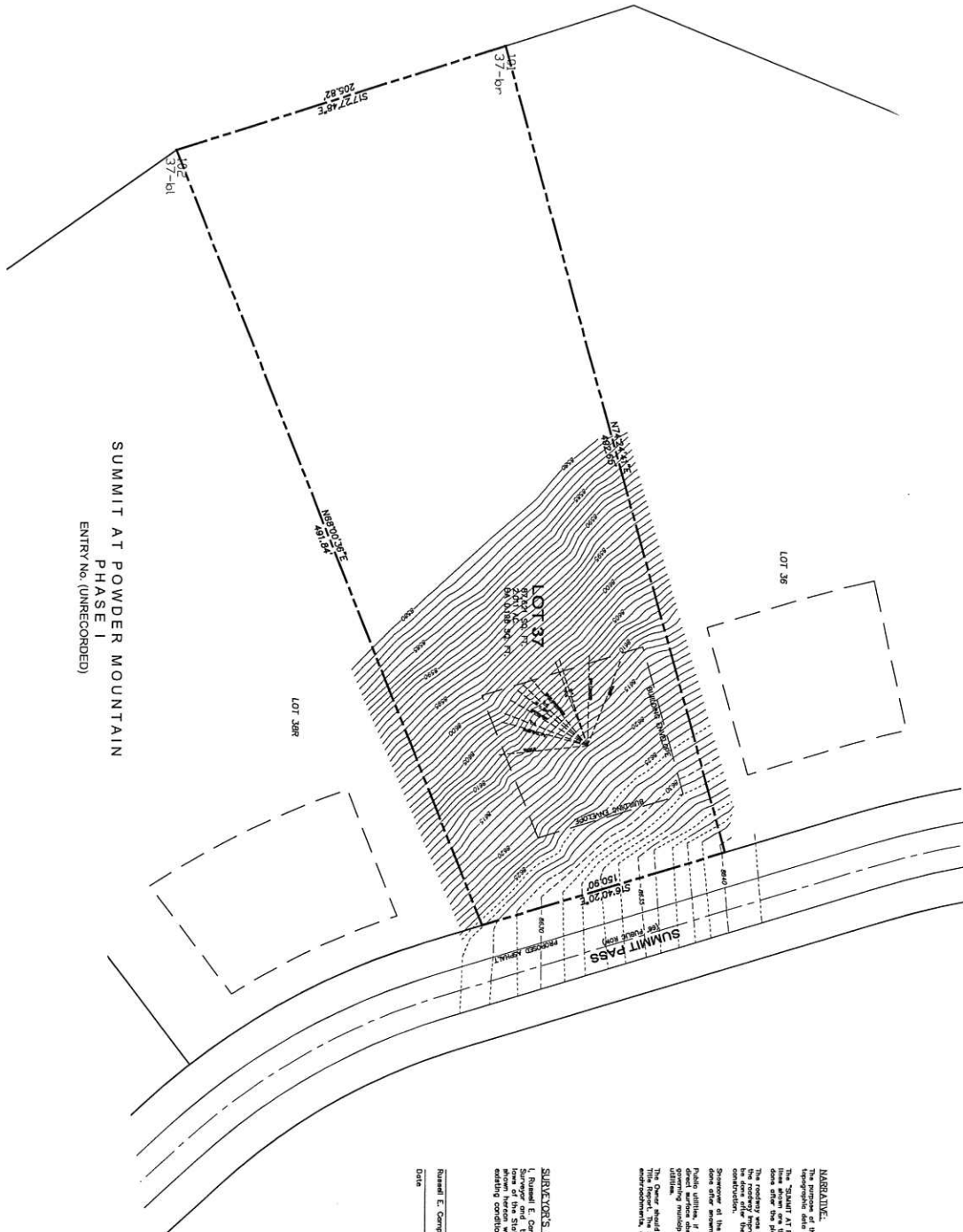






**Exhibit A**

PARCELS OF  
OPEN SPACE



SUMMIT AT POWDER MOUNTAIN  
PHASE I  
ENTRY No. (UNRECORDED)

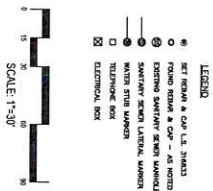
**TOPOGRAPHIC SURVEY MAP**  
LOT 37, SUMMIT AT POWDER MOUNTAIN PHASE I  
LOCATED IN THE SOUTHWEST QUARTER OF SECTION 5, &  
THE NORTHWEST QUARTER OF SECTION 8,  
TOWNSHIP 7 NORTH, RANGE 2 EAST  
SALT LAKE BASE & MERIDIAN  
WEBER COUNTY, UTAH



**MARGINALIA:** The intent is to locate the property boundary and provide the proper data for the design of a project. The survey was conducted in accordance with the standards of a professional land surveyor. The survey was conducted in accordance with the standards of a professional land surveyor. The survey was conducted in accordance with the standards of a professional land surveyor.

**SURVEYOR'S CERTIFICATE:**  
I, Russell E. Campbell, do hereby certify that I am a Professional Land Surveyor and that I had conducted the survey on premises under the provisions of the Utah Surveying Act, Chapter 10, Title 19, Utah Code, and that the same was conducted in accordance with the standards of a professional land surveyor. The survey was conducted in accordance with the standards of a professional land surveyor.

Russell E. Campbell  
Date \_\_\_\_\_



BOUNDARY & TOPOGRAPHIC SURVEY  
LOT 37, SUMMIT AT POWDER MOUNTAIN PHASE I  
WEBER COUNTY, UTAH

JOB No.	1110
DC SURVEY No.	
DATE	

REVISIONS	
DATE	COMMENTS

**BASELINE SURVEYING, Inc**  
1058 E. 2100 S  
Salt Lake City, UT 84106  
(801) 209-2152

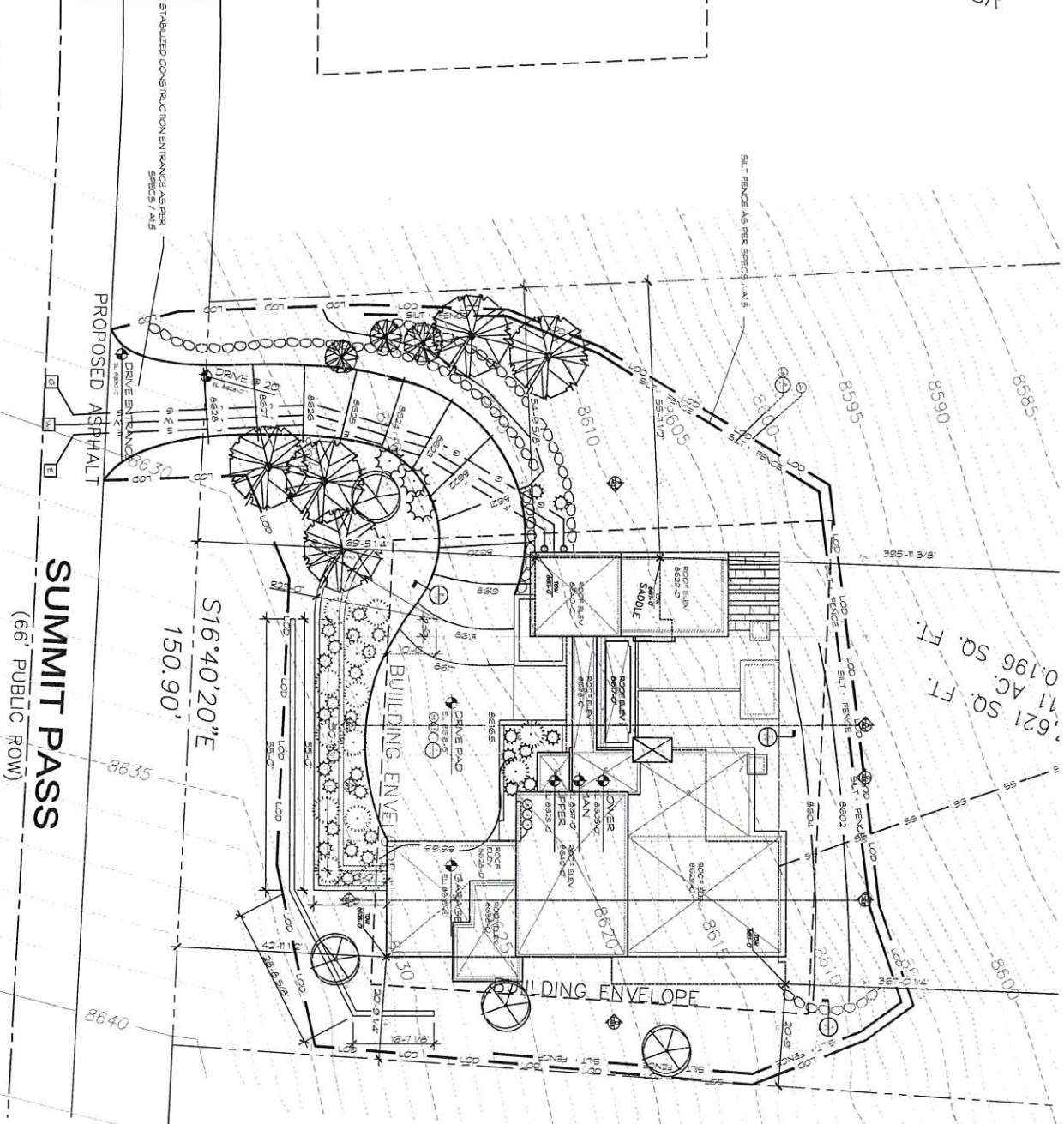
SHEET  
1 OF 1





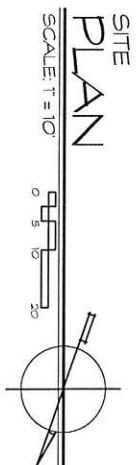
JBR

# Exhibit A



0.621 SQ. FT.  
0.196 AC. SQ. FT.

**SUMMIT PASS**  
(66' PUBLIC ROW)



SITE  
**PLAN**  
SCALE 1" = 10'

**NOTE**

SEE SHEET A10 FOR FIELD NOTES & INFO

CONTRACTOR TO FIELD VERIFY LOCATION OF UTILITY LINES AS REQUIRED

CONTRACTOR TO FIELD VERIFY LOCATION BETWEEN GAS AND ELECTRICAL LINES

A1.2

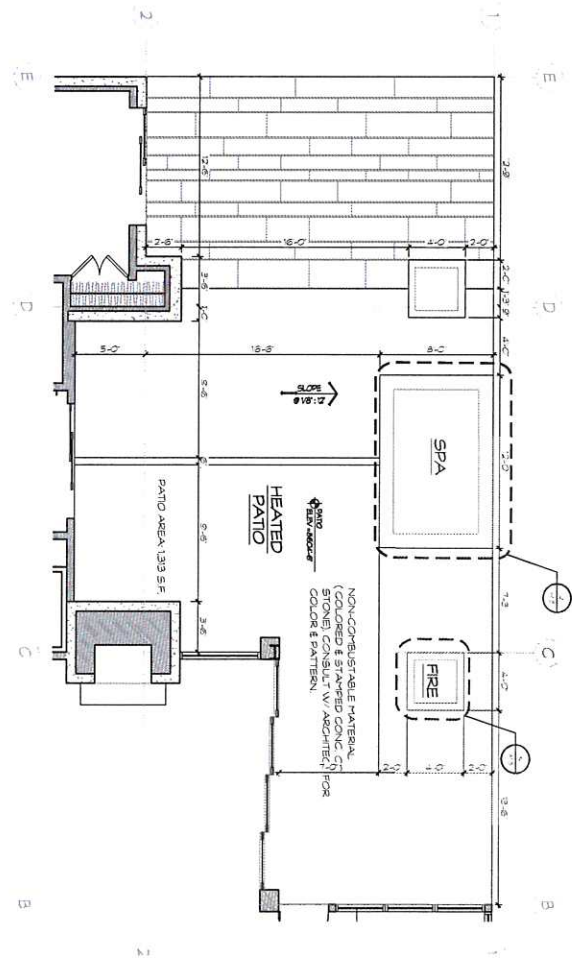
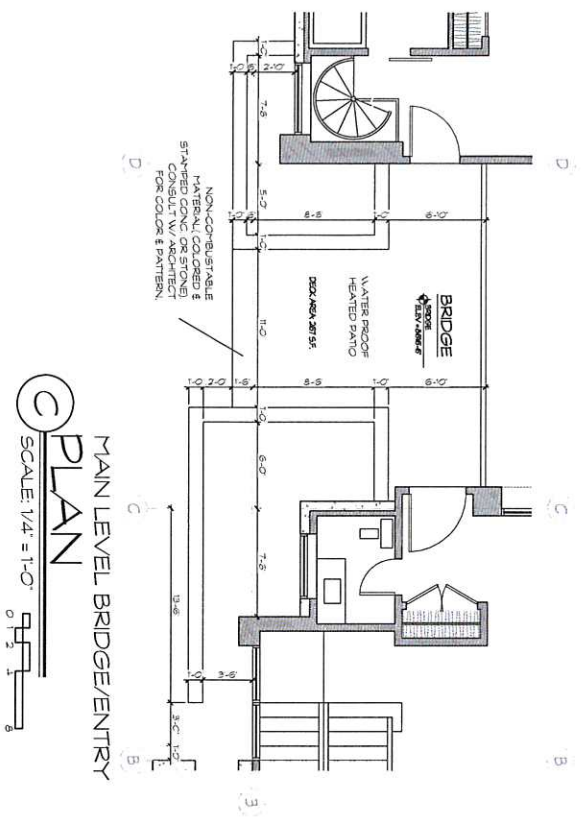
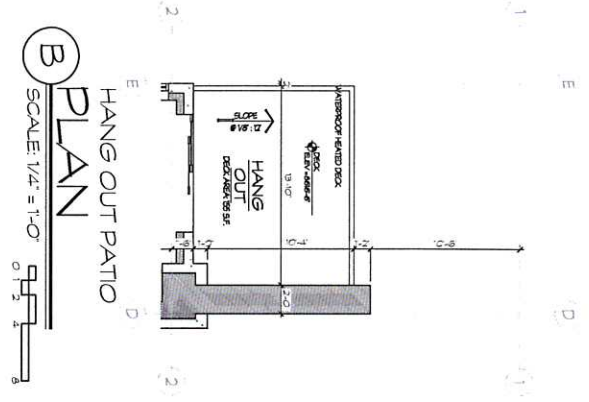
**UP WALL DESIGN**  
1025 EAST HOLLYWOOD AVE. S.U.C. UT. 84140-6700

A NEW DESIGN FOR :  
**LOT 37 POWDER MOUNTAIN**  
WEBER COUNTY, UT

2 JAN 2018  
REVISIONS

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**Exhibit A**

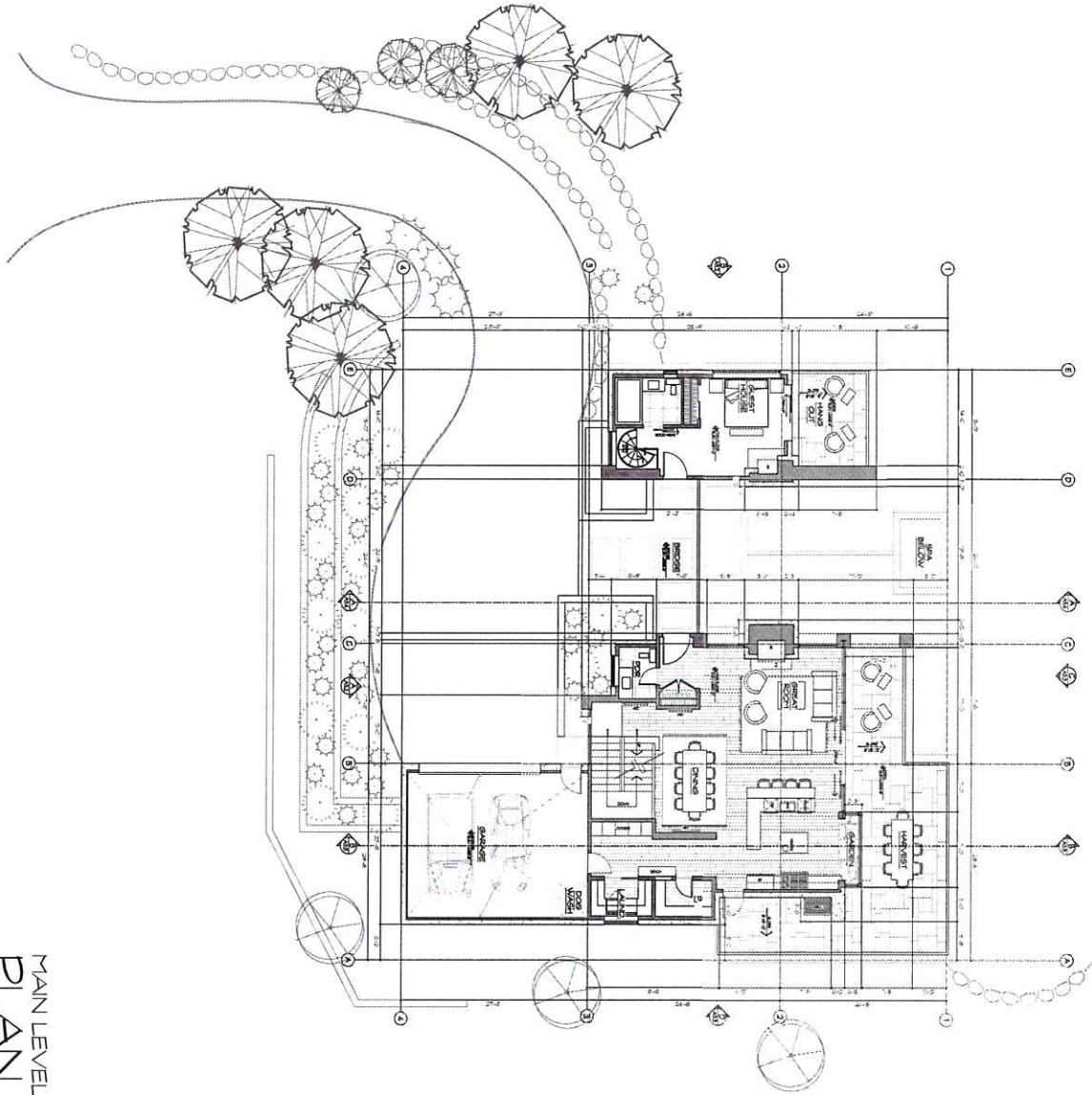


**NOTE**  
GRADE OF ALL PATIOS ADJACENT TO HOME TO SLOPE AWAY AT A MINIMUM OF 1% PER 1'-0"

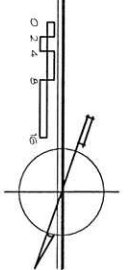




**Exhibit A**

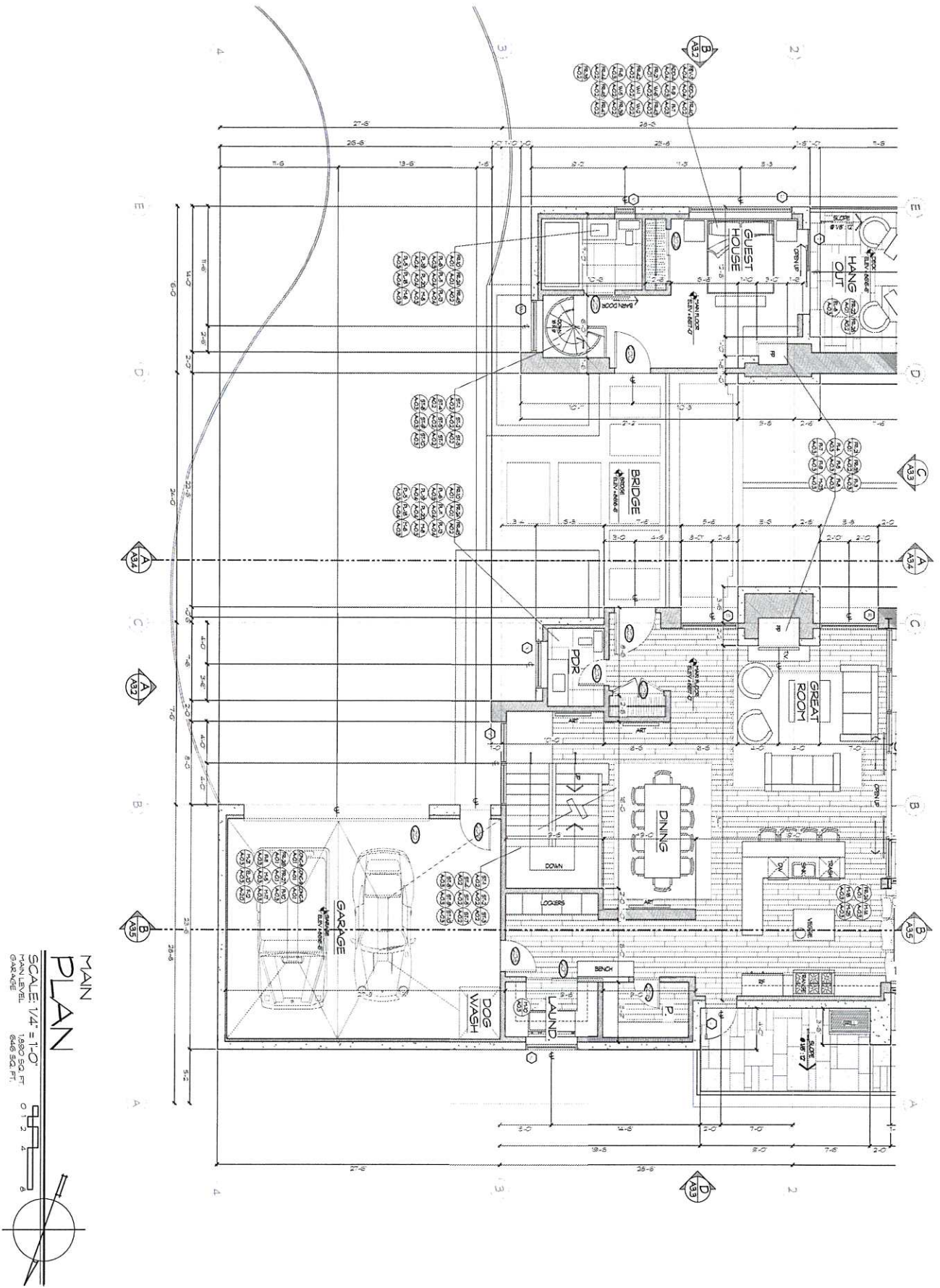


MAIN LEVEL  
**PLAN**  
 SCALE 1/8" = 1'-0"  
 MAIN LEVEL 1,897 SQ. FT.  
 GARAGE 646 SQ. FT.





**Exhibit A**



A2.3

**UP WALL DESIGN**

10-25 EAST HOLLYWOOD AVE. S.E.C. UT 80148-0799

A NEW DESIGN FOR:  
**LOT 37 POWDER MOUNTAIN**

10-25 EAST HOLLYWOOD AVE. S.E.C. UT 80148-0799  
 WEBER COUNTY, UT

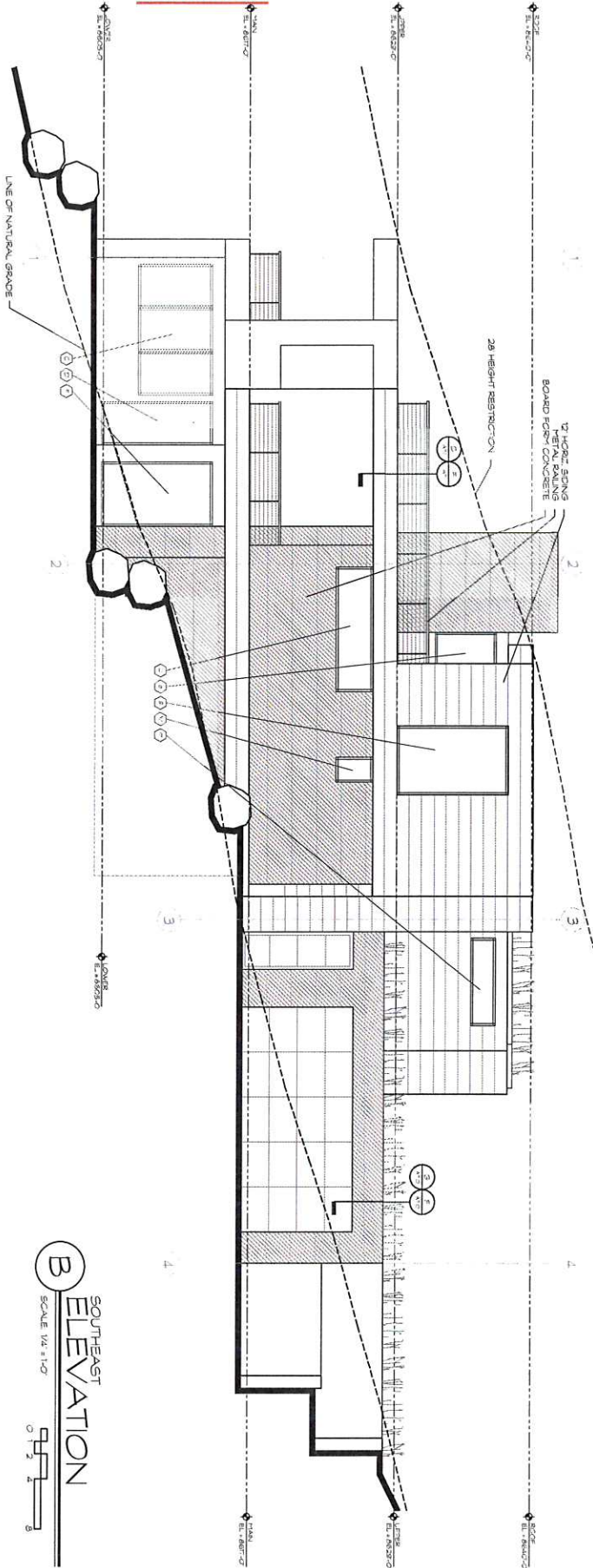
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DATE	2.14.2018
BY	BRUCE
CHECKED	
DATE	

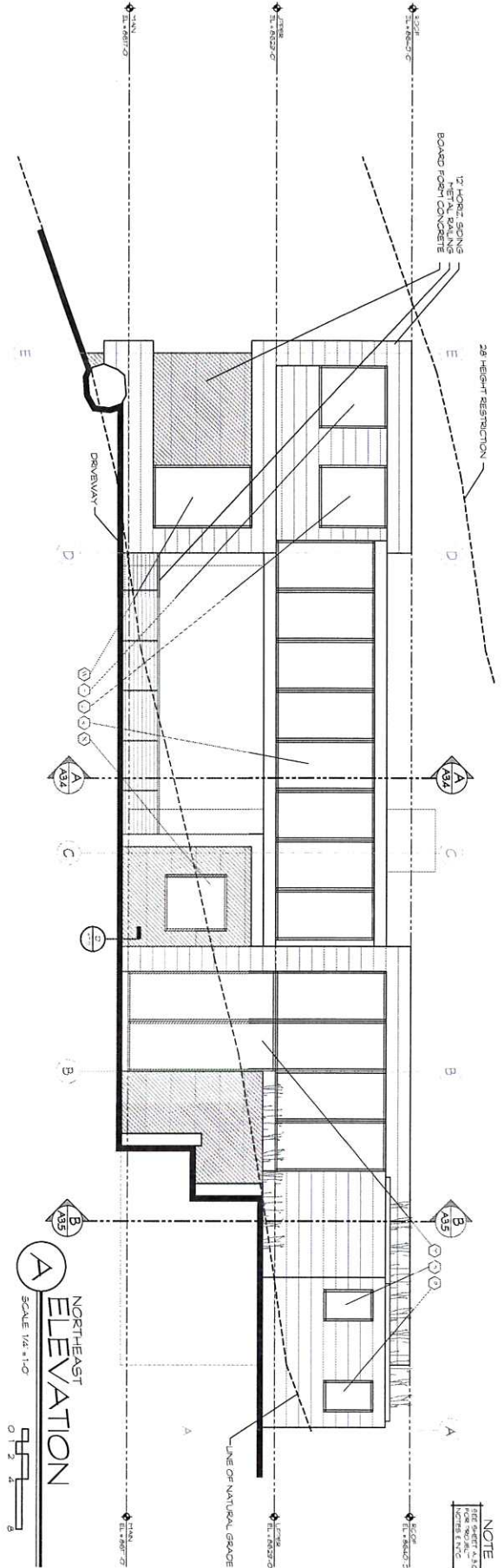
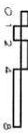




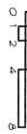
**Exhibit A**



**B** SOUTHEAST  
ELEVATION  
SCALE 1/4" = 1'-0"

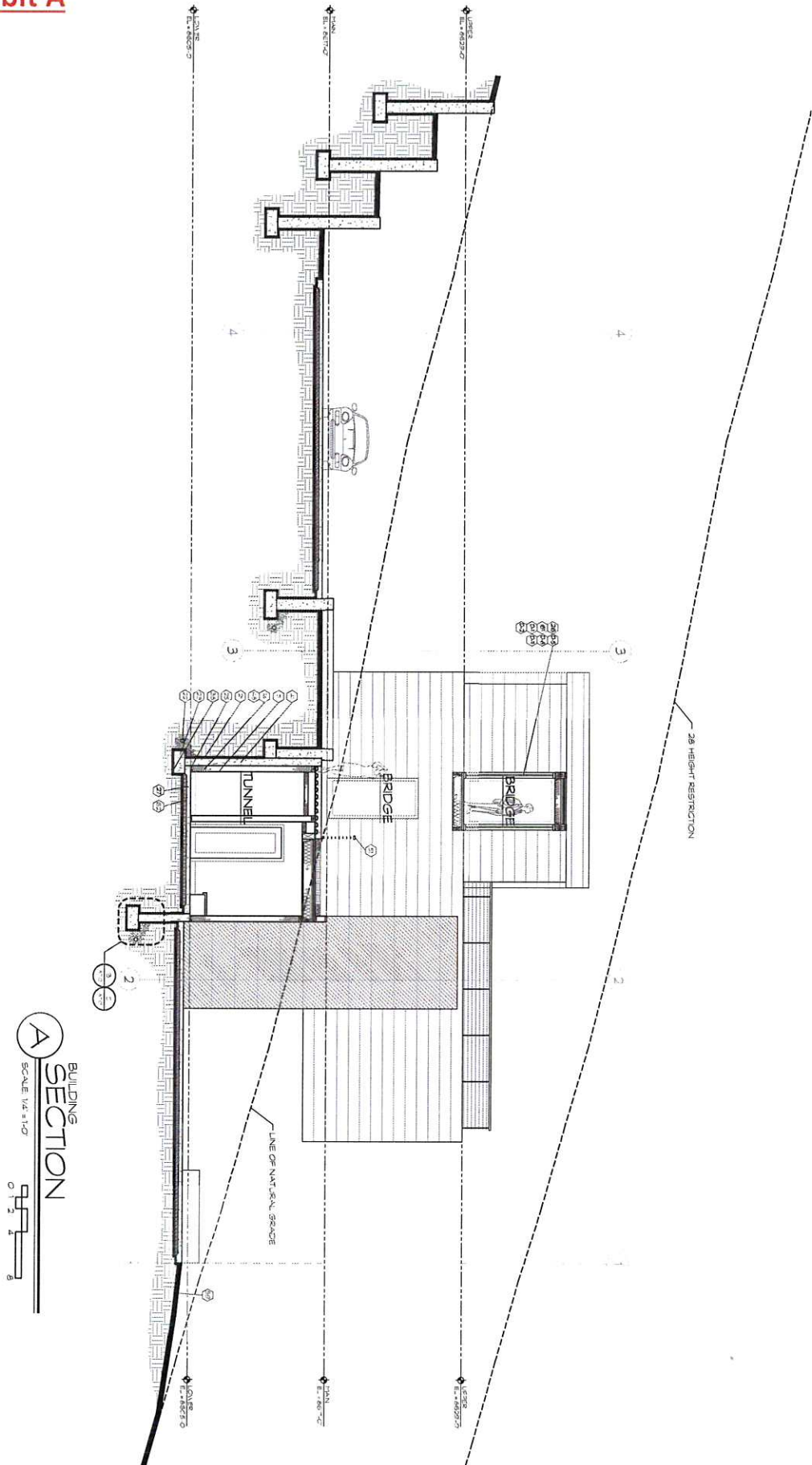


**A** NORTHEAST  
ELEVATION  
SCALE 1/4" = 1'-0"



NOTE  
SEE SHEET A-130  
FOR SCHEDULE  
OF FINISHES

**Exhibit A**



**A**  
BUILDING SECTION  
SCALE 1/4" = 1'-0"

NOTE  
SEE SHEET A.10 FOR NOTES  
CONSTRUCTION

A3.4

**UP WALL DESIGN**  
1025 EAST HOLLYWOOD AVE. S.E.C. CT. BLDG 6000

A NEW DESIGN FOR:  
**LOT 37 POWDER MOUNTAIN**  
LOT 37 POWDER MOUNTAIN  
WEBER COUNTY, UT

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DATE	2 JAN 2018
REVISIONS	
NO.	DESCRIPTION

DATE	2 JAN 2018
REVISIONS	
NO.	DESCRIPTION







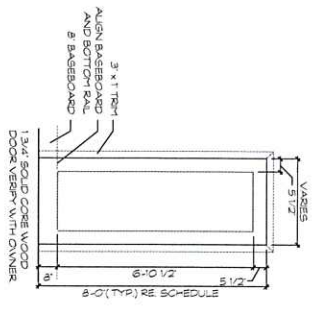




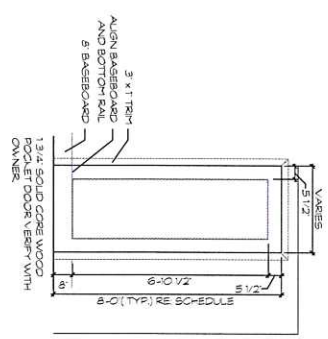
NOTE  
 1. MATCH DOOR SCHEDULE TO ALL ARCHITECTURE. DO NOT  
 2. OMIT MATERIALS FROM THE SCHEDULE FOR GLASS  
 3. DOOR TYPES TO BE ON THE BASIS OF THE DOOR

### DOOR SCHEDULE

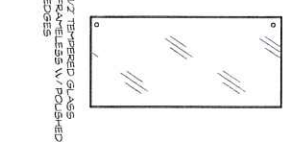
NO.	W.D.	H.G.H.	SIZE	THICKNESS	MATERIAL	TYPE	FINISH	HARDWARE	RATING	REMARKS	LOCATION	DETAILS	FRAMING	MATERIAL	TYPE	FINISH	REMARKS	NO.	
LOWER LEVEL																			
100	3'-6"	8'-0"	1/2"		GLASS	C	CLEAR				INTERIOR			GLASS		CLEAR		GLASS BATH DOOR	100
101	2'-4"	8'-0"	1/2"		GLASS	C	CLEAR				INTERIOR			GLASS		CLEAR		SHOWER GUARD GLASS	101
102	4'-6"	8'-0"	1/2"		WOOD	D	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	102
103	4'-6"	8'-0"	1/2"		WOOD	D	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	103
104	3'-0"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	104
105	2'-8"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	105
106	2'-8"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	106
107	3'-0"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	107
108	2'-8"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	108
109	2'-0"	8'-0"	1/2"		GLASS	C	CLEAR				INTERIOR			GLASS		CLEAR		SHOWER GUARD GLASS	109
110	2'-8"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	110
MAIN LEVEL																			
200	3'-6"	8'-0"	1/2"		WOOD	E	STAIN				EXTERIOR			WOOD		STAIN		CUSTOM ENTRY DOOR	200
201	3'-0"	8'-0"	1/2"		WOOD	D	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	201
202	5'-0"	8'-0"	1/2"		WOOD	D	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	202
203	4'-0"	8'-0"	1/2"		WOOD	E	STAIN				EXTERIOR			WOOD		STAIN		CUSTOM ENTRY DOOR	203
204	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	204
205	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		DOUBLE DOOR	205
206	5'-0"	8'-0"	1/2"		WOOD	B	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	206
207	5'-0"	8'-0"	1/2"		WOOD	B	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	207
208	3'-0"	8'-0"	1/2"		WOOD	F	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	208
209	3'-0"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	209
210	18'-0"	9'-0"	0.75"		WOOD	G	STAIN				EXTERIOR			WOOD		STAIN		SHOWER DOOR	210
UPPER LEVEL																			
300	2'-6"	8'-0"	1/2"		WOOD	B	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	300
301	4'-0"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	301
302	3'-0"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	302
303	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	303
304	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	304
305	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		POCKET DOOR	305
306	2'-6"	8'-0"	1/2"		GLASS	C	CLEAR				INTERIOR			GLASS		CLEAR		SHOWER GUARD GLASS	306
307	2'-6"	8'-0"	1/2"		WOOD	A	STAIN				INTERIOR			WOOD		STAIN		SHOWER GUARD GLASS	307



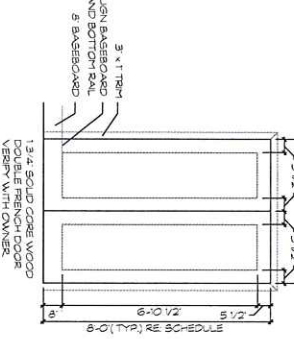
A SINGLE INTERIOR SOLID



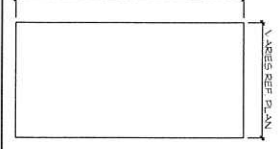
B SINGLE INTERIOR POCKET



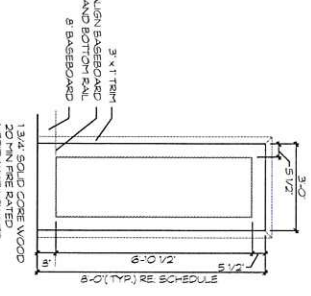
C INTERIOR SHOWER



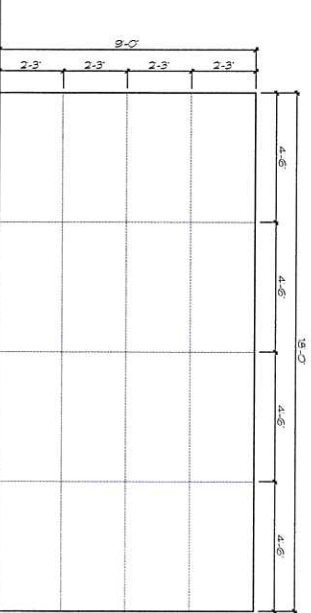
D DOUBLE INTERIOR DOOR



E CUSTOM ENTRY DOOR



F SINGLE INTERIOR SOLID 20 MIN FIRE RATED



G GARAGE DOOR

Exhibit A

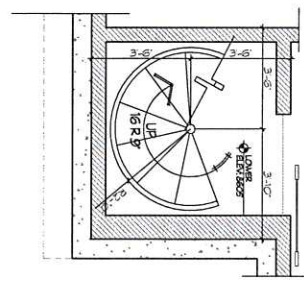
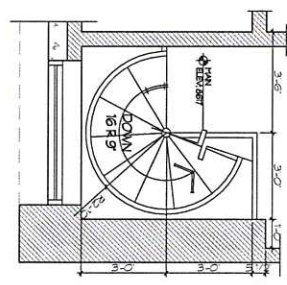
UP WALL DESIGN





1

2  
H  
LOOKS TO MAN



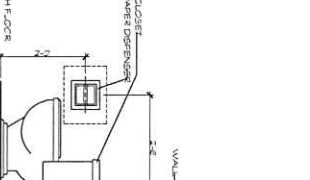
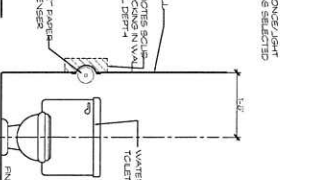
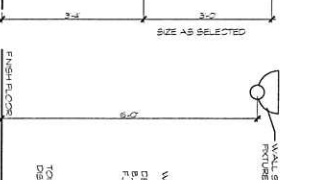
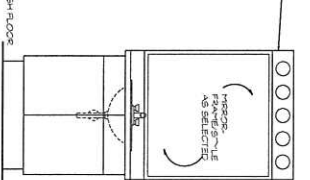
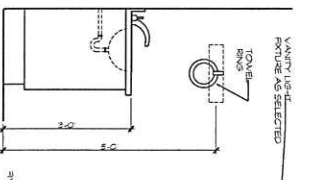
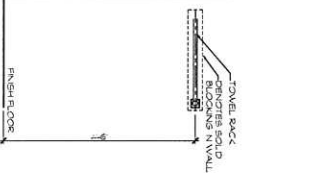
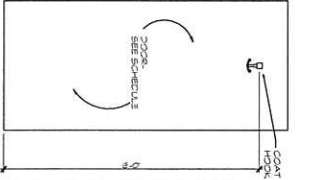
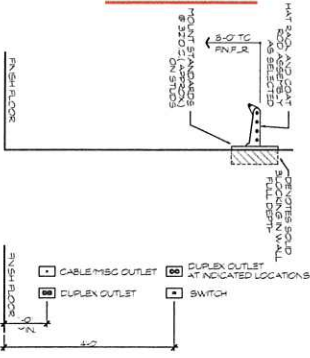
ALL RIGHTS RESERVED. THIS DOCUMENT IS THE PROPERTY OF UP WALL DESIGN. IT IS TO BE USED ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED HEREIN. ANY REUSE OR REPRODUCTION OF THIS DOCUMENT WITHOUT THE WRITTEN PERMISSION OF UP WALL DESIGN IS STRICTLY PROHIBITED. UP WALL DESIGN SHALL NOT BE LIABLE FOR ANY DAMAGES, INCLUDING CONSEQUENTIAL DAMAGES, ARISING FROM THE USE OF THIS DOCUMENT. THE USER ASSUMES ALL LIABILITY FOR THE ACCURACY AND COMPLETENESS OF THE INFORMATION CONTAINED HEREIN. THIS DOCUMENT IS NOT TO BE USED AS A SUBSTITUTE FOR PROFESSIONAL ENGINEERING OR ARCHITECTURAL SERVICES. THE USER SHALL OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE APPROPRIATE AGENCIES. UP WALL DESIGN SHALL NOT BE RESPONSIBLE FOR ANY ERRORS OR OMISSIONS IN THIS DOCUMENT. THE USER SHALL BE RESPONSIBLE FOR VERIFYING ALL DIMENSIONS AND CONDITIONS BEFORE CONSTRUCTION. UP WALL DESIGN SHALL NOT BE RESPONSIBLE FOR ANY DELAYS OR COST INCREASES RESULTING FROM CHANGES OR OMISSIONS BY THE USER. UP WALL DESIGN SHALL NOT BE RESPONSIBLE FOR ANY DAMAGES, INCLUDING CONSEQUENTIAL DAMAGES, ARISING FROM THE USE OF THIS DOCUMENT. THE USER ASSUMES ALL LIABILITY FOR THE ACCURACY AND COMPLETENESS OF THE INFORMATION CONTAINED HEREIN. THIS DOCUMENT IS NOT TO BE USED AS A SUBSTITUTE FOR PROFESSIONAL ENGINEERING OR ARCHITECTURAL SERVICES. THE USER SHALL OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE APPROPRIATE AGENCIES. UP WALL DESIGN SHALL NOT BE RESPONSIBLE FOR ANY ERRORS OR OMISSIONS IN THIS DOCUMENT. THE USER SHALL BE RESPONSIBLE FOR VERIFYING ALL DIMENSIONS AND CONDITIONS BEFORE CONSTRUCTION. UP WALL DESIGN SHALL NOT BE RESPONSIBLE FOR ANY DELAYS OR COST INCREASES RESULTING FROM CHANGES OR OMISSIONS BY THE USER.



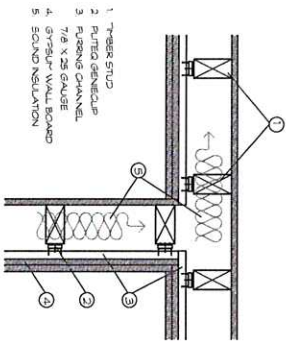


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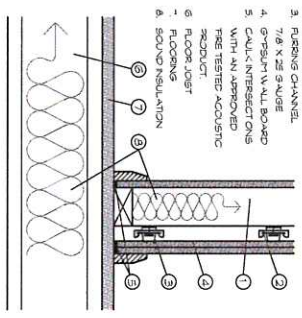
## F TYPICAL MOUNTING HEIGHTS



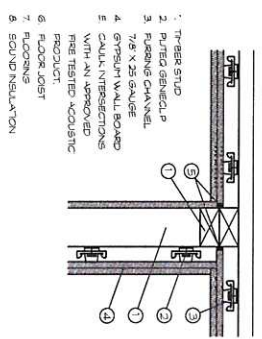
## E SOUNDPROOFING WALL INTERSECTIONS



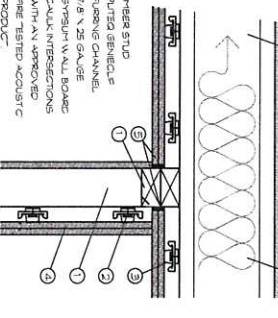
## D SOUNDPROOFING WALL TO FLOOR



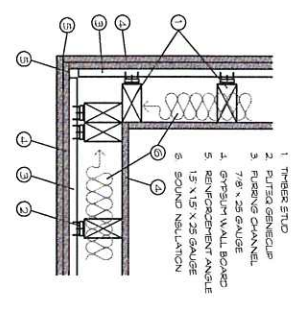
## B SOUNDPROOFING WALL TO CEILING



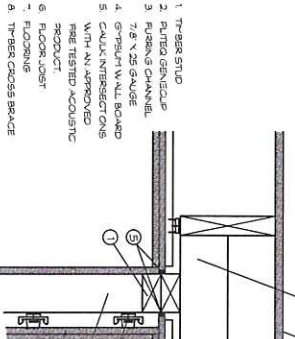
## A SOUNDPROOFING WALL TO CEILING FLOOR



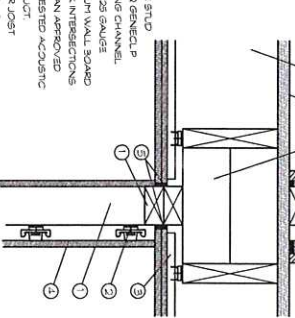
## C SOUNDPROOFING CORNER JUNCTION



## B SOUNDPROOFING WALL TO CEILING

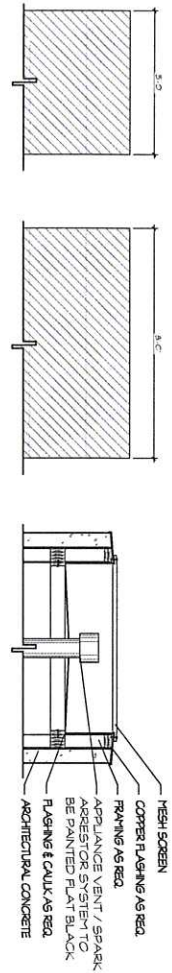


## A SOUNDPROOFING WALL TO CEILING FLOOR





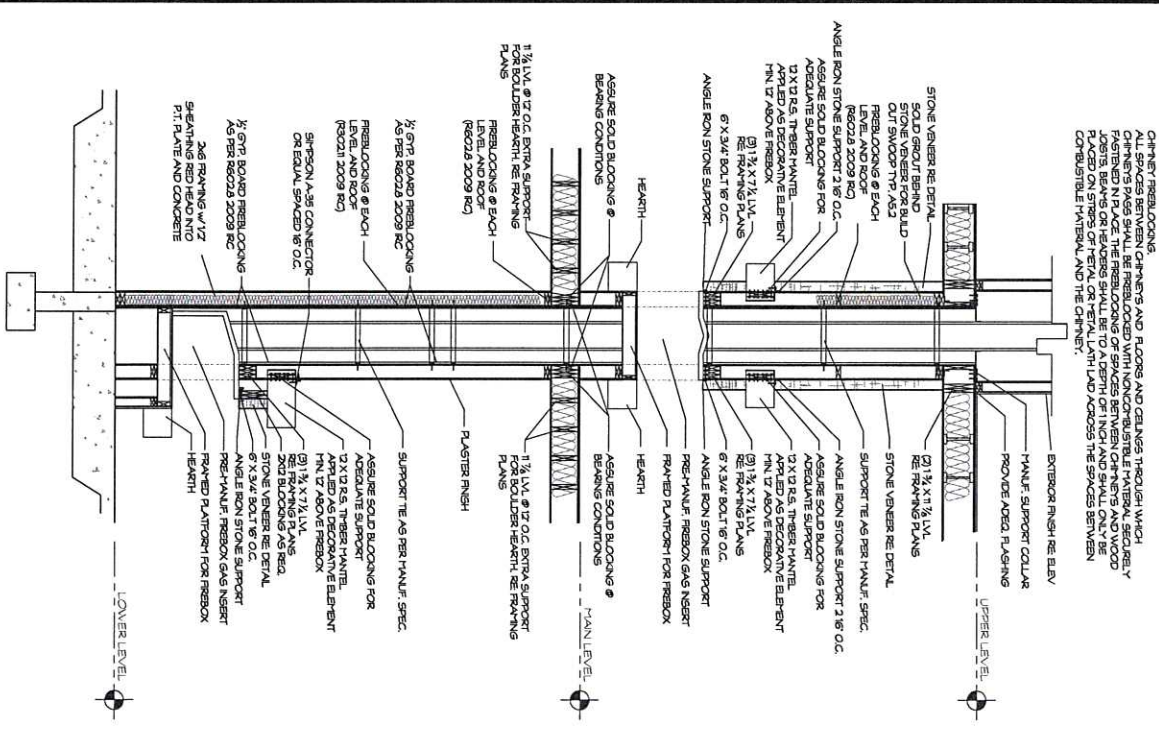
B CHIMNEY DETAIL



HIGH SCREEN  
COPPER FLASHING AS REQ.  
APPLIANCE VENT / GAS/AIR EXHAUSTOR SYSTEM TO BE PAINTED FLAT BLACK FLASHING & GULLY AS REQ.  
ARCHITECTURAL CONCRETE

NOTE: PASTER REBRIDGE CHASE SHALL AS WITH SEALED GAS UNIT

NOTE: PASTER REBRIDGE CHASE SHALL AS WITH SEALED GAS UNIT

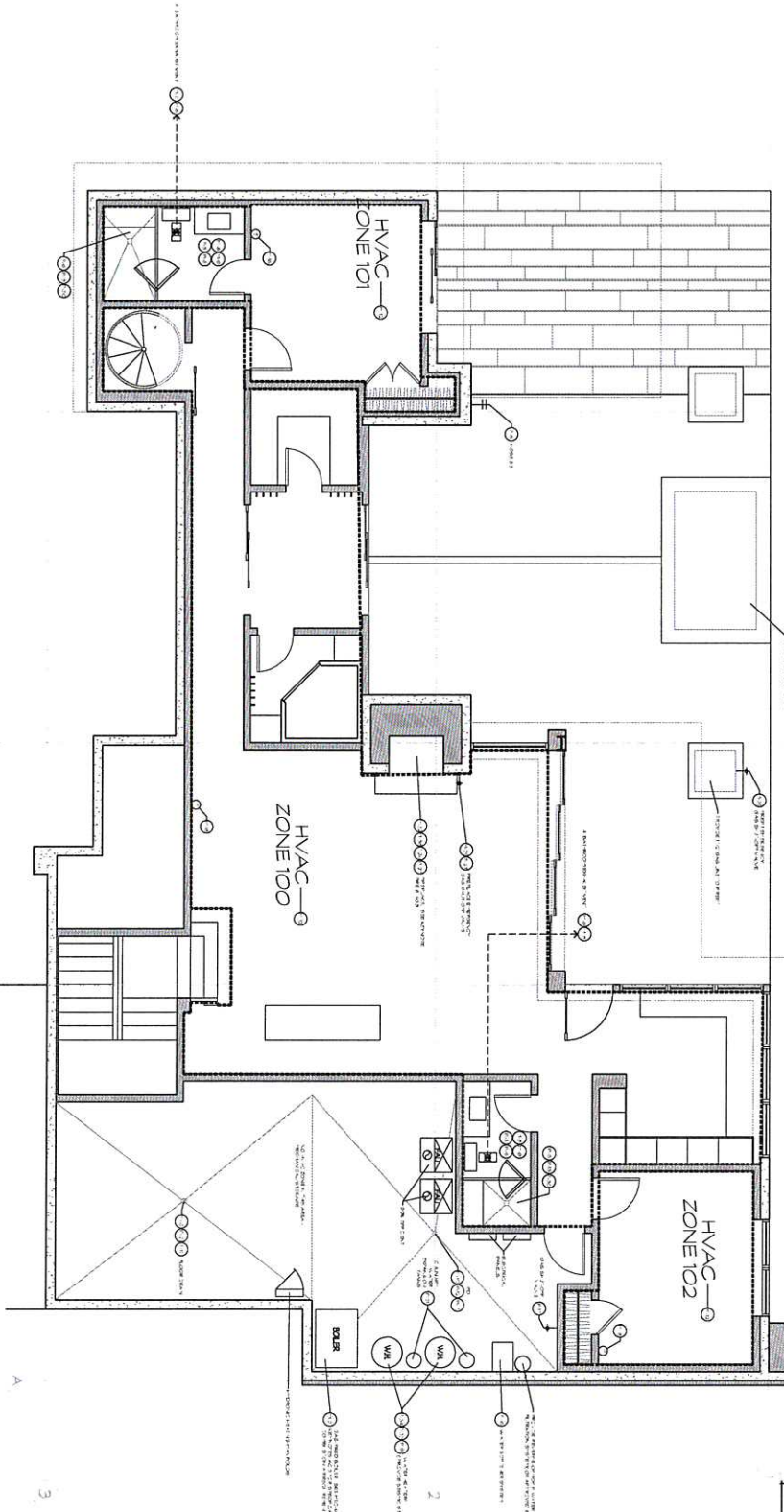


A DIRECT VENT CHIMNEY DETAIL



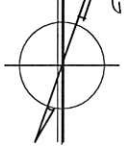


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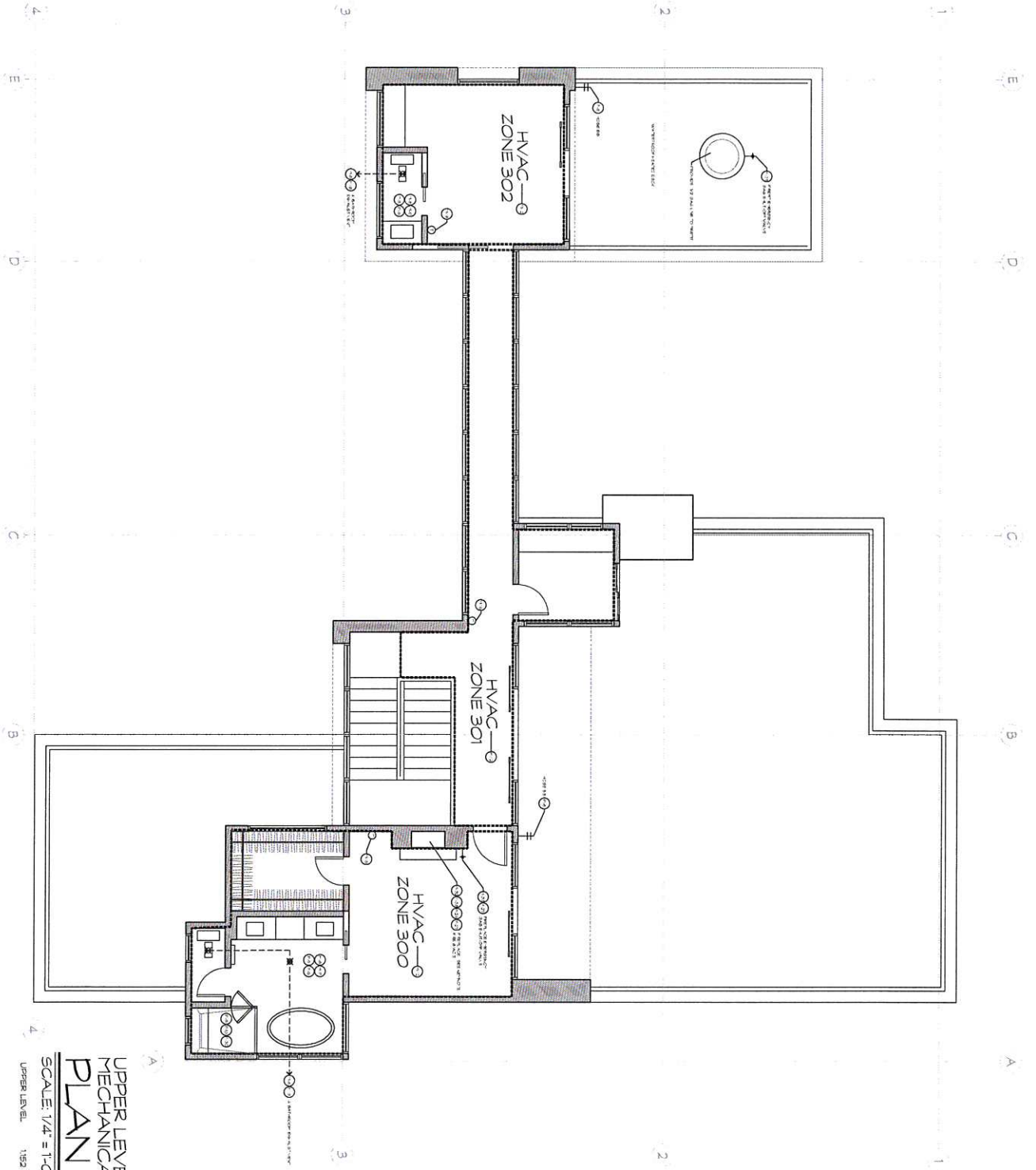
## LOWER LEVEL MECHANICAL & PLUMBING PLAN

SCALE 1/4" = 1'-0"  
 LOWER LEVEL 1,810 SQ. FT.  
 5'0" / 1' = 1" 644 SQ. FT.



- MECHANICAL PLUMBING LAYOUTS ARE SHOWN IN SEPARATE. THE CONTRACTOR IS RESPONSIBLE TO INSTALLATION OF ALL RELATED ITEMS WITH EXISTING CONDITIONS AND RELATED TRADES.
- SEE SHEET 101 FOR MECHANICAL PROJECT NOTES AND INFORMATION.
- SEE SHEET 101 FOR PLUMBING PROJECT NOTES AND INFORMATION.
- FOR USE GENERAL AS CONDITIONS THROUGHOUT COORDINATE WITH CONTRACTOR FOR INSTALLATION.
- CONTRACTOR TO ENSURE ALL HANGABLE SPACES TO BE PROVIDED WITH ADEQUATE RETURN AIR.

**Exhibit A**



UPPER LEVEL  
MECHANICAL & PLUMBING  
PLAN  
SCALE: 1/4" = 1'-0"  
UPPER LEVEL 1153 SQ. FT.

- MECHANICAL/PLUMBING LAYOUTS ARE SHOWN IN SCHEMATIC. THE CONTRACTOR IS RESPONSIBLE TO INSTALLATION OF ALL RELATED ITEMS WITH EXISTING CONDITIONS AND RELATED TRADES.
- SEE SHEET #01 FOR MECHANICAL PROJECT NOTES AND INFORMATION.
- SEE SHEET #01 FOR PLUMBING PROJECT NOTES AND INFORMATION.
- PROVIDE GENERAL AND COORDINATING THROUGHOUT COORDINATE WITH CONTRACTOR FOR INSTALLATION.
- CONTRACTOR TO ENSURE ALL HABITABLE SPACES TO BE PROVIDED WITH ADEQUATE RETURN AIR.

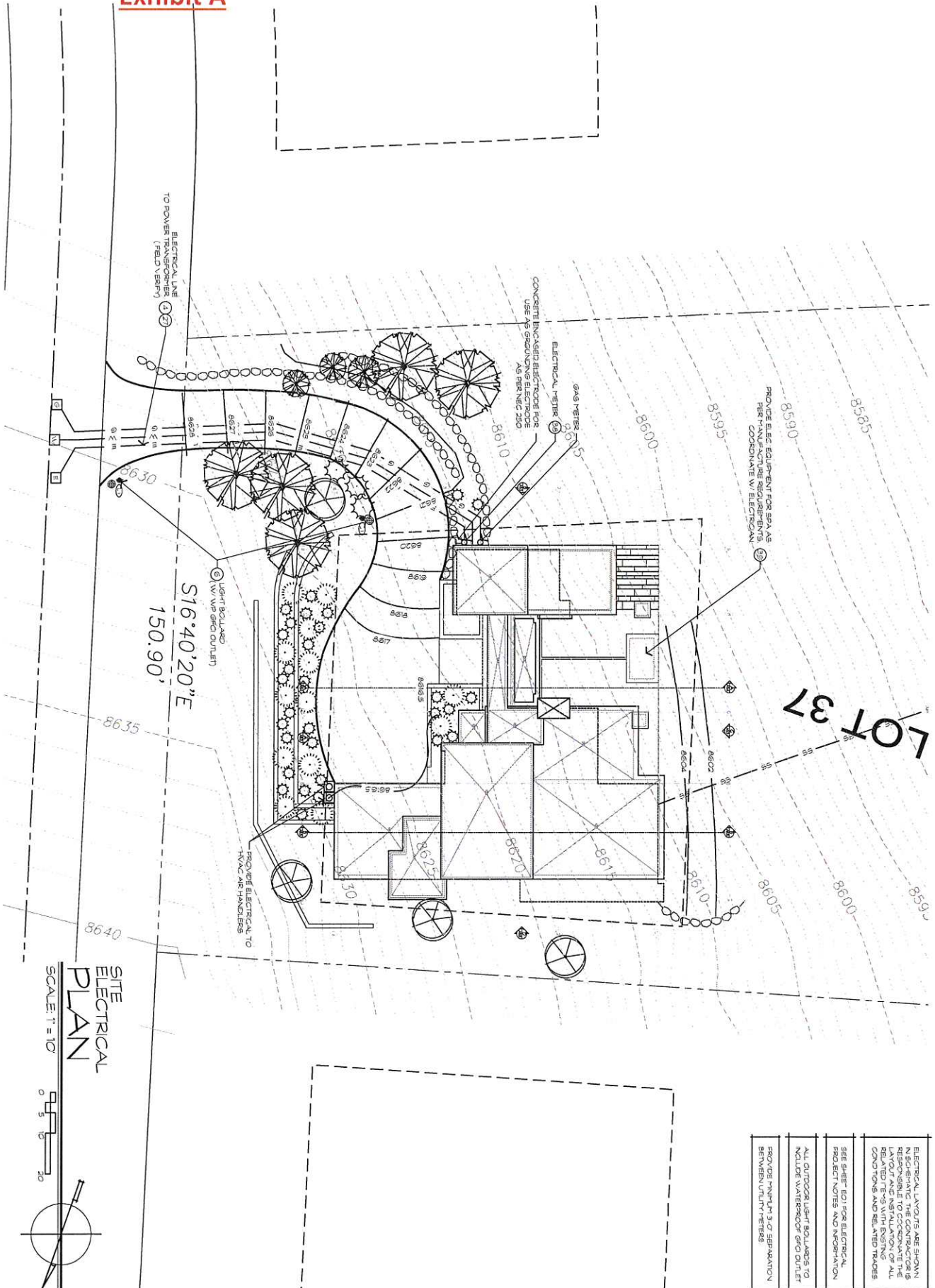
**UP WALL DESIGN**  
1625 EAST HOLLYWOOD AVE. S.E.C. UT 80146-60704  
MP2.2

A NEW DESIGN FOR:  
**LOT 37 POWDER MOUNTAIN**  
LOT 37 POWDER MOUNTAIN  
WEBER COUNTY, UT

**Page 52 of 136**

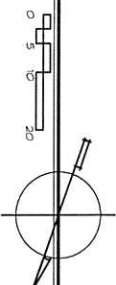


**Exhibit A**



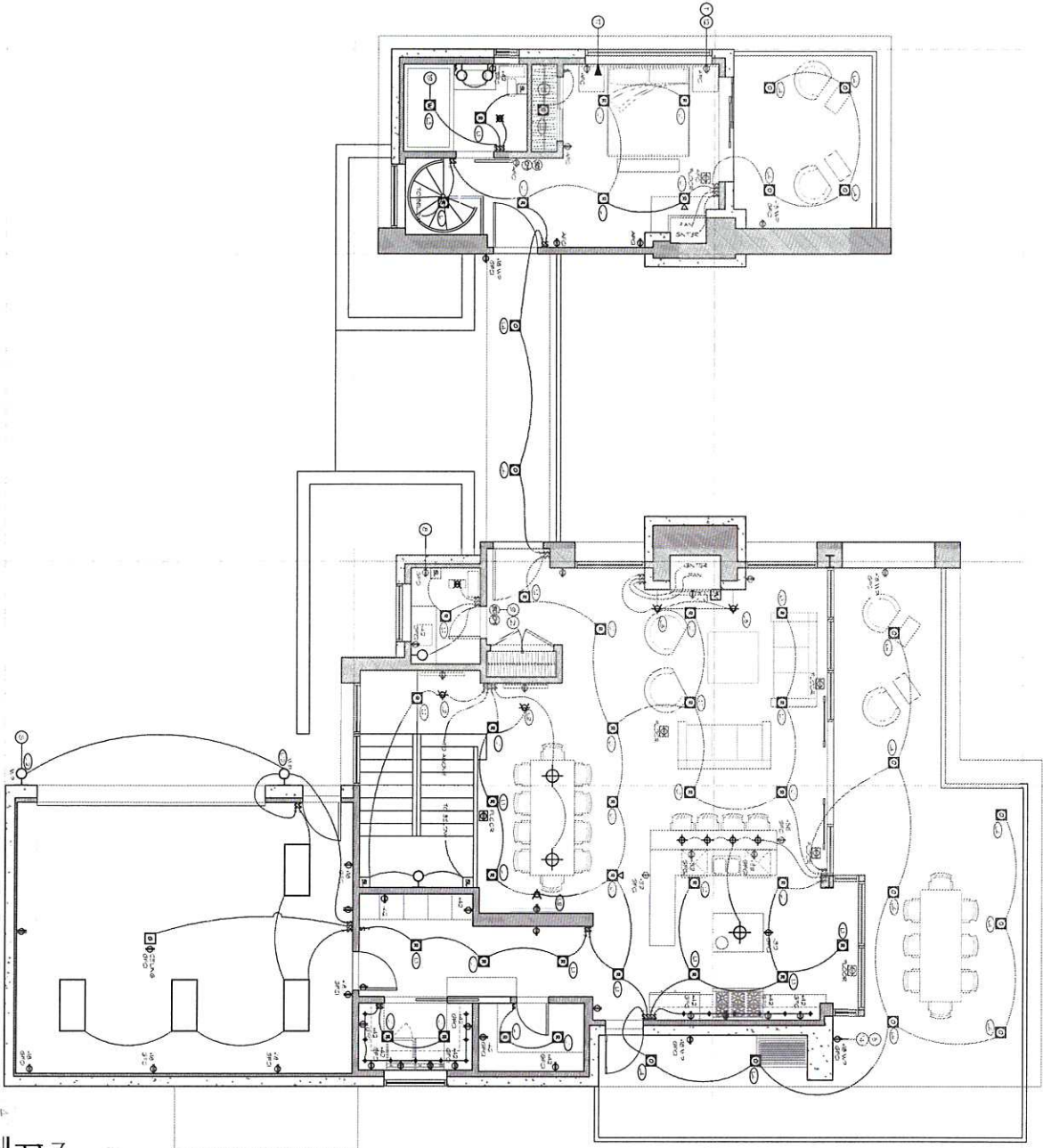
**SITE ELECTRICAL PLAN**

SCALE: 1" = 10'



ELECTRICAL LAYOUTS ARE SHOWN FOR INFORMATION ONLY. THE CONTRACTOR SHALL BE RESPONSIBLE TO COORDINATE THE LAYOUT AND INSTALLATION OF ALL ELECTRICAL WORK WITH THE ARCHITECT AND ALL OTHER TRADES.
PROVIDE MINIMUM 3" CT SEPARATION BETWEEN ALL LIGHT FIXTURES.
ALL OUTDOOR LIGHT FIXTURES TO INCLUDE WATERPROOF GFCI OUTLET.
SEE SHEET E01 FOR ELECTRICAL PROJECT NOTES AND INFORMATION.
REVISIONS:
2 JAN 2018

**Exhibit A**



MAIN LEVEL ELECTRICAL  
**PLAN**  
 SCALE: 1/4" = 1'-0"

ELECTRICAL LAYOUTS ARE SHOWN RESPONSIBLE TO COORDINATE THE LAYOUT AND INSTALLATION OF ALL RELATED ITEMS WITH EXISTING CONDITIONS AND RELATED TRADES

SEE SHEET 601 FOR ELECTRICAL PROJECT NOTES AND INFORMATION

PROVIDE AIR/FIX CL. LIGHT AS PER NOTE 601

E2.1

**UP WALL DESIGN**  
 1095 EAST HOLLYWOOD AVE. S.F.C. UT 604-485-0708

A NEW DESIGN FOR :  
**LOT 37 POWDER MOUNTAIN**  
 LOT 37 POWDER MOUNTAIN  
 WEBER COUNTY, UT

2 JAN 2018  
 ENDS/5/5  
 Page 56 of 136







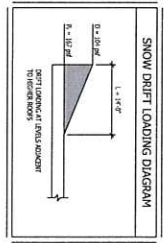






# Exhibit A

1 SECOND FLOOR FRAMING PLAN  
SCALE: 1/8" = 1'-0"



**MARKS AND SYMBOLS**

	SYSTEM NAME
	SHEET NUMBER
	FLOOR FINISHING
	FLOOR SLAB
	FLOOR JOIST
	FLOOR TRUSS
	FLOOR BEAM
	FLOOR COLUMN
	FLOOR WALL
	FLOOR WINDOW
	FLOOR DOOR
	FLOOR STAIR
	FLOOR ELEVATOR
	FLOOR MECHANICAL
	FLOOR ELECTRICAL
	FLOOR PLUMBING
	FLOOR FINISH
	FLOOR TRUSS
	FLOOR BEAM
	FLOOR COLUMN
	FLOOR WALL
	FLOOR WINDOW
	FLOOR DOOR
	FLOOR STAIR
	FLOOR ELEVATOR
	FLOOR MECHANICAL
	FLOOR ELECTRICAL
	FLOOR PLUMBING
	FLOOR FINISH

- FLOOR FRAMING PLAN NOTES**
1. SEE ARCHITECTURAL DRAWINGS FOR ALL FINISHING.
  2. VERIFY ALL FLOOR FINISHING FOR WEIGHTS, SLOPE, AND FINISHING.
  3. SET FLOOR FINISHING ON THE FINISHING AND ALL.
  4. CONSTRUCTION SHALL HAVE SLOPE AND FINISH TO MATCH ARCHITECTURAL DRAWINGS.
  5. ALL FLOOR FINISHING SHALL BE FINISHED WITH SLOPE AND FINISH TO MATCH ARCHITECTURAL DRAWINGS.
  6. VERIFY ALL FLOOR FINISHING FOR WEIGHTS, SLOPE, AND FINISHING.
  7. VERIFY ALL FLOOR FINISHING FOR WEIGHTS, SLOPE, AND FINISHING.
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  15. VERIFY ALL FLOOR FINISHING FOR WEIGHTS, SLOPE, AND FINISHING.
  16. VERIFY ALL FLOOR FINISHING FOR WEIGHTS, SLOPE, AND FINISHING.

**STRUCTURAL ENGINEERS**  
5613 S REDWOOD DR  
SALT LAKE CITY, UT 84123

S203

**UP WALL DESIGN**  
1025 EAST HOLLYWOOD AVE. S.L.C. UT (801)485-0708

A NEW DESIGN FOR :  
**LOT 37 POWDER MOUNTAIN**  
WEBER COUNTY, UT

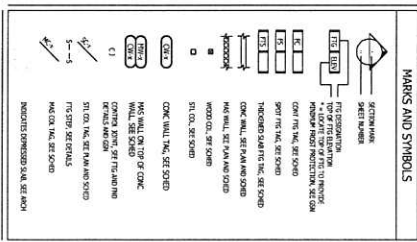
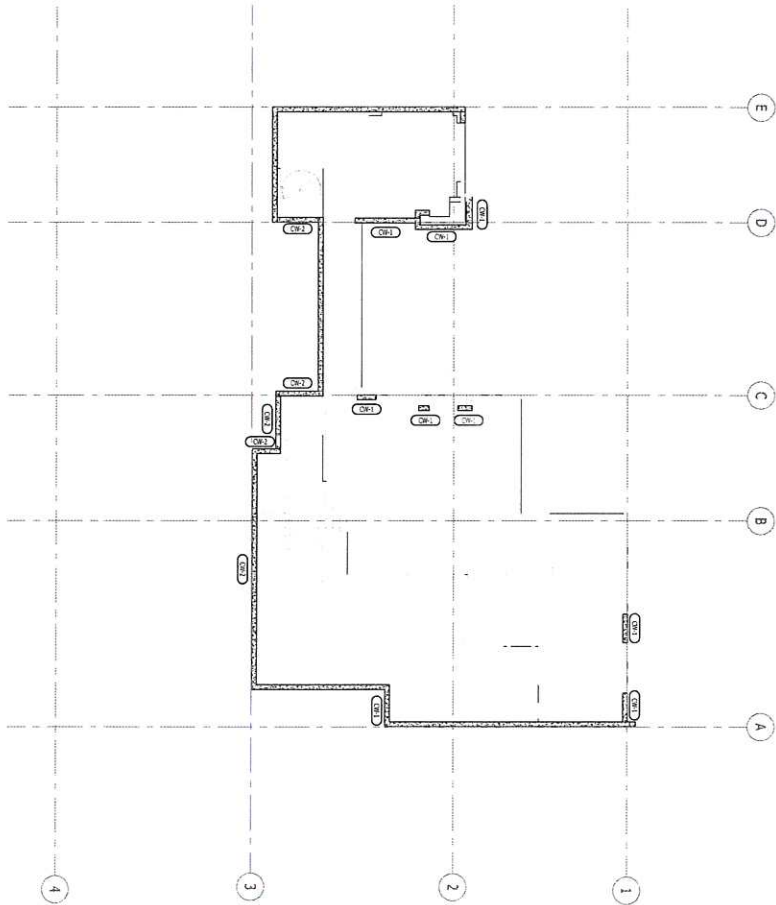
01 JUNE 2016  
REVISED





# Exhibit A

1 LOWER FLOOR SHEARWALL PLAN



- ### FOUNDATION PLAN NOTES
1. SEE ARCHITECTURAL DRAWINGS FOR ALL COMPONENTS.
  2. FOUNDATION TO BE CONCRETE ON COMPACTED GRAVEL.
  3. FOUNDATION TO BE CONCRETE ON COMPACTED GRAVEL.
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  100. FOUNDATION TO BE CONCRETE ON COMPACTED GRAVEL.



STRUCTURAL ENGINEERS  
5673 S REDWOOD DR  
SALT LAKE CITY, UT 84123

**UP WALL DESIGN**  
1025 EAST HOLLYWOOD AVE. S.L.C. UT (801)485-0708

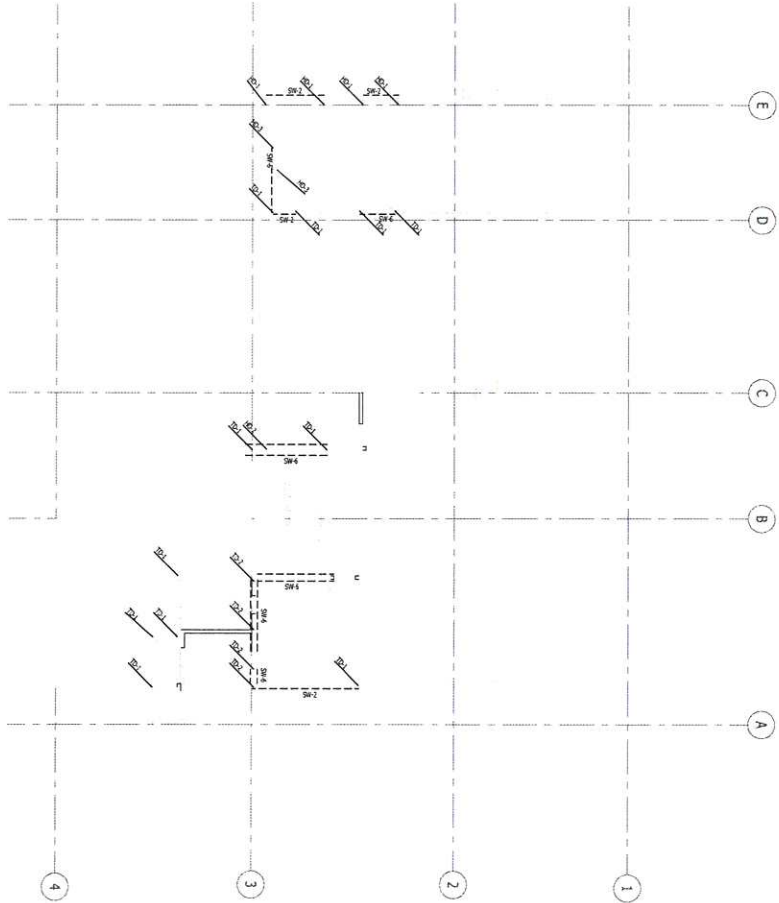
A NEW DESIGN FOR :  
**LOT 37 POWDER MOUNTAIN**  
Page 66 of 136  
LOT 37 POWDER MOUNTAIN  
WEBER COUNTY, UT

01 JUNE 2016  
REVISED



# Exhibit A

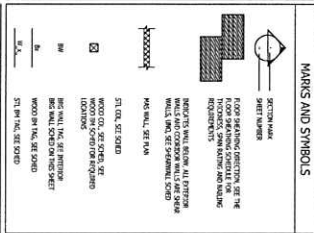
1 UPPER FLOOR SHEARWALL PLAN



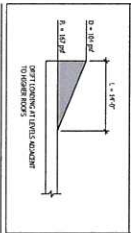
**FLOOR FRAMING PLAN NOTES**

1. REFER TO THE FOUNDATION PLAN FOR ALL FOUNDATION DETAILS.
2. REFER TO THE FOUNDATION PLAN FOR ALL FOUNDATION DETAILS.
3. REFER TO THE FOUNDATION PLAN FOR ALL FOUNDATION DETAILS.
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**MARKS AND SYMBOLS**



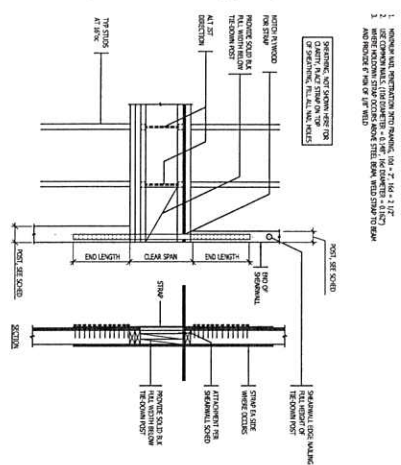
**SHOW DRIFT LOADING DIAGRAM**





### COIL STRAP TIEDOWN SCHEDULE

LINE	TYPE	REQ. QTY	GRADE	DESCRIPTION	REVISIONS	DATE
101	COIL STRAP	10	30	3/4" DIA. 30M. 48"	10/18	10/18
102	COIL STRAP	12	30	3/4" DIA. 30M. 48"	10/18	10/18



### STEEL COLUMN SCHEDULE

LINE	SIZE	STEEL GRADE	STEEL COLUMN	REMARKS
SC1	655 S40X14	A992	34' (39'-2 1/2')	
SC2	655 S40X14	A992	34' (39'-2 1/2')	
SC3	655 S40X14	A992	34' (39'-2 1/2')	
SC4	655 S40X14	A992	34' (39'-2 1/2')	
SC5	655 S40X14	A992	34' (39'-2 1/2')	
SC6	655 S40X14	A992	34' (39'-2 1/2')	

1 COIL STRAP TYPE HOLDOWN SCHEDULE

2 STEEL COLUMN SCHEDULE

1. THIS SCHEDULE CONTAINS ALL COLUMN SIZES IN ACCORDANCE WITH THE 2015 IBC AND 2015 AISC STEEL EDITION. THE SIZES LISTED ARE THE MINIMUM SIZES TO BE USED UNLESS OTHERWISE NOTED. THE SIZES LISTED ARE THE MINIMUM SIZES TO BE USED UNLESS OTHERWISE NOTED. THE SIZES LISTED ARE THE MINIMUM SIZES TO BE USED UNLESS OTHERWISE NOTED.

2. ALL COLUMN SIZES SHALL BE A992 UNLESS OTHERWISE NOTED.

3. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

4. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

5. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

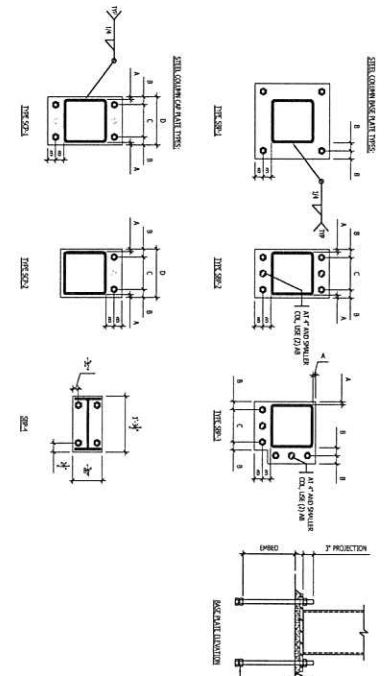
6. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

7. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

8. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

9. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.

10. ALL COLUMN SIZES SHALL BE 34' UNLESS OTHERWISE NOTED.



### EMBED PLATE CONNECTION SCHEDULE

LINE	TYPE	REQ. QTY	GRADE	DESCRIPTION	REVISIONS	DATE
101	EMBED PLATE	10	30	3/4" DIA. 30M. 48"	10/18	10/18
102	EMBED PLATE	12	30	3/4" DIA. 30M. 48"	10/18	10/18

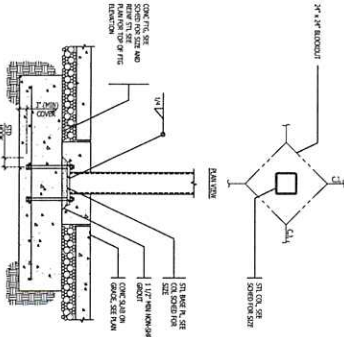
### A-325 BOLT SCHEDULE

LINE	SIZE	GRADE	DESCRIPTION	REVISIONS	DATE
B1	1/2"	A325	1/2" DIA. 30M. 48"	10/18	10/18
B2	3/8"	A325	3/8" DIA. 30M. 48"	10/18	10/18
B3	1/4"	A325	1/4" DIA. 30M. 48"	10/18	10/18
B4	5/16"	A325	5/16" DIA. 30M. 48"	10/18	10/18
B5	3/8"	A325	3/8" DIA. 30M. 48"	10/18	10/18
B6	1/2"	A325	1/2" DIA. 30M. 48"	10/18	10/18
B7	3/4"	A325	3/4" DIA. 30M. 48"	10/18	10/18
B8	1"	A325	1" DIA. 30M. 48"	10/18	10/18
B9	1 1/4"	A325	1 1/4" DIA. 30M. 48"	10/18	10/18
B10	1 1/2"	A325	1 1/2" DIA. 30M. 48"	10/18	10/18
B11	1 3/4"	A325	1 3/4" DIA. 30M. 48"	10/18	10/18
B12	2"	A325	2" DIA. 30M. 48"	10/18	10/18
B13	2 1/2"	A325	2 1/2" DIA. 30M. 48"	10/18	10/18
B14	3"	A325	3" DIA. 30M. 48"	10/18	10/18
B15	3 1/2"	A325	3 1/2" DIA. 30M. 48"	10/18	10/18
B16	4"	A325	4" DIA. 30M. 48"	10/18	10/18
B17	4 1/2"	A325	4 1/2" DIA. 30M. 48"	10/18	10/18
B18	5"	A325	5" DIA. 30M. 48"	10/18	10/18
B19	5 1/2"	A325	5 1/2" DIA. 30M. 48"	10/18	10/18
B20	6"	A325	6" DIA. 30M. 48"	10/18	10/18
B21	6 1/2"	A325	6 1/2" DIA. 30M. 48"	10/18	10/18
B22	7"	A325	7" DIA. 30M. 48"	10/18	10/18
B23	7 1/2"	A325	7 1/2" DIA. 30M. 48"	10/18	10/18
B24	8"	A325	8" DIA. 30M. 48"	10/18	10/18
B25	8 1/2"	A325	8 1/2" DIA. 30M. 48"	10/18	10/18
B26	9"	A325	9" DIA. 30M. 48"	10/18	10/18
B27	9 1/2"	A325	9 1/2" DIA. 30M. 48"	10/18	10/18
B28	10"	A325	10" DIA. 30M. 48"	10/18	10/18
B29	10 1/2"	A325	10 1/2" DIA. 30M. 48"	10/18	10/18
B30	11"	A325	11" DIA. 30M. 48"	10/18	10/18
B31	11 1/2"	A325	11 1/2" DIA. 30M. 48"	10/18	10/18
B32	12"	A325	12" DIA. 30M. 48"	10/18	10/18
B33	12 1/2"	A325	12 1/2" DIA. 30M. 48"	10/18	10/18
B34	13"	A325	13" DIA. 30M. 48"	10/18	10/18
B35	13 1/2"	A325	13 1/2" DIA. 30M. 48"	10/18	10/18
B36	14"	A325	14" DIA. 30M. 48"	10/18	10/18
B37	14 1/2"	A325	14 1/2" DIA. 30M. 48"	10/18	10/18
B38	15"	A325	15" DIA. 30M. 48"	10/18	10/18
B39	15 1/2"	A325	15 1/2" DIA. 30M. 48"	10/18	10/18
B40	16"	A325	16" DIA. 30M. 48"	10/18	10/18
B41	16 1/2"	A325	16 1/2" DIA. 30M. 48"	10/18	10/18
B42	17"	A325	17" DIA. 30M. 48"	10/18	10/18
B43	17 1/2"	A325	17 1/2" DIA. 30M. 48"	10/18	10/18
B44	18"	A325	18" DIA. 30M. 48"	10/18	10/18
B45	18 1/2"	A325	18 1/2" DIA. 30M. 48"	10/18	10/18
B46	19"	A325	19" DIA. 30M. 48"	10/18	10/18
B47	19 1/2"	A325	19 1/2" DIA. 30M. 48"	10/18	10/18
B48	20"	A325	20" DIA. 30M. 48"	10/18	10/18
B49	20 1/2"	A325	20 1/2" DIA. 30M. 48"	10/18	10/18
B50	21"	A325	21" DIA. 30M. 48"	10/18	10/18
B51	21 1/2"	A325	21 1/2" DIA. 30M. 48"	10/18	10/18
B52	22"	A325	22" DIA. 30M. 48"	10/18	10/18
B53	22 1/2"	A325	22 1/2" DIA. 30M. 48"	10/18	10/18
B54	23"	A325	23" DIA. 30M. 48"	10/18	10/18
B55	23 1/2"	A325	23 1/2" DIA. 30M. 48"	10/18	10/18
B56	24"	A325	24" DIA. 30M. 48"	10/18	10/18
B57	24 1/2"	A325	24 1/2" DIA. 30M. 48"	10/18	10/18
B58	25"	A325	25" DIA. 30M. 48"	10/18	10/18
B59	25 1/2"	A325	25 1/2" DIA. 30M. 48"	10/18	10/18
B60	26"	A325	26" DIA. 30M. 48"	10/18	10/18
B61	26 1/2"	A325	26 1/2" DIA. 30M. 48"	10/18	10/18
B62	27"	A325	27" DIA. 30M. 48"	10/18	10/18
B63	27 1/2"	A325	27 1/2" DIA. 30M. 48"	10/18	10/18
B64	28"	A325	28" DIA. 30M. 48"	10/18	10/18
B65	28 1/2"	A325	28 1/2" DIA. 30M. 48"	10/18	10/18
B66	29"	A325	29" DIA. 30M. 48"	10/18	10/18
B67	29 1/2"	A325	29 1/2" DIA. 30M. 48"	10/18	10/18
B68	30"	A325	30" DIA. 30M. 48"	10/18	10/18
B69	30 1/2"	A325	30 1/2" DIA. 30M. 48"	10/18	10/18
B70	31"	A325	31" DIA. 30M. 48"	10/18	10/18
B71	31 1/2"	A325	31 1/2" DIA. 30M. 48"	10/18	10/18
B72	32"	A325	32" DIA. 30M. 48"	10/18	10/18
B73	32 1/2"	A325	32 1/2" DIA. 30M. 48"	10/18	10/18
B74	33"	A325	33" DIA. 30M. 48"	10/18	10/18
B75	33 1/2"	A325	33 1/2" DIA. 30M. 48"	10/18	10/18
B76	34"	A325	34" DIA. 30M. 48"	10/18	10/18
B77	34 1/2"	A325	34 1/2" DIA. 30M. 48"	10/18	10/18
B78	35"	A325	35" DIA. 30M. 48"	10/18	10/18
B79	35 1/2"	A325	35 1/2" DIA. 30M. 48"	10/18	10/18
B80	36"	A325	36" DIA. 30M. 48"	10/18	10/18
B81	36 1/2"	A325	36 1/2" DIA. 30M. 48"	10/18	10/18
B82	37"	A325	37" DIA. 30M. 48"	10/18	10/18
B83	37 1/2"	A325	37 1/2" DIA. 30M. 48"	10/18	10/18
B84	38"	A325	38" DIA. 30M. 48"	10/18	10/18
B85	38 1/2"	A325	38 1/2" DIA. 30M. 48"	10/18	10/18
B86	39"	A325	39" DIA. 30M. 48"	10/18	10/18
B87	39 1/2"	A325	39 1/2" DIA. 30M. 48"	10/18	10/18
B88	40"	A325	40" DIA. 30M. 48"	10/18	10/18
B89	40 1/2"	A325	40 1/2" DIA. 30M. 48"	10/18	10/18
B90	41"	A325	41" DIA. 30M. 48"	10/18	10/18
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B92	42"	A325	42" DIA. 30M. 48"	10/18	10/18
B93	42 1/2"	A325	42 1/2" DIA. 30M. 48"	10/18	10/18
B94	43"	A325	43" DIA. 30M. 48"	10/18	10/18
B95	43 1/2"	A325	43 1/2" DIA. 30M. 48"	10/18	10/18
B96	44"	A325	44" DIA. 30M. 48"	10/18	10/18
B97	44 1/2"	A325	44 1/2" DIA. 30M. 48"	10/18	10/18
B98	45"	A325	45" DIA. 30M. 48"	10/18	10/18
B99	45 1/2"	A325	45 1/2" DIA. 30M. 48"	10/18	10/18
B100	46"	A325	46" DIA. 30M. 48"	10/18	10/18
B101	46 1/2"	A325	46 1/2" DIA. 30M. 48"	10/18	10/18
B102	47"	A325	47" DIA. 30M. 48"	10/18	10/18
B103	47 1/2"	A325	47 1/2" DIA. 30M. 48"	10/18	10/18
B104	48"	A325	48" DIA. 30M. 48"	10/18	10/18
B105	48 1/2"	A325	48 1/2" DIA. 30M. 48"	10/18	10/18
B106	49"	A325	49" DIA. 30M. 48"	10/18	10/18
B107	49 1/2"	A325	49 1/2" DIA. 30M. 48"	10/18	10/18
B108	50"	A325	50" DIA. 30M. 48"	10/18	10/18
B109	50 1/2"	A325	50 1/2" DIA. 30M. 48"	10/18	10/18
B110	51"	A325	51" DIA. 30M. 48"	10/18	10/18
B111	51 1/2"	A325	51 1/2" DIA. 30M. 48"	10/18	10/18
B112	52"	A325	52" DIA. 30M. 48"	10/18	10/18
B113	52 1/2"	A325	52 1/2" DIA. 30M. 48"	10/18	10/18
B114	53"	A325	53" DIA. 30M. 48"	10/18	10/18
B115	53 1/2"	A325	53 1/2" DIA. 30M. 48"	10/18	10/18
B116	54"	A325	54" DIA. 30M. 48"	10/18	10/18
B117	54 1/2"	A325	54 1/2" DIA. 30M. 48"	10/18	10/18
B118	55"	A325	55" DIA. 30M. 48"	10/18	10/18
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B120	56"	A325	56" DIA. 30M. 48"	10/18	10/18
B121	56 1/2"	A325	56 1/2" DIA. 30M. 48"	10/18	10/18
B122	57"	A325	57" DIA. 30M. 48"	10/18	10/18
B123	57 1/2"	A325	57 1/2" DIA. 30M. 48"	10/18	10/18
B124	58"	A325	58" DIA. 30M. 48"	10/18	10/18
B125	58 1/2"	A325	58 1/2" DIA. 30M. 48"	10/18	10/18
B126	59"	A325	59" DIA. 30M. 48"	10/18	10/18
B127	59 1/2"	A325	59 1/2" DIA. 30M. 48"	10/18	10/18
B128	60"	A325	60" DIA. 30M. 48"	10/18	10/18
B129	60 1/2"	A325	60 1/2" DIA. 30M. 48"	10/18	10/18
B130	61"	A325	61" DIA. 30M. 48"	10/18	10/18
B131	61 1/2"	A325	61 1/2" DIA. 30M. 48"	10/18	10/18
B132	62"	A325	62" DIA. 30M. 48"	10/18	10/18
B133	62 1/2"	A325	62 1/2" DIA. 30M. 48"	10/18	10/18
B134	63"	A325	63" DIA. 30M. 48"	10/18	10/18
B135	63 1/2"	A325	63 1/2" DIA. 30M. 48"	10/18	10/18
B136	64"	A325	64" DIA. 30M. 48"	10/18	10/18
B137	64 1/2"	A325	64 1/2" DIA. 30M. 48"	10/18	10/18
B138	65"	A325			

# Exhibit A

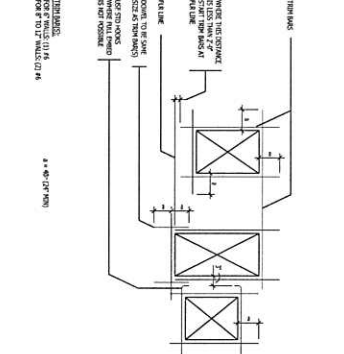
11 TYPICAL TUBE STEEL COLUMN TO CONCRETE FOOTING

NO SCALE



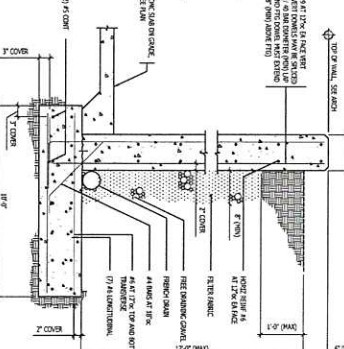
12 TYPICAL DETAILS OF TIE BARS AROUND MISCELLANEOUS CONCRETE WALL OPENINGS (I.U.O.)

NO SCALE



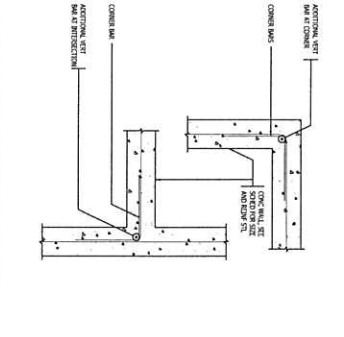
13 CONCRETE FOUNDATION WALL

NO SCALE



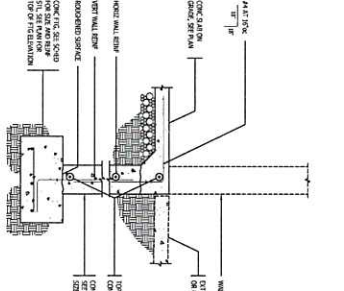
6 TYPICAL CORNER WALL REINFORCING DETAILS (PLAN VIEW)

NO SCALE



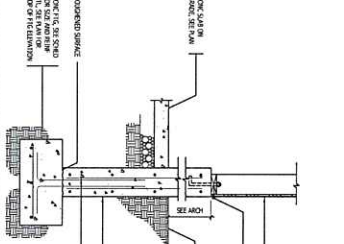
7 FOUNDATION WALL OPENING DETAIL AT DOOR

NO SCALE



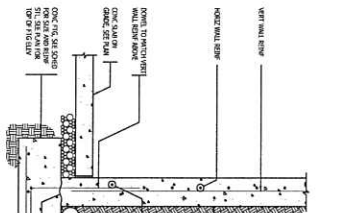
8 WOOD SHEARWALL AT CONCRETE WALL

NO SCALE



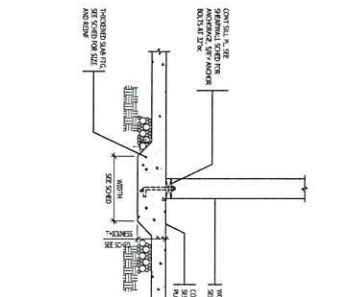
9 CONCRETE FOUNDATION WALL

NO SCALE



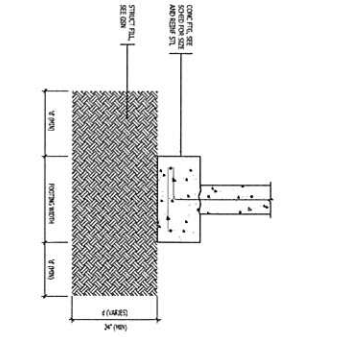
10 TYPICAL BEARING WALL AT INTERIOR FOOTING

NO SCALE



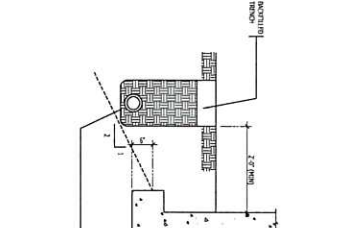
1 COMPACTED STRUCTURAL FILL

NO SCALE



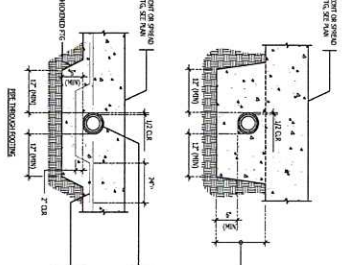
2 PIPE PARALLEL TO FOOTING DETAIL

NO SCALE



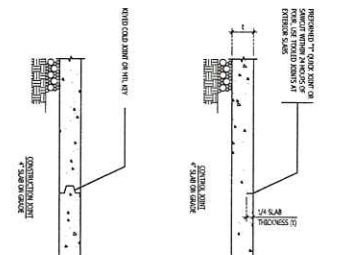
3 PIPE PERPENDICULAR TO FOOTING DETAIL

NO SCALE



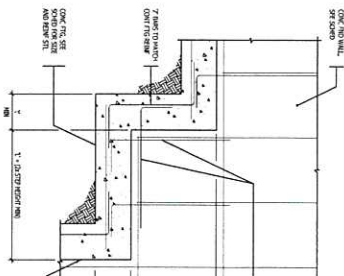
4 TYPICAL SLAB ON GRADE JOINT DETAILS

NO SCALE



5 TYPICAL CONCRETE FOOTING STEP DETAIL

NO SCALE



NJ STRUCTURAL ENGINEERS  
5613 S REDWOOD DR  
SALT LAKE CITY, UT 84123

SS01

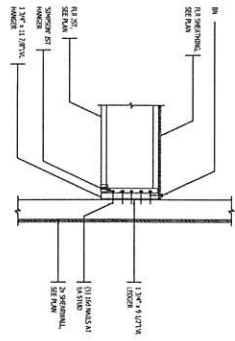
**UP WALL DESIGN**  
1025 EAST HOLLYWOOD AVE. S.L.C. UT (801)485-0708

A NEW DESIGN FOR :  
**LOT 37 POWDER MOUNTAIN**  
WEBER COUNTY, UT

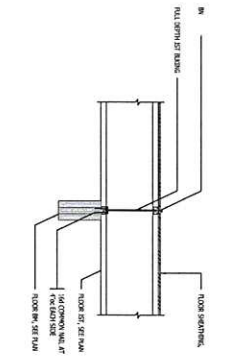
01 JUNE 2016  
REVISIONS



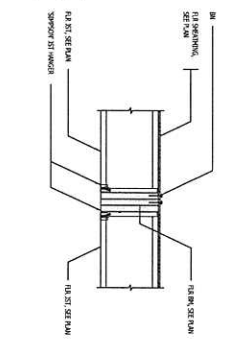
# Exhibit A



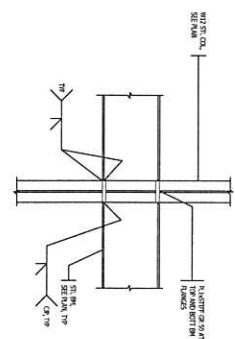
1 STAIR LANDING AT EXTERIOR WALL



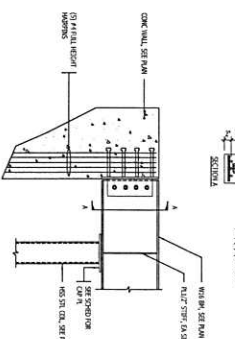
2 FLOOR JOIST AT FLOOR BEAM



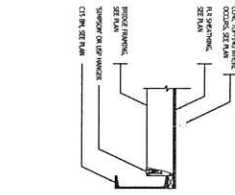
3 TYPICAL FLUSH JOIST TO BEAM CONNECTION



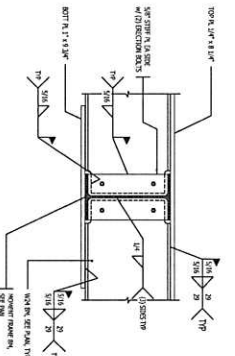
4 CANTILEVERED BEAM CONNECTION



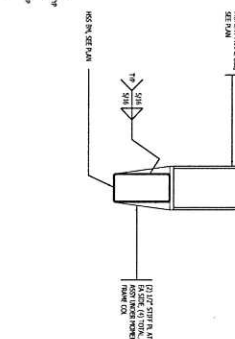
5 CANTILEVERED BEAM CONNECTION



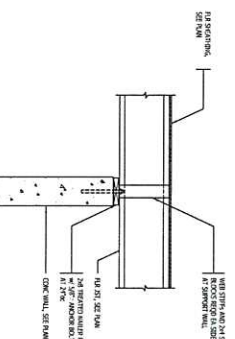
6 BRIDGE RAVING



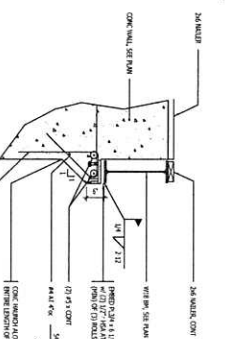
7 CANTILEVERED BEAM CONNECTION



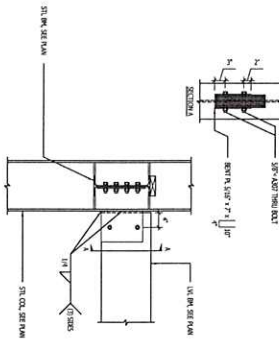
8 MOMENT FRAME SUPPORT CONNECTION



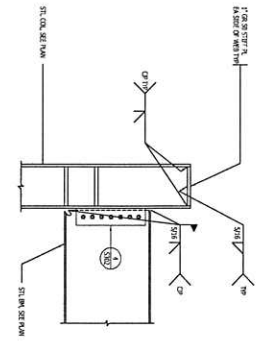
9 CANTILEVERED JOIST



10 CANTILEVERED BEAM CONNECTION



11 WOOD BEAM TO STEEL COLUMN CONNECTION



12 MOMENT FRAME CONNECTION

STRUCTURAL ENGINEERS  
5873 S REDWATER DR.  
SALT LAKE CITY, UT 84123

S602

**UP WALL**  
DESIGN  
1025 EAST HOLLYWOOD AVE. S.L.C. UT (801)485-0708

A NEW DESIGN FOR :  
LOT 37 POWDER MOUNTAIN  
WEBER COUNTY, UT

Page 74 of 136

01 JUNE 2016  
RS-150305-5  


**Exhibit A**

**U P W A L L                      D E S I G N**  
**A R C H I T E C T**  
1025 EAST HOLLYWOOD AVENUE SALT LAKE CITY, UTAH 84105 (801) 485-0708 FAX(801) 48

21 July, 2016

Weber County Building Department  
2380 Washington Blvd., Suite 240  
Ogden, UT 84401

Re: Lot 37 Powder Mountain 2015 Code Review

Dear Sir or Madam,

As of July 1st, Utah has adopted the 2015 series of codes from the ICC. Upon studying the residence located on lot 37 of Powder Mountain. I have determined that the project is in compliance with the code with the following revision;

A Carbon Monoxide Detector will be required outside the guest suite adjacent to the boot room on the lower level and outside the master suite on the upper level.

If you have any questions, please contact me.

Sincerely

*Josh Arrington*  
Josh Arrington, Architect  
Upwall Design









TITLE: \_\_\_\_\_

SNOW LOAD

$$P_g = \sqrt{P_o^2 + S^2(A - A_o)^2}$$

$P_o = 43$  WEEBEE COUNTRY

$S = 63$

$A = 8.6$

$A_o = 4.5$

$$= \sqrt{43^2 + 63^2(8.6 - 4.5)^2}$$

$P_g = 265 \text{ psf}$

$P_s = 0.7 C_e C_t I_s P_g$

$C_e = 0.9$  (EXPOSURE, FULL EXPOSED)

$C_t = 1.0$

$I_s = 1.0$

$= 0.7(0.9)(1.0)(1.0)(265)$

$= 167 \text{ psf}$

DRIFTING ON LOWER ROOFS

$h_d = 0.43 \sqrt{L_u + \sqrt{P_g + 10}} - 1.5$

$0.43 \sqrt{23 + \sqrt{275}} - 1.5$

$= 3.48 \text{ ft}$

$P_d = L_u \delta = 3.48 \left( 0.13 \times 265 + 14 \right)$   $< 30$

Width  $= 4h_d = 4(3.48) = 13.9 \rightarrow 14 \text{ ft}$





TITLE: \_\_\_\_\_

MASTER BEAM WALL LINE A

ROOF LOAD  $12 \text{ psf} \times 1 \text{ ft TRIB} = 12 \text{ plf}$

WALL LOAD  $12 \text{ psf} \times 11 \text{ ft TALL} = 132 \text{ plf}$

SNOW LOAD  $167 = 1 \text{ ft TRIB} = 167 \text{ plf}$

$DL = 144 \text{ plf} \times 16'' = 192$

$SL = 167 \text{ plf} \times 16'' = 227$

BEAM @ 3<sup>RD</sup> FLOOR

$DL = 25 \text{ psf} \times \frac{5'}{2} = 63 \text{ plf}$

$LL = 40 \text{ psf} \times \frac{5'}{2} = 100 \text{ plf}$

MASTER BEAM WALL LINE A.2

ROOF LOAD  $18 \text{ psf} \times 1 \text{ ft TRIB}$

WALL LOAD  $12 \text{ psf} \times 11 \text{ ft TALL}$

$DL = 144 \text{ plf}$

$SL = 167 \text{ plf}$

GREEN ROOF LOAD  $142 \text{ psf} \times 1 \text{ ft TRIB}$

SNOW LOAD  $167 + 104 = 271 \text{ psf} \times 1 \text{ ft}$

BEAM LOAD  $DL = 25 \text{ psf} \times 3 \text{ ft TRIB} = 75 \text{ plf}$

$LL = 40 \text{ psf} \times 3 = 120 \text{ plf}$

$DL = 351 \text{ plf}$

$LL = 120$

$SL = 438 \text{ plf}$



TITLE:

<p>MASTER BORM WALL W/AVE 3,5 FROM A-B 23'-0 w/ 0'-8'</p>	<p>ROOF DL = <math>142 \text{ psf} \times 13\frac{1}{2}' \text{ TAB} = 1917 \text{ plf DL}</math></p>	
	<p>SL = <math>167 \text{ psf} \times 6' + 271 \text{ psf} \times 7\frac{1}{2}' = 3035 \text{ plf SL}</math></p>	
	<p>LL = <math>20 \times 13\frac{1}{2} = 270 \text{ plf LL}</math></p>	
<p>8'-16'6</p>	<p>ROOF DL = <math>142 \text{ psf} \times 8' \text{ TAB} = 1136 \text{ plf DL}</math></p>	
	<p>SL = <math>1825 \text{ plf} + 271 + 2' = 2367 \text{ plf SL}</math></p>	
	<p>LL = <math>20 \text{ plf} \times 8' = 160 \text{ plf LL}</math></p>	
<p>16'-6-23'</p>	<p>L. ROOF DL = <math>12 \text{ psf} \times 7\frac{1}{2}' \text{ TAB} = 90 \text{ plf}</math> WALL DL = <math>12 \text{ plf} \times 11' \text{ TALL} = 132 \text{ plf}</math></p>	<p>DL = 1099 plf</p>
	<p>L. ROOF DL = <math>142 + 6' \text{ TAB} = 852 \text{ plf}</math> FLOOR DL = <math>25 \text{ psf} \times 1' \text{ TAB} = 25 \text{ plf}</math></p>	<p>SL = 3078 plf</p>
	<p>SL ROOF = <math>167 \text{ psf} \times 7\frac{1}{2}' \text{ TAB} = 1253 \text{ plf}</math> SL WALL = <math>1825 \text{ plf}</math></p>	<p>LL = 310 plf</p>
	<p>LL ROOF = <math>20 \text{ psf} \times 7\frac{1}{2}' \text{ TAB} = 150 \text{ plf}</math> LL L. ROOF = <math>20 \text{ psf} \times 6' \text{ TAB} = 120 \text{ plf}</math> LL FLOOR = <math>40 \text{ psf} \times 1' \text{ TAB} = 40</math></p>	<p>DL = 241 plf</p>
<p>23'-28'</p>	<p>ROOF DL = 90 plf WALL DL = 132 plf FLOOR DL = 25 plf</p>	<p>SL ROOF = 1253 plf SL WALL = 1825 plf SL FLOOR = 190 plf</p>
	<p>LL ROOF = 150 plf LL FLOOR = 40 plf</p>	<p>LL = 190 plf</p>





STRUCTURAL ENGINEERS


SHEET NUMBER: \_\_\_\_\_

JOB NUMBER: \_\_\_\_\_

DATE: \_\_\_\_\_

BY: \_\_\_\_\_

TITLE: \_\_\_\_\_

GARAGE DOOR HEADER	18' long	
		$P = 42351b$ DL $339971b$ SL
CONC BEAM 27" TALL	8" THICK	$W = 142 \times 1 = 142 pl$ $167 \times 1 = 167 pl$
$d = 25"$		$W_D = \frac{150(27+8)}{144} = 225$
$M = 289.98$ k-ft		
	$A_s = \frac{M}{f_d} = \frac{289.98}{4(87)} = 2.9 in^2 \rightarrow$	



TITLE:

CANTILEVERED BEAM ON GRID E - 2ND LEVEL	
	$Dis = 39943 \text{ lb}$ $KL = 12$ $P_{allow} = 112k \rightarrow H956 \times 6$
$1.2D + 1.6S$ $= 1.2(13112) + 1.6(17955) = 44462 \text{ lb}$	
BOLTS: USE 4 A325 $7/8"$ $V = 4(24.3) = 97.2k > 44.5k$	
WELDS: $0.75(616)(70)(1/4)(\sqrt{2})(12") = 66.82k > 44.5$	
NELSON STUDS: $51000 \text{ psi}$	$\frac{44462}{51000} = 0.87 \text{ in}^2 \text{ REQ'D}$
	$6 \text{ STUDS} = \frac{0.87}{6} = 0.145 \text{ in}^2$
	USE (3) $1/2" \times 6 \text{ LSA'S}$
SUPPLEMENTARY REINF	
$0.9(60 \text{ ksi}) = 54000 \text{ lb}$	
$A_s = \frac{44462}{54000} = 0.82 \text{ in}^2$	$\text{No. of bars} = \frac{0.82}{0.2} = 4$



# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	143
Date:	5/31/
By:	B

Blue Cells Must be Entered Manually

WOOD BEAMS Species Designation Description	STEEL W10X22 W-FLANGE Beam 6		STEEL W10X22 W-FLANGE Beam 7		STEEL W10X22 W-FLANGE Beam 8		WOOD 1 1/2" TJI 360 TJI Res Joist Beam 9		WOOD (1) 1 3/4" x 11 7/8" LVL (1) 1 3/4" x 11 7/8" LVL Beam 10		STEEL Section Design Descr
	Roof level - North Section - North Cantilevered Beam		Roof level - North Section - South Cantilevered Beam		Roof level - North Section - South Cantilevered Beam - on Grid C		Roof Level - Main Bldg - South Span Joists		Roof Level - Guest House - Joists		
$L_{Left\_Span}$ (ft) $L_{Center\_Span}$ (ft) $L_{Right\_Span}$ (ft) $L_L$ (ft)   $Auto$ (ft) Beam Slope   $\alpha$	13.25 6.75	13.25 6.75	13.25 6.75	13.25 6.75	4.75 6.75	4.75 6.75	9.00	9.00	15.50 1.25	15.50 1.25	$L_{Left\_Span}$ $L_{Center\_Span}$ $L_{Right\_Span}$ $L_L$ (ft) Beam S
Include Self Wt. $\gamma_{Wood}$ (lb/ft <sup>3</sup> )   $w_{Self}$ (lb/ft)	Yes 488.1	Yes 488.1	Yes 488.1	Yes 488.1	Yes 488.1	Yes 488.1	No	No	No	No	Include $\gamma_{Steel}$ (lb/ft <sup>3</sup> )
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> ) Trib Width (ft)   $Auto$ Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	178.0 1.00 2475.0	178.0 1.00 2475.0	159.0 1.00 2213.0	159.0 1.00 2213.0	54.0 1.00 752.0	54.0 1.00 752.0	12.0 1.33 167.0	12.0 1.33 167.0	12.0 1.00 167.0	12.0 1.00 167.0	PSF <sub>DL</sub>   PS Trib Width Factored P
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> ) Trib Width (ft)   $Auto$ Start   End Dist frm Left Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											PSF <sub>DL</sub>   PS Trib Width Start   End I Factored P
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> ) Trib Width (ft)   $Auto$ Start   End Dist frm Left Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											PSF <sub>DL</sub>   PS Trib Width Start Dist Factored P
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> ) Trib Width (ft)   $Auto$ Max at L or R   $Auto$ Start   End Dist frm Left Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Incr PSF <sub>DL</sub>   F Trib Width Max at L c Start   End I Factored In
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> ) Trib Width (ft)   $Auto$ Max at L or R   $Auto$ Start   End Dist frm Left Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Incr PSF <sub>DL</sub>   F Trib Width Max at L c Start   End I Factored In
Pt 1 Dead   Live (lbs) Dist from Left   $Auto$ Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Pt 1 Dead Dist from Factored f
Pt 2 Dead   Live (lbs) Dist from Left   $Auto$ Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Pt 2 Dead Dist from Factored f
Pt 3 Dead   Live (lbs) Dist from Left   $Auto$ Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Pt 3 Dead Dist from Factored f
$C_D$   $C_r$ $C_t$   $C_i$	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.15 1.00	1.00 1.00	1.15 1.00	1.00 1.00	$C_D$   I D.N D.N
Wet Use (Y/N)?							No	No	No	No	D.N D.N
$F_v$ (psi)   $f_v$ (psi) $V_{ALL}$   $1.5V_{max}$ (kip) Shear Chk	2.45 48.96 45.6%	1.50 22.32 45.6%	2.45 48.96 40.8%	1.50 19.98 40.8%	2.45 48.96 12.1%	1.50 5.94 12.1%	300.69 2.94 54.8%	164.66 1.61 54.8%	327.75 6.81 30.8%	100.78 2.09 30.8%	$A_w$ (in <sup>2</sup> ) $V_r/\Omega$   V Shear
$F'_{b,TT}$   $F'_{b,CT}$ (psi) $S$ (in <sup>3</sup> )   $I_x$ (in <sup>4</sup> ) $M_{ALL}$ (k*ft) +   - $M_{max}$ (k*ft) +   - Bending Chk	50 26.00 64.87 32.19 49.6%	1.67 118.0 64.87 60.94 93.9%	50 26.00 64.87 28.81 44.4%	1.67 118.0 64.87 54.54 84.1%	50 26.00 64.87 0.00 0.0%	1.67 118.0 64.87 18.86 29.1%	2532 33.69 7.11 2.42 34.0%	2531.54 200.0 7.11 0.00 0.0%	2947 41.13 10.10 5.31 52.5%	2947.04 244.2 10.10 0.14 1.4%	$F_y$ (KS) $Z_x$ (in <sup>3</sup> ) $M_r/\Omega$ (k* $M_{max}$ (k* Bending
Max LL   TL $\Delta$ Ratio Allowable LL   TL $\Delta$	L/ 360	L/ 240	L/ 360	L/ 240	L/ 360	L/ 240	L/ 360	L/ 240	L/ 240	L/ 238	Max LL   I Allowable
$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in) $\Delta_{Live\_Cntr}$   $\Delta_{Tot\_Cntr}$ (in) $\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in) Actual LL   TL $\Delta$ Ratio	0.20 0.36	0.21 0.38	0.18 0.32	0.19 0.34	0.01 0.18	0.01 0.20	0.12 0.13	0.13 0.13	0.46 0.12	0.49 0.13	$\Delta_{Live\_Left}$   I $\Delta_{Live\_Cntr}$   I $\Delta_{Live\_Cant}$   I Actual LL   I
$R_L$ (lbs) $R_C$ (lbs) $R_R$ (lbs)	13123 981 12142	981 12142	11744 888 10856	888 10856	-2005 -184 -1821	-184 -1821	1074 72 1002	72 1002	1378 92 1286	92 1286	$R_L$ (lbs) $R_C$ (lbs) $R_R$ (lbs)
$F'_{C\_Perp}$ (psi)   Brg Chk Req'd Brg L   Brg Cap Req'd Brg C   Brg Cap Req'd Brg R   Brg Cap	DNA DNA DNA	DNA DNA DNA	DNA DNA DNA	DNA DNA DNA	DNA DNA DNA	DNA DNA DNA	0 1 3/4" 1 3/4"	99.4% 1080.0 1080.0	750 1 1/4" 1 1/4"	DNA DNA DNA	D.N D.N D.N D.N
Reactions are Service Level # Pls   Span Depth	Adequate		Adequate		Adequate		Adequate		Adequate		Reactions are Shape   S
Nailing Requirements (If More Than 1 PLY) Or Bearing Requirements (I-Joist Only)	DNA		DNA		DNA		LT: 1 3/4" Min End Brg, RT: 1 3/4" Min End Brg, Web Stiffn's Req'd at All Conc Loads		None Required		D.N
Query Location   Type Query Result	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	Location Query

# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	141
Date:	5/31/
By:	B

Blue Cells Must Be Entered Manually

	WOOD		WOOD		WOOD		WOOD		WOOD		STEEL
WOOD BEAMS	14" BCI 5000		(2) 1 3/4" x 14" LVL		(3) 1 3/4" x 14" LVL		(3) 1 3/4" x 14" LVL		14" BCI 5000		STEEL
Species	BCI Joist		LVL 2-DE FB-280G		LVL 1-3E FB-260G		LVL 1-3E FB-260G		BCI Joist		Section
Designation	Beam 16		Beam 17		Beam 18		Beam 19		Beam 20		Design
Description	Third Level - Main Bldg - Master Cantilevered Joists		Third Level - Main Bldg - Master Bdrm - E/W short wall support beam		Third Level - Main Bldg - Master Bdrm - N/S wall support beam		Third Level - Main Bldg - Master Bdrm - E/W long wall support beam		Third Level - Main Bldg - Floor joists North of Stairs		Descr
L <sub>Left_Span</sub> (ft)											L <sub>Left_Span</sub>
L <sub>Center_Span</sub> (ft)	15.00		4.00		15.00		15.00		15.00		L <sub>Center_Span</sub>
L <sub>Right_Cant</sub> (ft)	5.00										L <sub>Right_Cant</sub>
L <sub>u</sub> (ft)   Auto (ft)	1.0		1.0		1.0		1.0		1.0		L <sub>b</sub> (ft)
Beam Slope   α	0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		Beam Slope
Include Self Wt.	No		No		No		No		No		Include
w <sub>wood</sub> (lb/ft <sup>3</sup> )   w <sub>self</sub> (lb/ft <sup>3</sup> )											w <sub>steel</sub> (lb/ft <sup>3</sup> )
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	25.0 40.0		351.0 438.0		507.0 1461.0		473.5 568.5		20.0 40.0		PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   Auto	1.33		1.00		1.0		1.00		1.33		Trib Width
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	33.3 53.3		351.0 438.0		507.0 1461.0		473.5 568.5		26.7 53.3		Factored PLF
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )					507.0 1461.0						PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   Auto					1.0						Trib Width
Start   End Dist frm Left					0.00 8.5						Start   End Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>					507.0 1461.0						Factored PLF
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )					33.3 53.0						PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   Auto					8.5 15.0						Trib Width
Start   End Dist frm Left					8.5 15.0						Start Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>					33.3 53.0						Factored PLF
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L or R
Start   End Dist frm Left											Start   End Dist
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored Incr
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L or R
Start   End Dist frm Left											Start   End Dist
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored Incr
Pt 1 Dead   Live (lbs)	192.0 233.0				702.0 876.0						Pt 1 Dead   Live
Dist from Left   Auto	20.00				8.50						Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>	192.0 233.0				702.0 876.0						Factored PT
Pt 2 Dead   Live (lbs)											Pt 2 Dead   Live
Dist from Left   Auto											Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored PT
Pt 3 Dead   Live (lbs)											Pt 3 Dead   Live
Dist from Left   Auto											Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored PT
C <sub>b</sub>   C <sub>t</sub>	1.15 1.00		1.15 1.00		1.15 1.00		1.00 1.00		1.00 1.00		C <sub>b</sub>   C <sub>t</sub>
C <sub>t</sub>   C <sub>b</sub>	1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		C <sub>t</sub>   C <sub>b</sub>
Wet Use (Y/N)?											D.N
F <sub>v</sub> (psi)   F <sub>r</sub> (psi)	353.47 145.47		327.75 48.31		327.75 261.10		285.00 159.49		307.37 101.03		A <sub>v</sub> (in <sup>2</sup> )
V <sub>ALL</sub>   1.5V <sub>max</sub> (kip)	3.15 1.30		16.06 2.37		24.09 19.19		20.95 11.72		2.74 0.90		V <sub>r</sub> /Ω   V
Shear Chk	41.2%		14.7%		79.7%		56.0%		32.9%		Shear
F <sub>b,TT</sub>   F <sub>b,CT</sub> (psi)	1518 1518.17		3153 3152.94		2923 2923.21		2542 2542.47		1320 1320.14		F <sub>y</sub> (ksi)
S (in <sup>3</sup> )   I <sub>x</sub> (in <sup>4</sup> )	33.95 237.7		114.33 800.3		171.50 1200.5		171.50 1200.5		33.95 237.7		Z <sub>x</sub> (in <sup>3</sup> )
M <sub>ALL</sub> (k*ft) +   -	4.30 4.30		30.04 30.04		41.78 41.78		36.34 36.34		3.74 3.74		M <sub>u</sub> /Ω (k*ft)
M <sub>max</sub> (k*ft) +   -	1.10 3.21		1.58 0.00		41.59 0.00		29.31 0.00		2.25 0.00		M <sub>max</sub> (k*ft)
Bending Chk	25.5% 74.7%		5.3% 0.0%		99.5% 0.0%		80.7% 0.0%		60.2% 0.0%		Bending
Max LL   TL Δ Ratio	L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		Max LL   TL Δ
Allowable LL   TL Δ											Allowable
Δ <sub>Live,Left</sub>   Δ <sub>Tot,Left</sub> (in)	0.05 0.07		0.00 0.00		0.50 0.70		0.28 0.52		0.17 0.26		Δ <sub>Live,Left</sub>   Δ <sub>Tot,Left</sub>
Δ <sub>Live,Cent</sub>   Δ <sub>Tot,Cent</sub> (in)	0.12 0.24										Δ <sub>Live,Cent</sub>   Δ <sub>Tot,Cent</sub>
Δ <sub>Live,Cant</sub>   Δ <sub>Tot,Cant</sub> (in)											Δ <sub>Live,Cant</sub>   Δ <sub>Tot,Cant</sub>
Actual LL   TL Δ Ratio	L/ 970 L/ 491		L/ 30454 L/ 16906		L/ 360 L/ 259		L/ 634 L/ 346		L/ 1036 L/ 691		Actual LL   TL Δ
R <sub>L</sub> (lbs)	436 158 278		1578 702 876		12794 3440 9354		7815 3551 4264		600 200 400		R <sub>L</sub> (lbs)
R <sub>C</sub> (lbs)											R <sub>C</sub> (lbs)
R <sub>R</sub> (lbs)	1722 700 1022		1578 702 876		6073 1789 4285		7815 3551 4264		600 200 400		R <sub>R</sub> (lbs)
F <sub>C,Perp</sub> (psi)   Brg Chk	0 99.8%		750 DNA		750 DNA		750 DNA		0 63.1%		D.N
Req'd Brg L   Brg Cap	1 3/4" 950.0		3/4" DNA		3 1/4" DNA		2 " DNA		1 3/4" 950.0		D.N
Req'd Brg C   Brg Cap											D.N
Req'd Brg R   Brg Cap	3 1/2" & WS 1725.0		3/4" DNA		1 3/4" DNA		2 " DNA		1 3/4" 950.0		D.N

Reactions are Service Level

# Pkys | Span/Depth

Nailing Requirements (If More Than 1 PLY) Or Bearing Requirements (I-Joist Only)

LT: 1 3/4" Min End Brg. RT: 3 1/2" Min End Brg & Web Stiffeners. Web Stiffn'r's Req'd at All Conc Loads

(3) Rows of 12d or 16d (0.128" x 3" Min) Nails @ 12" O.C. 4" Edge Distance

(4) Rows of 12d or 16d (0.128" x 3" Min) Nails @ 12" O.C. 4" Edge Distance. Alternate Rows Through Both Outside Faces.

(3) Rows of 12d or 16d (0.128" x 3" Min) Nails @ 12" O.C. 4" Edge Distance. Alternate Rows Through Both Outside Faces.

LT: 1 3/4" Min End Brg. RT: 1 3/4" Min End Brg. Web Stiffn'r's Req'd at All Conc Loads

Reactions are

Shape: I S

D.N

Query

Location | Type

Query Result

2006 NDS Wood AISC Steel Beam Design v 5.13

by B. Saxey

10:36

B



# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	141
Date:	5/31/
By:	B

Blue Cells Must be Entered Manually

	WOOD		WOOD		WOOD		WOOD		WOOD		STEEL
WOOD BEAMS	14" BCI 5000		14" BCI 60		14" BCI 90		(2) 1 3/4" x 14" LVL		16" BCI 90		STEEL
Species	BCI Joist		BCI Joist		BCI Joist		LVL 2.0E FB 2800		BCI Joist		Section
Designation	Beam 26		Beam 27		Beam 28		Beam 29		Beam 30		Design
Description	Third Level - Guest House - Interior Floor Joists		Third Level - Guest House - Exterior Floor Joists		Third Level - Guest House - Exterior Floor Joists with max snow drift		Third Level - Guest House - Header near grid 2		Third Level - Main Bldg - Exterior Floor Joists - 4" soil		Descr
$L_{Left\_Span}$ (ft)											$L_{Left\_Sp}$
$L_{Center\_Span}$ (ft)	15.00		15.00		15.00		15.00		15.50		$L_{Center\_f}$
$L_{Right\_Span}$ (ft)											$L_{Right\_c}$
$L_L$ (ft)   Auto (ft)	1.0		1.0		1.0		1.0		1.0		$L_b$ (ft)
Beam Slope   $\alpha$	0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0.0°		Beam S
Include Self Wt.	1										Include
$\gamma_{wood}$ (lb/ft <sup>3</sup> )   $w_{self}$ (lb/ft)											$\gamma_{steel}$ (lb/ft <sup>3</sup> )
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	20.0 40.0		50.0 167.0		50.0 271.0		50.0 197.0		60.0 167.0		PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto	1.33		1.00		0.75		0.75		1.33		Trib Width
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	26.7 53.3		50.0 167.0		37.5 203.3		37.5 147.8		80.0 222.6		Factored P!
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto											Trib Width
Start   End Dist from Left											Start   End I
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											Factored P!
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto											Trib Width
Start   End Dist from Left											Start Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											Factored P!
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   F
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L c
Start   End Dist from Left											Start   End I
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored In
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   F
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L c
Start   End Dist from Left											Start   End I
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored In
Pt 1 Dead   Live (lbs)											Pt 1 Dead
Dist from Left   Auto											Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored I
Pt 2 Dead   Live (lbs)											Pt 2 Dead
Dist from Left   Auto											Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored I
Pt 3 Dead   Live (lbs)											Pt 3 Dead
Dist from Left   Auto											Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored I
$C_D$   $C_r$	1.00 1.00		1.15 1.00		1.15 1.00		1.00 1.00		1.00 1.00		$C_b$   I
$C_t$   $C_i$	1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		D.N
Wet Use (Y/N)?											D.N
$F_v$ (psi)   $f_r$ (psi)	307.37 101.03		300.17 220.68		277.18 185.19		285.00 42.53		248.78 228.79		$A_v$ (in <sup>2</sup> )
$V_{ALL}$   $1.5V_{max}$ (kip)	2.74 0.90		3.32 2.44		4.05 2.71		13.97 2.08		3.83 3.52		$V_r/\Omega$   V
Shear Chk	32.9%		73.5%		66.8%		14.9%		92.0%		Shear
$F'_{b,TT}$   $F'_{b,CT}$ (psi)	1320 1320.14		2290 2289.66		2425 2425.01		2743 2743.18		2012 2012.43		$F_y$ (ksi)
$S$ (in <sup>3</sup> )   $I_x$ (in <sup>4</sup> )	33.95 237.7		44.84 313.9		64.82 453.7		114.33 800.3		77.82 622.5		$Z_x$ (in <sup>3</sup> )
$M_{ALL}$ (k*ft) +   -	3.74 3.74		8.56 8.56		13.10 13.10		26.14 26.14		13.05 13.05		$M_r/\Omega$ (k*
$M_{max}$ (k*ft) +   -	2.25 0.00		6.10 0.00		6.77 0.00		5.21 0.00		9.09 0.00		$M_{max}$ (k*
Bending Chk	60.2% 0.0%		71.3% 0.0%		51.7% 0.0%		19.9% 0.0%		69.6% 0.0%		Bending
Max LL   TL $\Delta$ Ratio	L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 240 L/ 240		Max LL   T
Allowable LL   TL $\Delta$											Allowable
$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in)											$\Delta_{Live\_Left}$   i
$\Delta_{Live\_Cntr}$   $\Delta_{Tot\_Cntr}$ (in)	0.17 0.26		0.36 0.46		0.31 0.37		0.11 0.13		0.30 0.41		$\Delta_{Live\_Cntr}$   i
$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in)											$\Delta_{Live\_Cant}$   i
Actual LL   TL $\Delta$ Ratio	L/ 1036 L/ 691		L/ 506 L/ 389		L/ 572 L/ 483		L/ 1712 L/ 1365		L/ 624 L/ 459		Actual LL
$R_L$ (lbs)	$R_{L,DL}$ 600 $R_{L,LL}$ 200 400		1628 375 1253		1806 281 1524		1389 281 1108		2345 620 1725		$R_L$ (lbs)
$R_C$ (lbs)	$R_{C,DL}$ $R_{C,LL}$										$R_C$ (lbs)
$R_R$ (lbs)	$R_{R,DL}$ 600 $R_{R,LL}$ 200 400		1628 375 1253		1806 281 1524		1389 281 1108		2345 620 1725		$R_R$ (lbs)
$F'_{C\_Perp}$ (psi)   Brg Chk	0 63.1%		0 94.3%		0 92.6%		750 DNA		0 99.8%		D.N
Req'd Brg L   Brg Cap	1 3/4" 950.0		3 1/2" & WS 1725.0		1 3/4" & WS 1950.0		3/4 " DNA		3 1/2" & WS 2350.0		D.N
Req'd Brg C   Brg Cap											D.N
Req'd Brg R   Brg Cap	1 3/4" 950.0		3 1/2" & WS 1725.0		1 3/4" & WS 1950.0		3/4 " DNA		3 1/2" & WS 2350.0		D.N

Reactions are Service Level  
# Phys | Span/Depth

1 12.86  
Nailing Requirements (If More Than 1 PLY) Or Bearing Requirements (I-Joist Only)

1 12.86  
LT: 1 3/4" Min End Brg & Web Stiffeners. RT: 3 1/2" Min End Brg & Web Stiffeners. Web Stiffener's Req'd at All Conc Loads

1 12.86  
LT: 1 3/4" Min End Brg & Web Stiffeners. RT: 1 3/4" Min End Brg & Web Stiffeners. Web Stiffener's Req'd at All Conc Loads

2 12.86  
(3) Rows of 12d or 16d (0.128" x 3" Min) Nails @ 12" O.C. 4" Edge Distance

1 11.63  
LT: 3 1/2" Min End Brg & Web Stiffeners. RT: 3 1/2" Min End Brg & Web Stiffeners. Web Stiffener's Req'd at All Conc Loads

Reactions are Shape 1 S

D.N

Query  
Location | Type  
Query Result

DESIGN	DESIGN	DESIGN	DESIGN	DESIGN

Location  
Query

2006 NDS Wood AISC Steel Beam Design v 5.13

by B. Saxey

16:36

B

# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	143
Date:	5/31/
By:	B

Blue Cells Must be Entered Manually

	STEEL		STEEL		STEEL		WOOD		STEEL		STEEL
WOOD BEAMS	W18X60		W21X132		W18X40		14" BCI 5000		W16X40		STEEL
Species	W-FLANGE		W-FLANGE		W-FLANGE		BCI Joist		W-FLANGE		Section
Designation	Beam 36		Beam 37		Beam 38		Beam 39		Beam 40		Design
Description	Third Level - Main Bldg - Cantilever of Grid C		Third Level - Main Bldg - Cantilever on Grid B		Third Level - Main Bldg - Cantilevered edge beam at Grid A.2		Second Level - Guest House Floor Joists		Second Level - Guest House Cantilevered edge beam at Grid E		Descr
$L_{Left\_Span}$ (ft)											$L_{Left\_Sp}$
$L_{Center\_Span}$ (ft)	6.50		22.50		18.50		16.50		1.50		$L_{Center\_s}$
$L_{Right\_Span}$ (ft)	10.25		16.50		16.50				12.00		$L_{Right\_c}$
$L_L$ (ft)   Auto (ft)	1.0		1.0		16.5		1.0		13.5		$L_b$ (ft)
Beam Slope   $\alpha$	0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		0 : 12 0.0°		Beam Sl
Include Self Wt.	No		No		Yes		No		Yes		Include
$\gamma_{Wood}$ (lb/ft <sup>3</sup> )   $W_{Self}$ (lb/ft)	1				488.1 40.0				488.1 40.0		$\gamma_{Steel}$ (lb/ft <sup>3</sup> )
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	60.0 167.0		60.0 167.0		60.0 167.0		25.0 40.0		25.0 40.0		PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto	8.50		12.25		2.00		1.33		9.50		Trib Width
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	510.0 1419.5		735.0 2045.8		120.0 334.0		33.3 53.3		237.5 380.0		Factored PS
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )					52.0						PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto			12.25		2.00						Trib Width
Start   End Dist frm Left			6.5 20.5		2.50 16.5						Start   End D
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>			0.0 637.0		0.0 104.0						Factored PS
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											PSF <sub>DL</sub>   PS
Trib Width (ft)   Auto											Trib Width
Start   End Dist frm Left											Start Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											Factored PS
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   F
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L c
Start   End Dist frm Left											Start   End D
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored In
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   F
Trib Width (ft)   Auto											Trib Width
Max at L or R   Auto											Max at L c
Start   End Dist frm Left											Start   End D
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored In
Pt 1 Dead   Live (lbs)	1119.0 3114.0		207.0 575.0		-20.0 -56.0						Pt 1 Dead
Dist from Left   Auto	16.75		39.00		35.00						Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>	1119.0 3114.0		207.0 575.0		-20.0 -56.0						Factored F
Pt 2 Dead   Live (lbs)											Pt 2 Dead
Dist from Left   Auto											Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored F
Pt 3 Dead   Live (lbs)											Pt 3 Dead
Dist from Left   Auto											Dist from
Factored PT <sub>DL</sub>   PT <sub>LL</sub>											Factored F
$C_b$   $C_c$	1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		$C_b$   I
$C_t$   $C_i$	1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		1.00 1.00		D.N
Wet Use (Y/N)?											D.N
$F_v$ (psi)   $f_v$ (psi)	7.55 1.50		14.17 1.50		5.64 1.50		307.37 120.39		4.88 1.50		$A_w$ (in <sup>2</sup> )
$V_{ALL}$   $1.5V_{max}$ (kip)	151.06 28.54		283.40 54.03		112.77 8.88		2.74 1.07		97.60 32.05		$V_r/\Omega$   V
Shear Chk	18.9%		19.1%		7.9%		39.2%		32.8%		Shear
$F_{b,TT}$   $F_{b,CT}$ (psi)	50 1.67		50 1.67		50 1.67		1320 1320.14		50 1.67		$F_y$ (KS)
$S$ (in <sup>3</sup> )   $I_x$ (in <sup>4</sup> )	123.00 984.0		333.00 3220.0		78.40 612.0		33.95 237.7		73.00 518.0		$Z_x$ (in <sup>3</sup> )
$M_{ALL}$ (k*ft) +   -	306.89 306.89		830.84 830.84		82.39 82.39		3.74 3.74		128.95 128.95		$M_r/\Omega$ (k*
$M_{max}$ (k*ft) +   -	0.00 144.75		54.77 391.43		2.92 65.99		2.95 0.00		0.00 47.34		$M_{max}$ (k*
Bending Chk	0.0% 47.2%		6.6% 47.1%		3.5% 80.1%		78.9% 0.0%		0.0% 36.7%		Bending
Max LL   TL $\Delta$ Ratio	L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		L/ 360 L/ 240		Max LL   I
Allowable LL   TL $\Delta$											Allowable
$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in)	0.02 0.02		0.04 0.06		0.04 0.06		0.25 0.41		0.00 0.00		$\Delta_{Live\_Left}$   i
$\Delta_{Live\_Cntr}$   $\Delta_{Tot\_Cntr}$ (in)	0.32 0.43		0.65 0.92		0.55 0.84				0.13 0.23		$\Delta_{Live\_Cntr}$   i
$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in)											$\Delta_{Live\_Cant}$   i
Actual LL   TL $\Delta$ Ratio	L/ 770 L/ 567		L/ 605 L/ 432		L/ 717 L/ 472		L/ 793 L/ 488		L/ 2180 L/ 1260		Actual LL   I
$R_L$ (lbs)	$R_{L,DL}$ -15998 $R_{L,LL}$ -4229 -11769		17454 3670 13783		1711 321 1390		715 275 440		-31067 -13112 -17955		$R_L$ (lbs)
$R_C$ (lbs)	$R_{C,DL}$ $R_{C,LL}$		$R_{C,DL}$ $R_{C,LL}$		$R_{C,DL}$ $R_{C,LL}$		$R_{C,DL}$ $R_{C,LL}$		$R_{C,DL}$ $R_{C,LL}$		$R_C$ (lbs)
$R_R$ (lbs)	52550 13890 38660		100696 25202 75494		16959 5259 11700		715 275 440		39943 16858 23085		$R_R$ (lbs)
$F_{C-Perp}$ (psi)   Brg Chk	DNA DNA		DNA DNA		DNA DNA		0 75.2%		DNA DNA		D.N
Req'd Brg L   Brg Cap	DNA DNA		DNA DNA		DNA DNA		1 3/4" 950.0		DNA DNA		D.N
Req'd Brg C   Brg Cap	DNA DNA		DNA DNA		DNA DNA		1 3/4" 950.0		DNA DNA		D.N
Req'd Brg R   Brg Cap	DNA DNA		DNA DNA		DNA DNA		1 3/4" 950.0		DNA DNA		D.N

Reactions are Service Level # Pls. s | Span | Depth | 13.52 | 18.17 | 22.12 | 14.14 | 18.00 | Reactions are Shape | S

Nailing Requirements (if More Than 1 PLY) Or Bearing Requirements (I-Joist Only) DNA DNA DNA DNA DNA DNA LT: 1 3/4" Min End Brg, RT: 1 3/4" Min End Brg, Web Stiffnr's Req'd at All Conc Loads DNA D.N

Query	DESIGN	DESIGN	DESIGN	DESIGN	DESIGN	Location
Location   Type						Query
Query Result						

2006 NDS Wood AISC Steel Beam Design v 5.13



# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	141
Date:	5/31/
By:	B

Blue Cells Must be Entered Manually

	STEEL		STEEL		STEEL		STEEL		STEEL			
WOOD BEAMS	W12X65		W21X44		W21X44		W12X40		W21X73		STEEL	
Species	W FLANGE		W FLANGE		W FLANGE		W FLANGE		W FLANGE		Section	
Designation	Beam 46		Beam 47		Beam 48		Beam 49		Beam 50		Design	
Description	Second Level - Main Bldg - Beam Running E/W at grid A.4		Second Level - Main Bldg - North Beam at Grid 1.6		Second Level - Main Bldg - Beam running N/S at Grid 2.4		Second Level - Main Bldg - N/S beam along Grid 2.1 -		Second Level - Main Bldg - Main E/W beam along Grid A.7		Descr	
$L_{center\_span}$ (ft)	18.50		10.50		15.50		23.50		20.50		$L_{center\_span}$ (ft)	
$L_{center\_span}$ (ft)	18.50		10.50		15.50		23.50		20.50		$L_{center\_span}$ (ft)	
$L_{span\_clear}$ (ft)	17.0		9.0		11.5		1.3		8.0		$L_{span\_clear}$ (ft)	
$L_u$ (ft)   Auto (ft)	0 : 12		0 : 12		0 : 12		0 : 12		0 : 12		$L_u$ (ft)   Auto (ft)	
Beam Slope   $\alpha$	0.0°		0.0°		0.0°		0.0°		0.0°		Beam Slope   $\alpha$	
Include Self Wt.	Yes		Yes		Yes		Yes		Yes		Include	
$W_{wood}$ (lb/ft <sup>2</sup> )   $W_{self}$ (lb/ft)	490.1	65.0	487.4	44.0	487.4	44.0	492.3	40.0	488.9	73.0	$W_{steel}$ (lb/ft <sup>2</sup> )   $W_{self}$ (lb/ft)	
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	1678.0	2255.0	1125.0	167.0	25.0	40.0	25.0	40.0	25.0	40.0	PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	
Trib Width (ft)   Auto	1.00		1.33		12.50		11.25		1.33		Trib Width (ft)   Auto	
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	1678.0	2255.0	1499.6	222.6	312.5	500.0	281.3	450.0	33.3	53.3	Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	
Trib Width (ft)   Auto											Trib Width (ft)   Auto	
Start   End Dist from Left											Start   End Dist from Left	
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	
Trib Width (ft)   Auto											Trib Width (ft)   Auto	
Start   End Dist from Left											Start   End Dist from Left	
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>											Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>	
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )		832.0									Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	
Trib Width (ft)   Auto		1.0									Trib Width (ft)   Auto	
Max at L or R   Auto		Left									Max at L or R   Auto	
Start   End Dist from Left		3.0		17.0							Start   End Dist from Left	
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>		0.0		832.0							Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>	
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )											Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )	
Trib Width (ft)   Auto											Trib Width (ft)   Auto	
Max at L or R   Auto											Max at L or R   Auto	
Start   End Dist from Left											Start   End Dist from Left	
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>											Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>	
Pt 1 Dead   Live (lbs)			16123.0	24269.0	16123.0	23272.0			19524.0	61473.0	Pt 1 Dead   Live (lbs)	
Dist from Left   Auto			1.50		11.50				5.50		Dist from Left   Auto	
Factored PT <sub>DL</sub>   PT <sub>LL</sub>			16123.0	24269.0	16123.0	23272.0			19524.0	61473.0	Factored PT <sub>DL</sub>   PT <sub>LL</sub>	
Pt 2 Dead   Live (lbs)									6970.0	9881.0	Pt 2 Dead   Live (lbs)	
Dist from Left   Auto									9.50		Dist from Left   Auto	
Factored PT <sub>DL</sub>   PT <sub>LL</sub>									6970.0	9881.0	Factored PT <sub>DL</sub>   PT <sub>LL</sub>	
Pt 3 Dead   Live (lbs)									3657.0	5288.0	Pt 3 Dead   Live (lbs)	
Dist from Left   Auto									17.75		Dist from Left   Auto	
Factored PT <sub>DL</sub>   PT <sub>LL</sub>									3657.0	5288.0	Factored PT <sub>DL</sub>   PT <sub>LL</sub>	
$C_D$   $C_r$	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	$C_b$   $C_t$	
$C_s$   $C_i$	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	$D_N$	
Wet Use (Y/N)?											$D_N$	
$F_v$ (psi)   $f_v$ (psi)	4.72	1.50	7.25	1.50	7.25	1.50	3.51	1.50	9.65	1.50	$A_v$ (in <sup>2</sup> )	
$V_{ALL}$   $1.5V_{max}$ (kip)	94.38	40.39	144.90	43.89	144.90	35.87	70.21	9.06	192.92	71.14	$V_u/\Omega$   $V_u$	
Shear Chk	42.8%		30.3%		24.8%		12.9%		36.9%		Shear	
$F_{b,TT}$   $F_{b,CT}$ (psi)	50	1.67	50	1.67	50	1.67	50	1.67	50	1.67	$F_y$ (ksi)	
$S$ (in <sup>3</sup> )   $I_x$ (in <sup>4</sup> )	96.80	533.0	95.40	843.0	95.40	843.0	57.00	307.0	172.00	1600.0	$Z_x$ (in <sup>3</sup> )	
$M_{ALL}$ (k*ft) +   -	218.73	218.73	187.18	187.18	159.25	159.25	142.22	142.22	408.46	408.46	$M_u/\Omega$ (k*ft)	
$M_{max}$ (k*ft) +   -	188.80	0.00	64.06	0.00	136.40	0.00	53.24	0.00	388.46	0.00	$M_{max}$ (k*ft)	
Bending Chk	86.3%		0.0%		85.7%		0.0%		37.4%		0.0%	
Max LL   TL $\Delta$ Ratio	L/ 360	L/ 240	L/ 360	L/ 240	L/ 360	L/ 240	L/ 360	L/ 240	L/ 360	L/ 240	Max LL   TL $\Delta$ Ratio	
Allowable LL   TL $\Delta$											Allowable	
$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in)	0.45	0.75	0.02	0.05	0.12	0.20	0.35	0.59	0.39	0.55	$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in)	
$\Delta_{Live\_Cnr}$   $\Delta_{Tot\_Cnr}$ (in)											$\Delta_{Live\_Cnr}$   $\Delta_{Tot\_Cnr}$ (in)	
$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in)											$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in)	
Actual LL   TL $\Delta$ Ratio	L/ 489	L/ 296	L/ 6274	L/ 2580	L/ 1581	L/ 931	L/ 813	L/ 474	L/ 637	L/ 450	Actual LL   TL $\Delta$ Ratio	
$R_L$ (lbs)	40392	16123	43894	21924	16804	6924	9062	3775	71144	19606	$R_L$ (lbs)	
$R_{LL}$		24269		21971		9881		5288		51538		
$R_C$ (lbs)											$R_C$ (lbs)	
$R_{CL}$												
$R_{CLL}$												
$R_R$ (lbs)	39395	16123	15043	10407	35866	14725	9062	3775	38921	12724	$R_R$ (lbs)	
$R_{RL}$		23272		4636		21141		5288		26197		
$F_{C\_Perp}$ (psi)   Brg Chk	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	$D_N$	
Req'd Brg L   Brg Cap	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	$D_N$	
Req'd Brg C   Brg Cap											$D_N$	
Req'd Brg R   Brg Cap	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	DNA	$D_N$	

Reactions are Service Level

# Pkts | Span/Depth

Nailing Requirements

(If More Than 1 PLY)

Or Bearing Requirements

(1-Joist Only)

Query

Location | Type

Query Result

2006 NDS Wood AISC Steel Beam Design v.5.13

by B. Saxey

28:36

B

# Exhibit A

## MJ STRUCTURAL ENGINEERS

ASD Design

Design of Wood Beams Based on the NDS  
Design of Steel Beams Based on AISC 360

Sht Number:	
Job Number:	143
Date:	5/31/
By:	B

Blue Cells Must be Entered Manually

	STEEL	WOOD	WOOD	STEEL	WOOD	
<b>WOOD BEAMS</b>	<b>HSS14X6X5/16</b>					<b>STEEL</b>
Species	HSS RECT					Section
Designation	Beam 56	Beam 57	Beam 58	Beam 59	Beam 60	Design
Description	Second Level - Main Bldg - Moment Frame support beam	Second Level - Main Bldg - Beam Running N/S at grid 1.5 - South Span	Second Level - Main Bldg - Edge Beam at Grid 1.2	Second Level - Main Bldg - Cantilevered Beam Grid C	Second Level - Main Bldg - Cantilevered beam on Grid B	Descr
$L_{Left\_Span}$ (ft)						$L_{Left\_Span}$
$L_{Center\_Span}$ (ft)	4.50					$L_{Center\_Span}$
$L_{Right\_Cant}$ (ft)						$L_{Right\_Cant}$
$L_U$ (ft)   <i>Auto</i> (ft)	1.0					$L_U$ (ft)
Beam Slope   $\alpha$	0 : 12    0.0°					Beam Slope
Include Self Wt.						Include
$Y_{wood}$ (lb/ft <sup>3</sup> )   $W_{self}$ (lb/ft)	1					$Y_{steel}$ (lb/ft <sup>3</sup> )
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )						PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   <i>Auto</i>	2					Trib Width
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>						Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )						PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   <i>Auto</i>	3					Trib Width
Start   End Dist frm Left						Start   End Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>						Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>
PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )						PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   <i>Auto</i>	4					Trib Width
Start   End Dist frm Left						Start   End Dist
Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>						Factored PLF <sub>DL</sub>   PLF <sub>LL</sub>
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )						Incr PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   <i>Auto</i>	5					Trib Width
Max at L or R   <i>Auto</i>						Max at L or R
Start   End Dist frm Left						Start   End Dist
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>						Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>
Incr PSF <sub>DL</sub>   PSF <sub>LL</sub> (lb/ft <sup>2</sup> )						Incr PSF <sub>DL</sub>   PSF <sub>LL</sub>
Trib Width (ft)   <i>Auto</i>	6					Trib Width
Max at L or R   <i>Auto</i>						Max at L or R
Start   End Dist frm Left						Start   End Dist
Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>						Factored Incr <sub>DL</sub>   Incr <sub>LL</sub>
Pt 1 Dead   Live (lbs)	67.8    11.2					Pt 1 Dead   Live
Dist from Left   <i>Auto</i>	2.25					Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>	67.8    11.2					Factored PT <sub>DL</sub>   PT <sub>LL</sub>
Pt 2 Dead   Live (lbs)						Pt 2 Dead   Live
Dist from Left   <i>Auto</i>						Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>						Factored PT <sub>DL</sub>   PT <sub>LL</sub>
Pt 3 Dead   Live (lbs)						Pt 3 Dead   Live
Dist from Left   <i>Auto</i>						Dist from Left
Factored PT <sub>DL</sub>   PT <sub>LL</sub>						Factored PT <sub>DL</sub>   PT <sub>LL</sub>
$C_D$   $C_r$	1.00    1.00					$C_D$   $C_r$
$C_t$   $C_i$	1.00    1.00					$C_t$   $C_i$
Wet Use (Y/N)?						
$F_v$ (psi)   $f_v$ (psi)	8.15    1.67					$A_w$ (in <sup>2</sup> )
$V_{ALL}$   $1.5V_{max}$ (kip)	134.66    0.04					$V_r/\Omega$   $V$
Shear Chk	0.0%					Shear
$F_{b\_TT}$   $F_{b\_CT}$ (psi)	46    1.67					$F_y$ (ksi)
$S$ (in <sup>3</sup> )   $I_x$ (in <sup>4</sup> )	48.60    271.0					$Z_x$ (in <sup>3</sup> )
$M_{ALL}$ (k*ft) +   -	111.56    111.56					$M_r/\Omega$ (k*ft)
$M_{max}$ (k*ft) +   -	0.09    0.00					$M_{max}$ (k*ft)
Bending Chk	0.1%    0.0%					Bending
Max LL   TL $\Delta$ Ratio	L/ 360    L/ 240					Max LL   TL $\Delta$ Ratio
Allowable LL   TL $\Delta$						Allowable
$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$ (in)						$\Delta_{Live\_Left}$   $\Delta_{Tot\_Left}$
$\Delta_{Live\_Cnr}$   $\Delta_{Tot\_Cnr}$ (in)	0.00    0.00					$\Delta_{Live\_Cnr}$   $\Delta_{Tot\_Cnr}$
$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$ (in)						$\Delta_{Live\_Cant}$   $\Delta_{Tot\_Cant}$
Actual LL   TL $\Delta$ Ratio	##### L/ 1638543					Actual LL   TL $\Delta$ Ratio
$R_L$ (lbs)	$R_{L\_DL}$ 34 $R_{L\_LL}$ 6					$R_L$ (lbs)
$R_C$ (lbs)	$R_{C\_DL}$ $R_{C\_LL}$					$R_C$ (lbs)
$R_R$ (lbs)	$R_{R\_DL}$ 34 $R_{R\_LL}$ 6					$R_R$ (lbs)
$F_c$ -Perp (psi)   Brg Chk	DNA    DNA					D.N
Req'd Brg L   Brg Cap	DNA    DNA					D.N
Req'd Brg C   Brg Cap						D.N
Req'd Brg R   Brg Cap	DNA    DNA					D.N

Reactions are Service Level  
# Plys | Span/Depth

HSS 3.36

Reactions are  
Shape 1 S

Nailing Requirements  
(If More Than 1 PLY)  
Or Bearing Requirements  
(1-Joist Only)

DNA

D.N

Query  
Location | Type  
Query Result

DESIGN	DESIGN	DESIGN	DESIGN	DESIGN

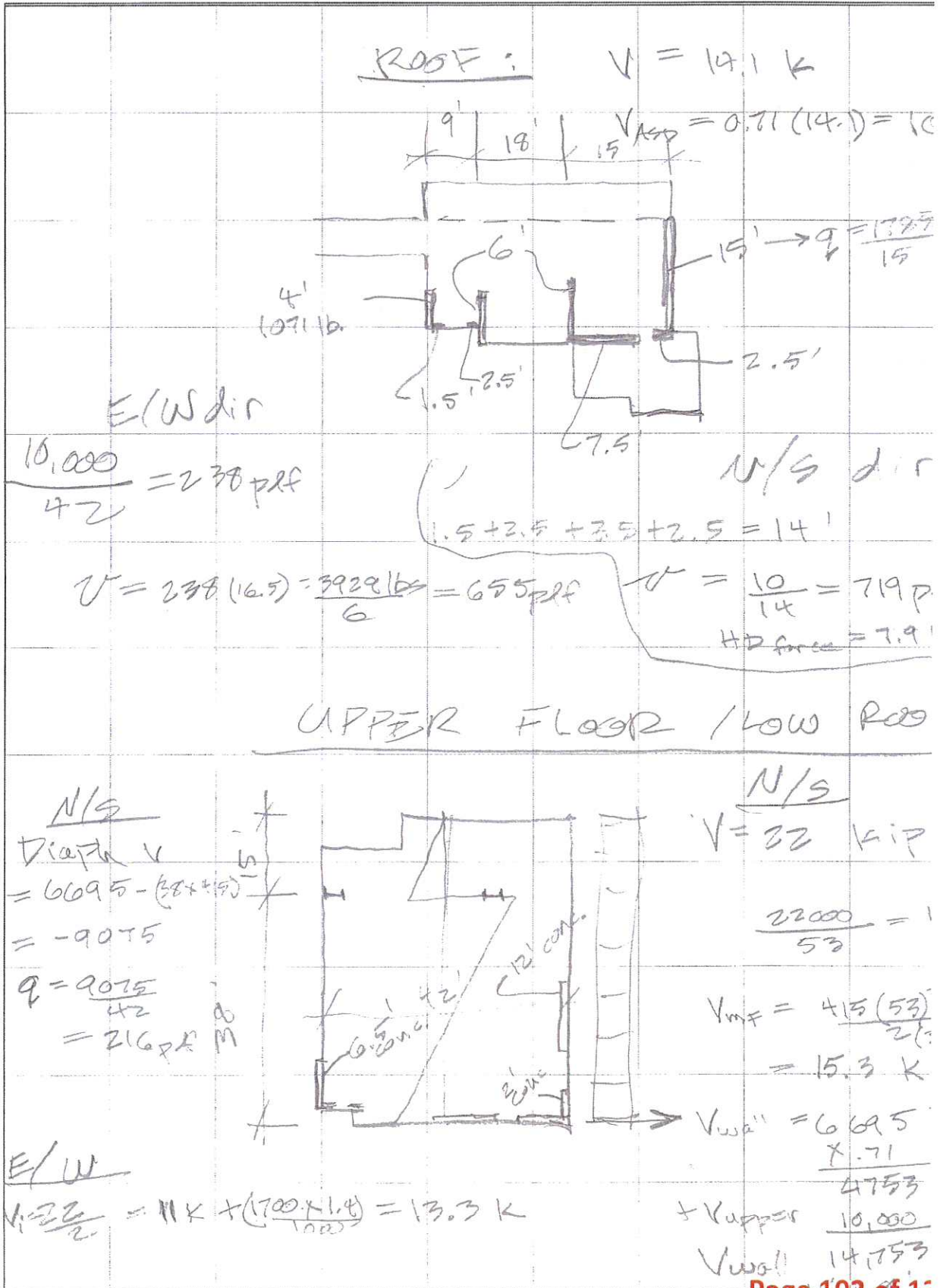
Location  
Query





Seismic Main House

TITLE:



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 and then using the "Printing &  
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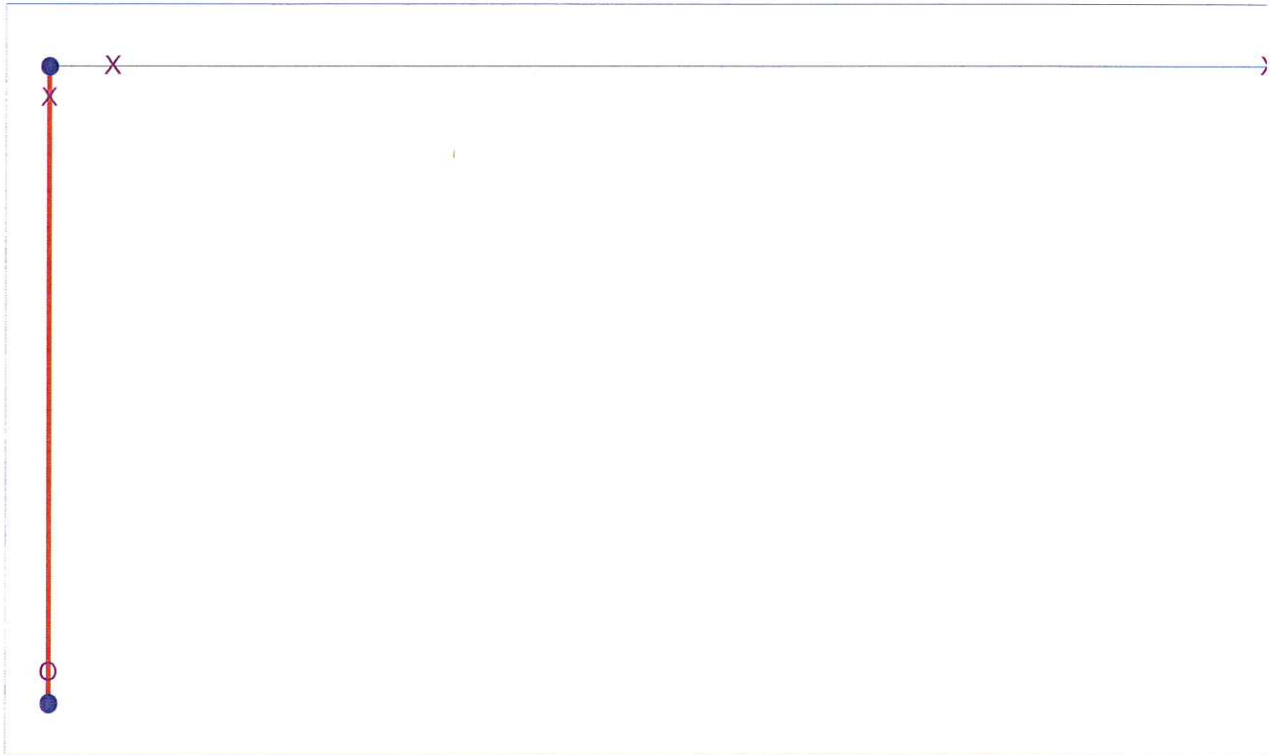
Project Title:  
 Engineer:  
 Project Descr:

Project ID

**2-D Frame**

Lic. # : KW-06009804

Printed: 31 MA  
 File = K:\2014\14123P-1\BR  
 ENERCALC, INC. 1983-2016, Build:6.16.4.15  
 Licensee : MJ Structura



**Joints...**

Joint Label	Joint Coordinates		X Translational Restraint	Y Translational Restraint	Z Rotational Restraint
	X ft	Y ft			
1	0.0	0.0	Fixed	Fixed	Fixed
2	0.0	12.0			
3	24.50	12.0	Fixed	Fixed	Fixed
4	24.50	0.0			

**Members...**

Member Label	Property Label	Endpoint Joints		Member Length ft	Releases Specify Connectivity of Member Ends to Joints				
		I Joint	J Joint		x	I End y	z (rotation)	J End x	y
A	Column	1	2	12.000	Fixed	Fixed	Pinned	Fixed	Fixed
B	Beam	2	3	24.500	Fixed	Fixed	Fixed	Fixed	Fixed
C	Column	3	4	12.000	Fixed	Fixed	Fixed	Fixed	Fixed

**Member Stress Check Data...**

Member Label	Unbraced Lengths		Slenderness Factors		AISC Bending & Stability Factors	
	Lu : z ft	Lu : y	K : z	K : y	Cm	Cb
A	12.000	12.000	1.00	1.00	Internal	Internal
B	24.500	24.500	1.00	1.00	Internal	Internal
C	12.000	12.000	1.00	1.00	Internal	Internal

**Materials...**

Member Label	Youngs ksi	Density kcf	Thermal in/deg	Yield ksi
Default	1.00	0.000	0.000000	1.00
Steel	29,000.00	0.490	0.000007	50.00
Wood	1,800.00	0.035	0.000000	0.00

**Wood Material Data...**





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using the "Settings" menu item  
and then using the "Printing &  
Title Block" selection.  
Title Block Line 6

**Exhibit A**

Project Title:  
Engineer:  
Project Descr:

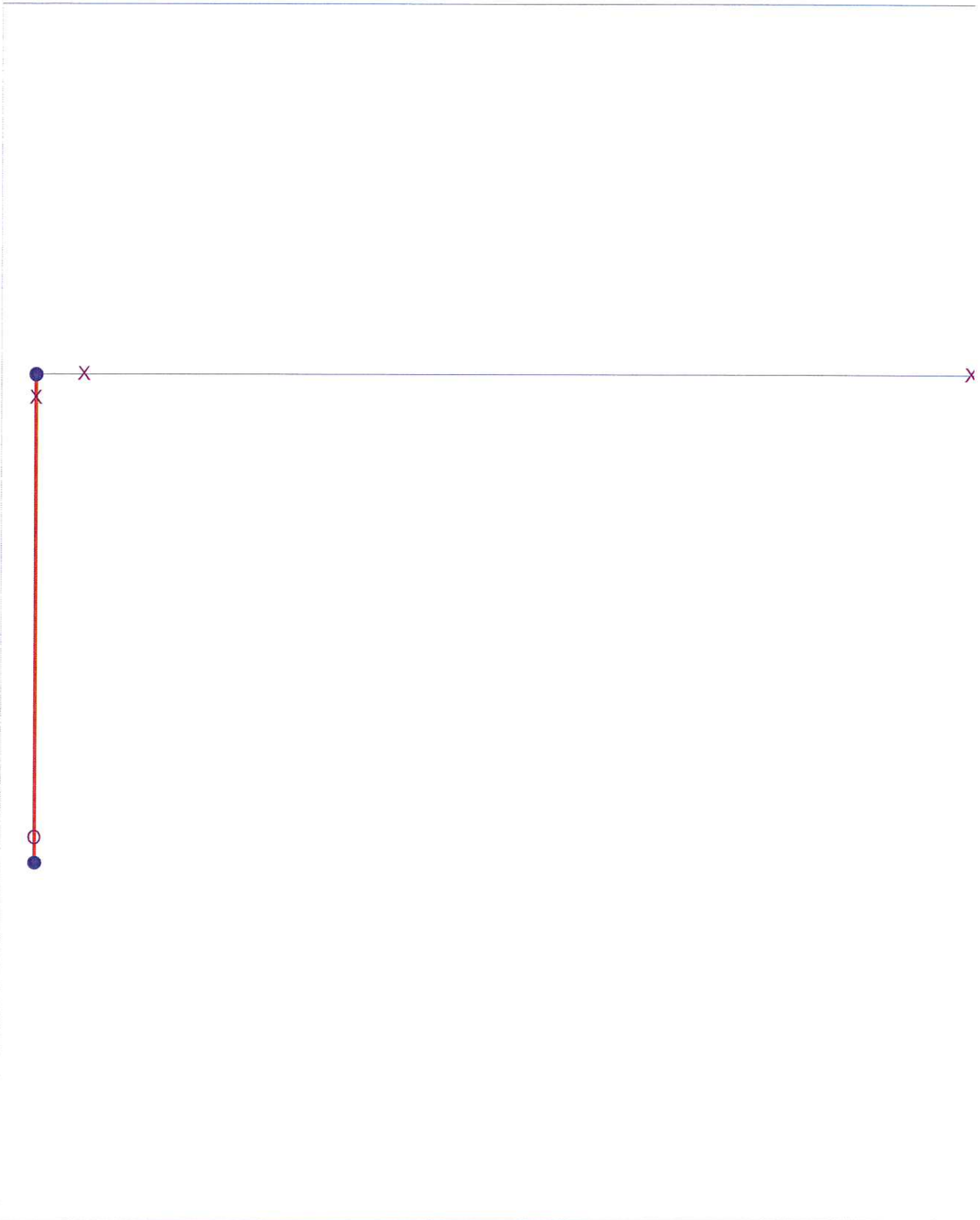
Project ID

Printed: 31 MA

## 2-D Frame

File = K:\2014\14123P-1\BR  
ENERCALC, INC. 1983-2016, Build:6.16.4.15  
Licensee : MJ Structura

Lic. # : KW-06009804





## **Exhibit B**

*Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah*

### **METHOD OF STUDY**

#### ***Literature Review***

IGES completed a geotechnical investigation for the Powder Mountain Resort expansion in 2012 (2012a, 2012b). Our previous work included twenty-two test pits and one soil boring excavated at various locations across the 200-acre development; as a part of this current study, the logs from relevant nearby test pits and other data from our reports were reviewed. We also reviewed the work previously done for the nearby Lot 39R located at 8365 East Summit Pass Road (2015a, 2015b, 2015c, 2016a, 2016b). In addition, Western Geologic (2012) completed a geologic hazard study for the greater 200-acre Powder Mountain expansion project – this report was reviewed to help assess the potential impact of geologic hazards on the subject lot.

#### ***Field Investigation***

Subsurface soils were investigated by excavating one test pit approximately 20 feet below the existing site grade. The approximate location of the test pit is illustrated on the *Local Geology and Geotechnical Map* (Plate 1). The soil types and conditions were visually logged at the time of the excavation in general accordance with the Unified Soil Classification System (USCS). Subsurface soil classifications and descriptions are included on the test pit log included as Figures A-2 in Appendix A. A key to USCS symbols and terminology is included as Figure A-3.

#### ***Laboratory Testing***

The majority of materials encountered in the test pits consisted of coarse, cemented colluvium with abundant cobbles, or relatively stiff/hard sandy clay. As such, soil samples suitable for testing in an oedometer could not be obtained. Therefore, laboratory testing and engineering analysis was based largely on previously completed geotechnical investigations (IGES, 2012a & 2012b) and laboratory testing for this project that included index testing (grain size analysis, Atterberg Limits).

#### ***Engineering Analysis***

Engineering analyses were performed using soil data obtained from laboratory testing and empirical correlations based on material density, depositional characteristics and classification. Appropriate factors of safety were applied to the results consistent with industry standards and the accepted standard of care. An allowable bearing pressure value was proportioned based on estimated shear strength of bearing soils with due consideration for allowable settlement.

### **FINDINGS**

#### ***Surface Conditions***

At the time of the excavation, the lot was in a relatively natural state and was covered with a sparse vegetative cover including native grasses and shrubs. Several boulders (>12 inches) were observed throughout the site. The lot drains to the southwest; the gradient of

## **Exhibit B**

*Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah*

areas where collapsible soils are identified at great depth, a deep foundation system may be prescribed. Typical characteristics of collapsible soils include a) low dry unit weight (silts and fine sands), b) relatively dry soils, and c) porous soil structure (“pinholes”). These characteristics were not identified during our subsurface exploration; as such, wetting-induced collapse is not expected to significantly impact the proposed improvements.

### ***Geology and Geologic Hazards***

Geology and geologic hazards have been previously addressed by Western Geologic in a separate submittal (Western Geologic, 2012). This work has also been referenced in our previous geotechnical reports for the project (IGES, 2012a and 2012b). The report by Western Geologic indicates that the building envelope is located outside of known geologically unstable areas. The lower quarter of the lot (beyond buildable areas) is mapped as undifferentiated “mixed slope colluvium, shallow landslides, and talus” (Western Geologic, 2012).

During our subsurface investigation, potentially adverse geologic structures (e.g., evidence of faulting or landslides) were not evident to the maximum depth of exploration (20 feet). Geomorphic expressions of shallow, surficial landslides were not observed on, or near the building envelope. An approximately 200-foot long linear feature was identified near the southern middle portion of the property, which at first glance appears to be a headscarp to a shallow surficial landslide; however, there are no associated landslide feature downslope (e.g., hummocky topography, toe bulge, internal scarps, etc.). Since there are no corresponding landslide features, this feature is thought to be associated with local, shallow soil creep, or possibly local surface erosion. Also, a shallow, surficial landslide was identified southwest of Lot 37R, downslope of Lot 38R (this feature is shown on Plate 1, *Local Geology & Geotechnical Map*). This landslide is not located directly downslope of Lot 37R and is not expected to impact the proposed improvements.

In conclusion, surface mapping did not reveal any geomorphic features indicative of potential geologic hazards (e.g., landslides, slumps, tension cracks, scarps, hummocky topography, etc.) on or near the building envelope. Based on currently available data and our observations, the potential for geologic hazards such as landslides, liquefaction, or surface fault rupture impacting the site is considered low. A map showing the local geology is presented as Plate 1, *Local Geology & Geotechnical Map*.

### ***Slope Stability***

The site is located on the side of a mountain, and therefore is on sloped terrain. The sloped terrain was modeled using SLIDE version 6.024 slope stability software. Spencer’s Method was used to evaluate the stability of the slope. Calculations for stability were developed by searching for the minimum factor-of-safety for a circular-type failure. A minimum static factor-of-safety of 1.5 and seismic factor-of-safety of 1.0 was considered acceptable for this project considering the available information. The section analyzed is Section A-A’, illustrated on Plate 1 of this report.



## Exhibit B

Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah

both *NEHRP Recommended Provisions for Seismic Regulations for New Buildings and Other Structures* (FEMA, 1997) and the *International Building Code* (IBC) (International Code Council, 2012).

To account for site effects, site coefficients that vary with the magnitude of spectral acceleration and *Site Class* are used. Site Class is a parameter that accounts for site amplification effects of soft soils and is based on the average shear wave velocity of the upper 100 feet; based on our field exploration and our understanding of the geology in this area, the subject site is appropriately classified as Site Class B (*very dense soil and soft rock*). Based on IBC criteria, the short-period ( $F_a$ ) coefficient is 1.0 and long-period ( $F_v$ ) site coefficient is 1.0. Based on the design spectral response accelerations for a *Building Risk Category* of I, II or III, the site's *Seismic Design Category* is D. The short- and long-period *Design Spectral Response Accelerations* are presented in Table 2.0; a summary of the *Design Maps* analysis is presented in Appendix B. The *peak ground acceleration* (PGA) may be taken as  $0.4 \cdot S_{MS}$ .

Table 2.0  
Short- and Long-Period Spectral Accelerations for MCE

Parameter	Short Period (0.2 sec)	Long Period (1.0 sec)
MCE Spectral Response Acceleration (g)	$S_S = 0.817$	$S_1 = 0.271$
MCE Spectral Response Acceleration Site Class B (g)	$S_{MS} = S_S F_a = 0.817$	$S_{M1} = S_1 F_v = 0.271$
Design Spectral Response Acceleration (g)	$S_{DS} = S_{MS}^{2/3} = 0.545$	$S_{D1} = S_{M1}^{2/3} = 0.181$

### CONCLUSIONS AND RECOMMENDATIONS

Based on the results of field observations, laboratory testing for this project and during a previously completed geotechnical investigation (IGES, 2012a), and other recent geotechnical work nearby, the subsurface conditions are considered suitable for the proposed construction provided that the recommendations presented in this report are incorporated into the design and construction of the project.

#### *General Site Preparation and Grading*

Prior to the placement of foundations, general site grading is recommended to provide proper support for exterior concrete flatwork, concrete slabs-on-grade, and pavement sections. Site grading is also recommended to provide proper drainage and moisture control on the subject property and to aid in preventing differential movement in foundation soils as a result of variations in moisture conditions.

## **Exhibit B**

*Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah*

### ***Structural Fill and Compaction***

All fill placed for the support of structures, flatwork or pavements should consist of structural fill. Structural fill should consist of granular native soils, which may be defined as soils with less than 25% fines, 10-60% sand, and contain no rock larger than 4 inches in nominal size (6 inches in greatest dimension). Structural fill should also be free of vegetation and debris. Soils not meeting these criteria may be suitable for use as structural fill; however, such soils should be evaluated on a case by case basis and should be approved by IGES prior to use.

All structural fill should be placed in maximum 4-inch loose lifts if compacted by small hand-operated compaction equipment, maximum 6-inch loose lifts if compacted by light-duty rollers, and maximum 8-inch loose lifts if compacted by heavy duty compaction equipment that is capable of efficiently compacting the entire thickness of the lift. These lift thicknesses are *maximums*; the contractor should be aware that thinner lifts may be necessary to achieve the desired compaction. We recommend that all structural fill be compacted on a horizontal plane, unless otherwise approved by IGES. Structural fill underlying all shallow footings and pavements should be compacted to at least 95 percent of the MDD as determined by ASTM D-1557. The moisture content should be at, or slightly above, the OMC for all structural fill. Any imported fill materials should be approved prior to importing. Also, prior to placing any fill, the excavations should be observed by IGES to confirm that unsuitable materials have been removed.

Specifications from governing authorities such as Weber County and/or special service districts having their own precedence for backfill and compaction should be followed where more stringent.

### ***Utility Trench Backfill***

Utility trenches should be backfilled with structural fill in accordance with the previous section. Utility trenches can be backfilled with the onsite soils free of debris, organic and oversized material. Prior to backfilling the trench, pipes should be bedded in and shaded with a uniform granular material that has a Sand Equivalent (SE) of 30 or greater. Pipe bedding may be water-densified in-place (jetting). Alternatively, pipe bedding and shading may consist of clean ¾-inch gravel, which generally does not require densification. Native earth materials can be used as backfill over the pipe bedding zone. All utility trenches backfilled below pavement sections, curb and gutter, hardscape, should be backfilled with structural fill compacted to at least 95 percent of the MDD as determined by ASTM D-1557. All other trenches should be backfilled and compacted to approximately 90 percent of the MDD (ASTM D-1557). However, in all cases the pipe bedding and shading should meet the design criteria of the pipe manufacturer. Specifications from governing authorities having their own precedence for backfill and compaction should be followed where they are more stringent.

### ***Foundations***

Based on our field observations and considering the presence of relatively competent native earth materials, we recommend that the footings for the proposed home be founded either



## Exhibit B

Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah

Ultimate lateral earth pressures from *granular* backfill acting against retaining walls, temporary shoring, or buried structures may be computed from the lateral pressure coefficients or equivalent fluid densities presented in Table 3.0:

**Table 3.0**  
**Lateral Earth Pressure Coefficients**

Condition	Level Backfill		2H:1V Backfill	
	Lateral Pressure Coefficient	Equivalent Fluid Density (pcf)	Lateral Pressure Coefficient	Equivalent Fluid Density (pcf)
Active (Ka)	0.33	40	0.53	64
At-rest (Ko)	0.50	60	0.80	96
Passive (Kp)	3.0	360	—	—

These coefficients and densities assume no buildup of hydrostatic pressures. The force of water should be added to the presented values if hydrostatic pressures are anticipated.

Clayey soils drain poorly and may swell upon wetting, thereby greatly increasing lateral pressures acting on earth retaining structures; therefore, clayey soils should not be used as retaining wall backfill. Backfill should consist of native granular soil with an Expansion Index (EI) less than 20.

Walls and structures allowed to rotate slightly should use the active condition. If the element is to be constrained against rotation (i.e., a basement or buried tank wall), the at-rest condition should be used. These values should be used with an appropriate factor of safety against overturning and sliding. A value of 1.5 is typically used. Additionally, if passive resistance is calculated in conjunction with frictional resistance, the passive resistance should be reduced by ½.

### **Concrete Slab-on-Grade Construction**

To minimize settlement and cracking of slabs, and to aid in drainage beneath the concrete floor slabs, all concrete slabs should be founded on a minimum 4-inch layer of compacted gravel overlying properly prepared subgrade. The gravel should consist of free-draining gravel or road base with a ¾-inch maximum particle size and no more than 5 percent passing the No. 200 mesh sieve. The layer should be compacted to at least 95 percent of the MDD as determined by ASTM D-1557.

All concrete slabs should be designed to minimize cracking as a result of shrinkage. Consideration should be given to reinforcing the slab with a welded wire fabric, re-bar, or fibermesh. Slab reinforcement should be designed by the structural engineer; however, as a minimum, slab reinforcement should consist of 4'×4' W4.0×W4.0 welded wire mesh within the middle third of the slab. We recommend that concrete be tested to assess that the slump and/or air content is in compliance with the plans and specifications. We recommend that concrete be placed in general accordance with the requirements of the

## **Exhibit B**

*Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah*

### ***Construction Considerations***

- **Excavation Difficulty**: The rocky, cemented colluvium identified approximately 6 feet below existing grade was difficult to excavate. Hard, cemented gravels, or conglomerate bedrock (Wasatch Formation) may be difficult to excavate and may require heavy-duty rippers or other specialized excavation procedures.
- **Over-Size Material**: Rounded boulders to 24 inches were identified in the test pits and on the ground surface; larger rocks may be present locally. The site is overlain with bouldery colluvium, largely derived from the underlying Wasatch Formation, which consists of cobbly/bouldery conglomerate. Large rocks may require special handling, such as segregation from structural fill, and disposal.

### **CLOSURE**

The recommendations presented in this report are based on limited field exploration, literature review, and a general understanding of the proposed construction. The subsurface data used in the preparation of this report were obtained from the exploration(s) made for this investigation. It is possible that variations in the soil and groundwater conditions could exist beyond the point explored. The nature and extent of variations may not be evident until construction occurs. If any conditions are encountered at this site that are different from those described in this report, IGES should be immediately notified so that any necessary revisions to recommendations contained in this report may be made. In addition, if the scope of the proposed construction changes from that described in this report, IGES should also be notified.

This report was prepared in accordance with the generally accepted standard of practice at the time the report was written. No warranty, expressed or implied, is made.

It is the Client's responsibility to see that all parties to the project including the Designer, Contractor, Subcontractors, etc. are made aware of this report in its entirety. The use of information contained in this report for bidding purposes should be done at the Contractor's option and risk.

### ***Additional Services***

The recommendations presented in this report are based on the assumption that an adequate program of tests and observations will be made during the construction. IGES staff should be on site to verify compliance with these recommendations. These tests and observations should include, but not necessarily be limited to, the following:

- Observations and testing during site preparation, earthwork and structural fill placement.
- Consultation as may be required during construction.
- Quality control testing of cast-in-place concrete.
- Review of plans and specifications to assess compliance with our recommendations.



## **Exhibit B**

*Lot 37R of Powder Mountain Resort  
8343 East Summit Pass, Weber County, Utah*

### References

- AMEC, 2001, Report Engineering Geologic Reconnaissance/Geotechnical Study Powder Mountain Resort.
- Federal Emergency Management Agency [FEMA], 1997, *NEHRP Recommended Provisions for Seismic Regulations for New Buildings and Other Structures*, FEMA 302, Washington, D.C.
- Frankel, A., Mueller, C., Barnard, T., Perkins, D., Leyendecker, E.V., Dickman, N., Hanson, S., and Hopper, M., 1996, *National Seismic-hazard Maps: Documentation*, U.S. Geological Survey Open-File Report 96-532, June.
- IGES, Inc., 2012a, Design Geotechnical Investigation, Powder Mountain Resort, Weber County, Utah, Project No. 01628-003, dated November 9, 2012.
- IGES, Inc., 2012b, Preliminary Geotechnical Investigation, Powder Mountain Resort, Weber County, Utah, Project No. 01628-001, dated July 26, 2012.
- IGES, Inc., 2015a, Geotechnical Investigation Report, Lot 39R of Powder Mountain Resort, 8365 East Summit Pass, Weber County, Utah, Project No. 02052-001, June 3, 2015
- International Building Code [IBC], 2012, International Code Council, Inc.
- U.S. Geological Survey, 2012, U.S. *Seismic "Design Maps" Web Application*, site: <https://geohazards.usgs.gov/secure/designmaps/us/application.php>.
- Western Geologic, 2012, Report: Geologic Hazards Reconnaissance, Proposed Area 1 Mixed-Use Development, Powder Mountain Resort, Weber County, Utah, dated August 28, 2012.

# Exhibit B

<b>DATE</b> STARTED: 6/23/16 COMPLETED: 6/23/16 BACKFILLED: 6/23/16		<b>Geotechnical Investigation</b> Lot 37R of Summit Eden Phase 1C 8343 East Summit Pass Weber County, Utah      Project Number 02332-001				IGES Rep: TQH		<b>TEST PIT N</b> <span style="font-size: 2em; font-weight: bold;">T</span>											
						Rig Type: CAT 315C													
						LOCATION LATITUDE 41.36540    LONGITUDE -111.75053    ELEVATION 8,620													
<b>DEPTH</b>	<b>ELEVATION</b>	<b>FEET</b>	<b>SAMPLES</b>	<b>WATER LEVEL</b>	<b>GRAPHICAL LOG</b>	<b>UNIFIED SOIL CLASSIFICATION</b>	<b>MATERIAL DESCRIPTION</b>		<b>Dry Density(pcf)</b>	<b>Moisture Content %</b>	<b>Percent minus 200</b>	<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>Moisture at Atterberg</b>	<b>Plastic Limit</b>	<b>Moi. Con</b>			
	0						<b>TOPSOIL</b> Clayey SAND with gravel - medium dense to loose, slightly moist to moist, dark brown - trace roots throughout <b>@ 2' COLLUVIUM (Oe)</b> Poorly Graded Clayey GRAVEL with sand - orangish brown, dry to moist, low plasticity clay, well-graded sand, large subangular to subrounded quartzite clasts (3- to 4-foot diameter maximum and 1- to 2-foot diameter typical), trace roots  <b>@ 6' WASATCH FORMATION (Twe)</b> Conglomerate, highly weathered, moderately cemented, readily disintegrates to soil classifying as Poorly Graded Clayey GRAVEL with sand (GC) - orangish red, moist, low plasticity clay, well-graded sand, large subangular to subrounded quartzite clasts (3- to 4-foot diameter maximum and 8- to 14-inch diameter typical), similar to overlying colluvium except Twe is more cemented and increasingly difficult to excavate				25.0	26	8	H	10	20	30	40	50
	5					GC													
	10																		
	15																		
	20																		
	Total depth 20 feet No groundwater																		

LOG OF TEST PITS 7/1/2016 02332-001.GPJ IGES.GDT 7/1/16



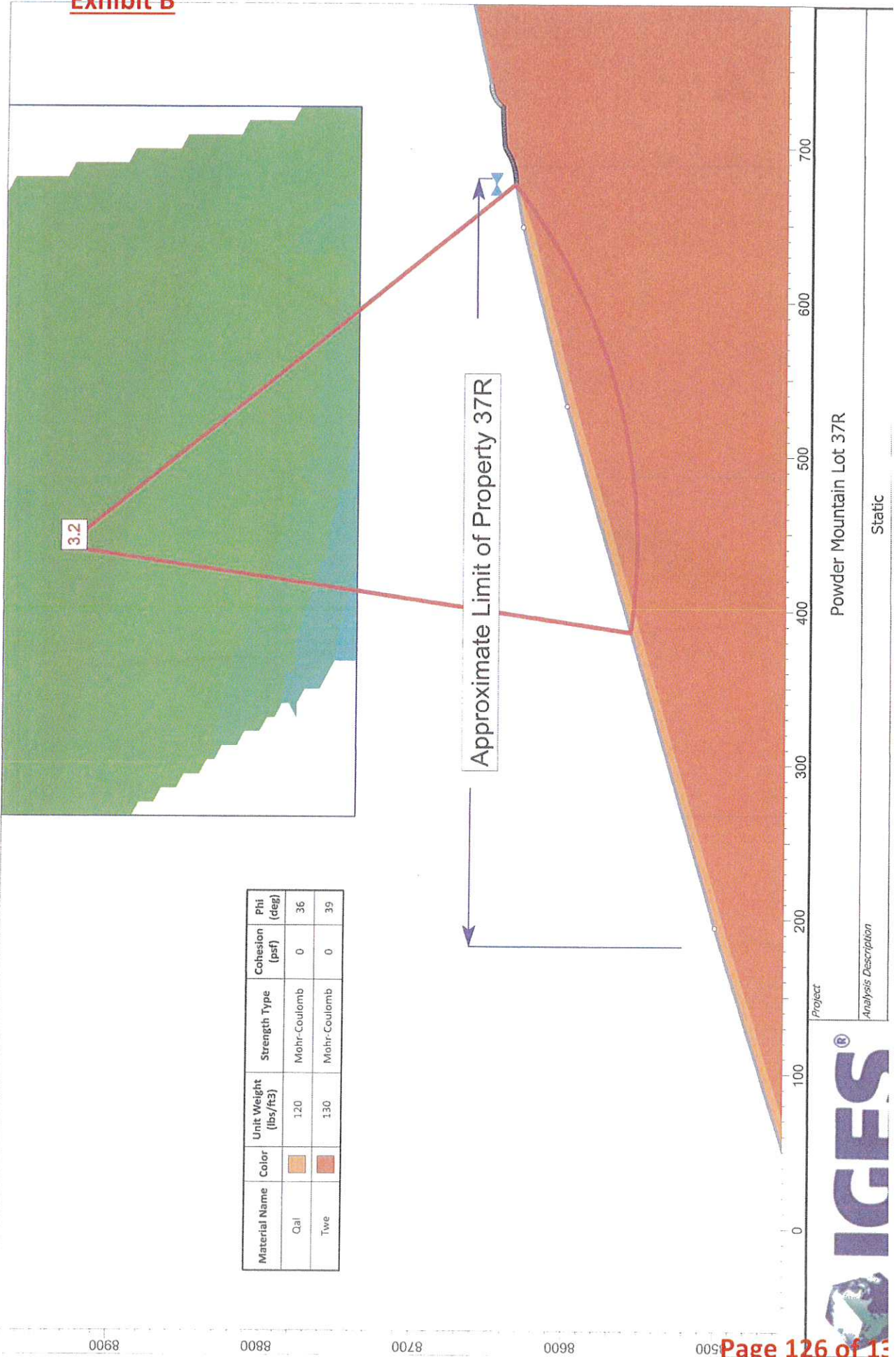
Copyright (c) 2016, IGES, INC

<b>SAMPLE TYPE</b>	
☐	- GRAB SAMPLE
☒	- 3" O.D. THIN-WALLED HAND SAMPLER
<b>WATER LEVEL</b>	
▼	- MEASURED
▽	- ESTIMATED

**NOTES:**



**Exhibit B**







# Exhibit B

## Particle-Size Distribution (Gradation) of Soils Using Sieve Analysis

(ASTM D6913)



Project: Lot 37R - Powder Mountain

No: 02332-001

Location: Eden, UT

Date: 6/28/2016

By: BRR/BSS

Boring No.:

Sample: 37R

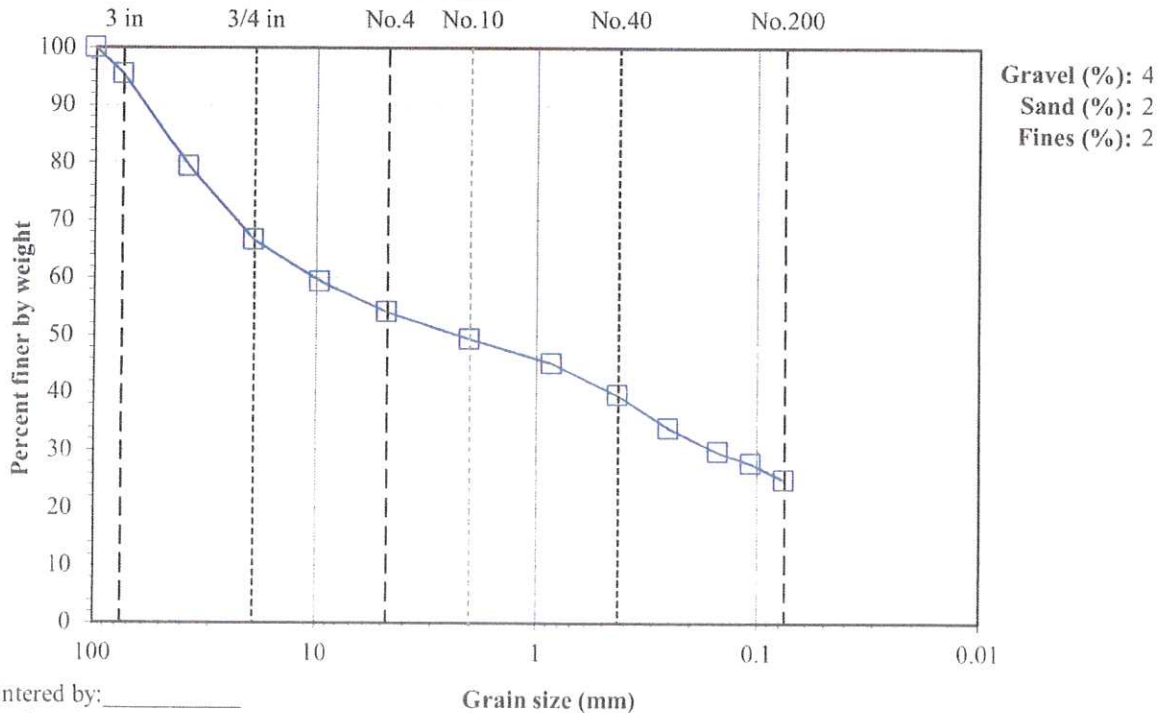
Depth:

Description: Brown clayey gravel

Split: Yes		Water content data C.F.(+3/4") S.F.(-3/4")	
Split sieve: 3/4"		Moist soil + tare (g):	2061.65 2083.86
Moist		Dry soil + tare (g):	2037.98 1971.10
Dry		Tare (g):	465.88 464.13
Total sample wt. (g):	61170.80 57991.79	Water content (%):	1.5 7.5
+3/4" Coarse fraction (g):	19704.70 19412.42		
-3/4" Split fraction (g):	1619.73 1506.97		
Split fraction:	0.665		

Sieve	Accum. Wt. Ret. (g)	Grain Size (mm)	Percent Finer
8"	-	200	-
6"	-	150	-
4"	-	100	100.0
3"	2691.48	75	95.4
1.5"	12047.51	37.5	79.2
3/4"	19412.42	19	66.5
3/8"	164.20	9.5	59.3
No.4	284.20	4.75	54.0
No.10	390.90	2	49.3
No.20	486.40	0.85	45.1
No.40	610.40	0.425	39.6
No.60	740.90	0.25	33.8
No.100	833.00	0.15	29.8
No.140	879.50	0.106	27.7
No.200	944.20	0.075	24.8



Entered by: \_\_\_\_\_  
Reviewed: \_\_\_\_\_

**Design Maps Detailed Report**

2012 International Building Code (41.36672°N, 111.75108°W)

Site Class B – “Rock”, Risk Category I/II/III

**Section 1613.3.1 — Mapped acceleration parameters**

Note: Ground motion values provided below are for the direction of maximum horizontal spectral response acceleration. They have been converted from corresponding geometric mean ground motions computed by the USGS by applying factors of 1.1 (to obtain  $S_c$ ) and 1.3 (to obtain  $S_1$ ). Maps in the 2012 International Building Code are provided for Site Class B. Adjustments for other Site Classes are made, as needed, in Section 1613.3.3.

**From Figure 1613.3.1(1)** <sup>[1]</sup>

$S_c = 0.817 \text{ g}$

**From Figure 1613.3.1(2)** <sup>[2]</sup>

$S_1 = 0.271 \text{ g}$

**Section 1613.3.2 — Site class definitions**

The authority having jurisdiction (not the USGS), site-specific geotechnical data, and/or the default has classified the site as Site Class B, based on the site soil properties in accordance with Section 1613.

2010 ASCE-7 Standard – Table 20.3-1  
SITE CLASS DEFINITIONS

Site Class	$\bar{v}_s$	$\bar{N}$ or $\bar{N}_{ch}$	$\bar{s}_u$
A. Hard Rock	>5,000 ft/s	N/A	N/A
B. Rock	2,500 to 5,000 ft/s	N/A	N/A
C. Very dense soil and soft rock	1,200 to 2,500 ft/s	>50	>2,000 psf
D. Stiff Soil	600 to 1,200 ft/s	15 to 50	1,000 to 2,000 psf
E. Soft clay soil	<600 ft/s	<15	<1,000 psf
Any profile with more than 10 ft of soil having the characteristics:			
<ul style="list-style-type: none"> <li>• Plasticity index <math>PI &gt; 20</math>,</li> <li>• Moisture content <math>w \geq 40\%</math>, and</li> <li>• Undrained shear strength <math>\bar{s}_u &lt; 500</math> psf</li> </ul>			
F. Soils requiring site response analysis in accordance with Section 21.1	See Section 20.3.1		

For SI: 1ft/s = 0.3048 m/s 1lb/ft<sup>2</sup> = 0.0479 kN/m<sup>2</sup>



**Equation (16-37):**

$$S_{MS} = F_a S_s = 1.000 \times 0.817 = 0.817 \text{ g}$$

---

**Equation (16-38):**

$$S_{M1} = F_v S_1 = 1.000 \times 0.271 = 0.271 \text{ g}$$

---

Section 1613.3.4 — Design spectral response acceleration parameters

**Equation (16-39):**

$$S_{DS} = \frac{2}{3} S_{MS} = \frac{2}{3} \times 0.817 = 0.545 \text{ g}$$

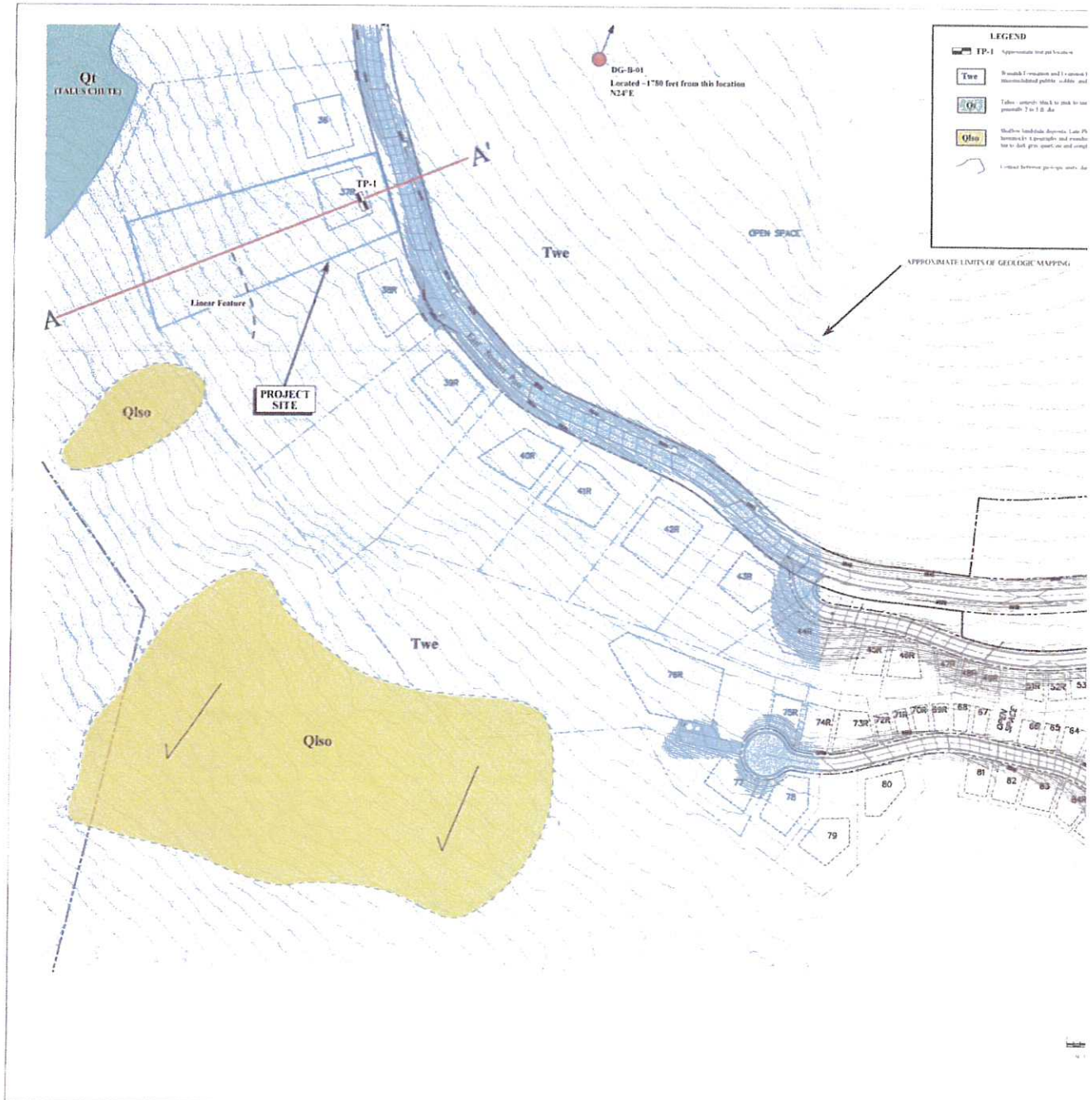
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**Equation (16-40):**

$$S_{D1} = \frac{2}{3} S_{M1} = \frac{2}{3} \times 0.271 = 0.181 \text{ g}$$

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# Exhibit B



LOCAL GEOLOGY AND GEOTECHNICAL MAP


 Geotechnical Investigation  
 Two (TP) of Summer Lake Phase II  
 1541 East Second Place  
 Richland, WA 99354  
 Project No. 02-111-001